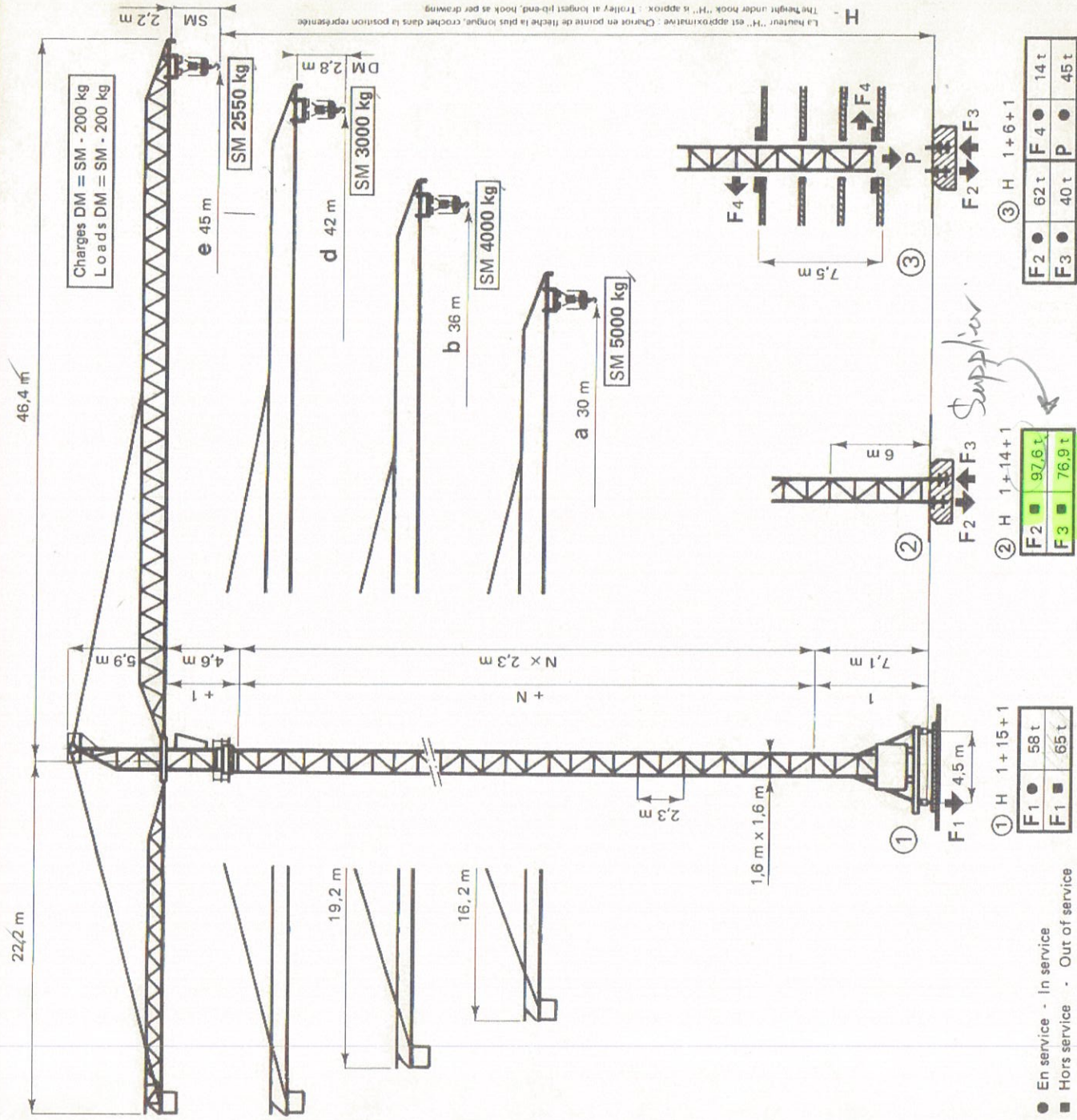


Potain 2440S



● En service - In service
■ Hors service - Out of service

LEVAGE - HOISTING		m/mn		kg
Trebail Hoist Winch	SM	1	0 → 30	5000
		2	0 → 40	4000
RCS 2A 45 - 45 ch/hp	DM	1	0 → 60	2500
		2	0 → 80	2000
1 - Tambour - Drum Grande vitesse Petite vitesse	2 - Coquilles - Laggings High speed Low speed	1	0 → 15	10000
		2	0 → 20	8000
		1	0 → 30	5000
		2	0 → 40	4000

Pylône Mast		H/S/M	
1 + 0 + 1	m	9,5	3
1 + 2 + 1	m	14,1	8,4
1 + 4 + 1	m	18,7	13
1 + 6 + 1	m	23,3	17,6
1 + 8 + 1	m	27,9	22,2
1 + 10 + 1	m	32,5	26,8
1 + 12 + 1	m	37,1	31,4
1 + 14 + 1	m	41,7	36
1 + 15 + 1	m	44	40,6
1 + 16 + 1	m	46,3	42,9
			45,2

H/DM = H/S/M - 0,6 m

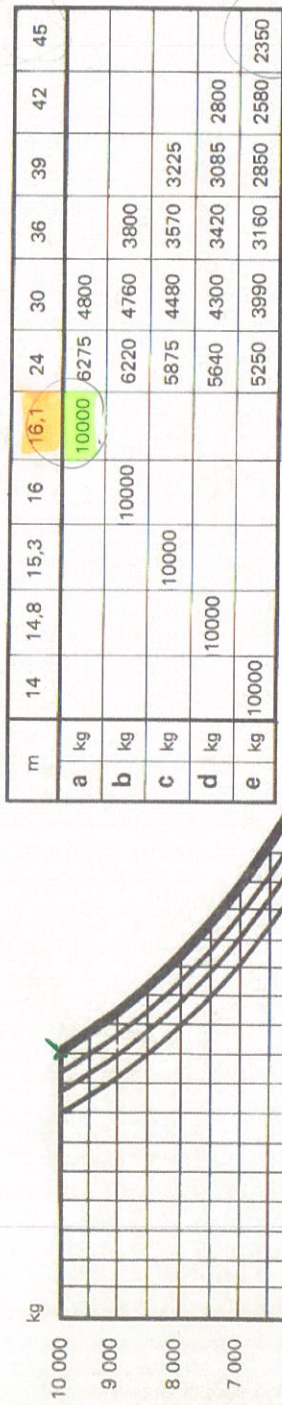
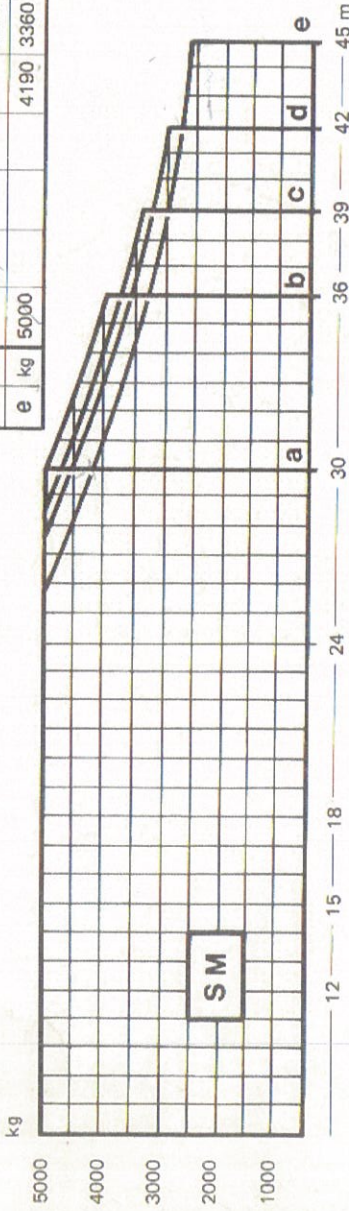
■ Ancre
Anchorage

Consider 2 case.

→ maximum load 5000kg L = 80m

→ maximum length = 45m load = 8550 kg

m	25,8	27,4	28,2	29,8	30	36	39	42	45
a kg					5000				
b kg						4000			
c kg			5000			3770	3425		
d kg		5000				3620	3285	3000	
e kg	5000					4190	3360	3050	2780
									2550



Consider 1 case.
→ maximum load 10000kg L = 16.1m.

Orientation Slewing	RCO	0 → 0,8 t/m n	2 x 6,5 ch hp	Puissance électrique nécessaire : 60 kVA Necessary electric power : 60 kVA
Chariot Jib-Trolley	RCC2	0 → 60 m/m n	7 ch hp	Courant triphasé 380 V - 50 périodes Mains supply 380 V - 3 phases - 50 cycles
Translacion Travelling	RT	25 m/m n	2 x 5 ch hp	Poids de la grue sans lest : 48 t Weight of crane without ballast : 48 t
Le poids de la grue indiqué correspond au cas ① avec flèche et hauteur maxi The weight of the crane is indicated for ① with longest jib and maxi height under hook.				

Modifications réservées
Subject to modification



Potain

R. C. Seine 63 B 4583
Route de Charbonnières - 69130 Ecully
Téléphone (78) 93.81.81 + Téléc 33179
Agences : Paris - Lyon - Marseille - Rennes -
Strasbourg - Toulouse - Nancy
Export : 89, av. du Président Roosevelt - F 94150 Chevilly-Larue
Téléphone (4) 677 67 67 - Téléc 270001

Potain. 744 ds.

Remark: Selfweight 48 Ton

SM (winche) 2 cage

→ maximum load 5000 kg Length = 30 m.

$$\text{Moment} = 5000(30) = 150000 \text{ kg}\cdot\text{m}.$$

SO: Ballast (weight)

$$y = P(L)$$

$$P = \frac{M}{L} = \frac{150000}{16.2} = 9300 \text{ kg}$$

Summary: DSE Live load = 5000 kg
Ballast = 9300 kg

→ maximum length 45 m. Load = 2550 kg

$$\text{moment} = (2550)(45\text{m})$$

$$= 114750 \text{ kg}\cdot\text{m}$$

Summary: SO: Ballast (weight)

$$\text{DSE Live load } 2550 \text{ kg} \quad y = P(L)$$

$$\text{Ballast} = 5100 \text{ kg} \quad P = \frac{M}{L} = \frac{114750}{22.5\text{m}} = 5100 \text{ kg}$$

DM (winche) 1 cage.

→ maximum load 10000 kg Length = 16.1 m.

$$\text{Moment} = (10000)(16.1) = 161000 \text{ kg}\cdot\text{m}.$$

SO: Ballast (weight)

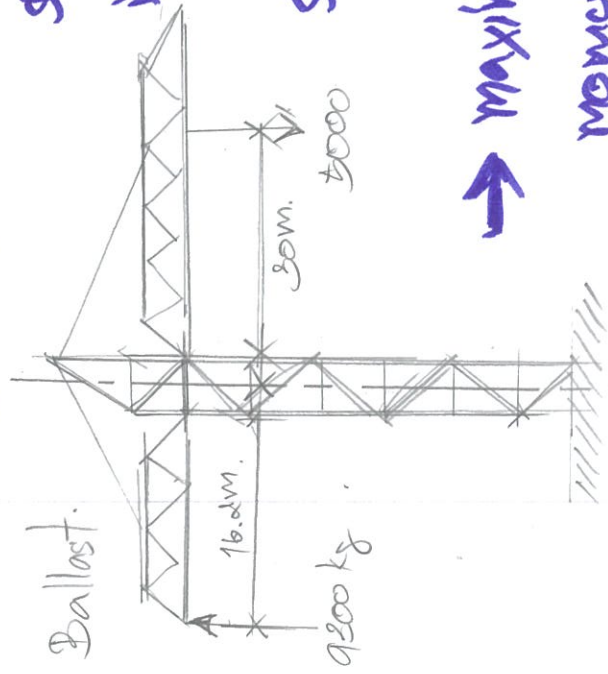
$$P = \frac{M}{L} = \frac{161000}{8.5} = 18900 \text{ kg}$$

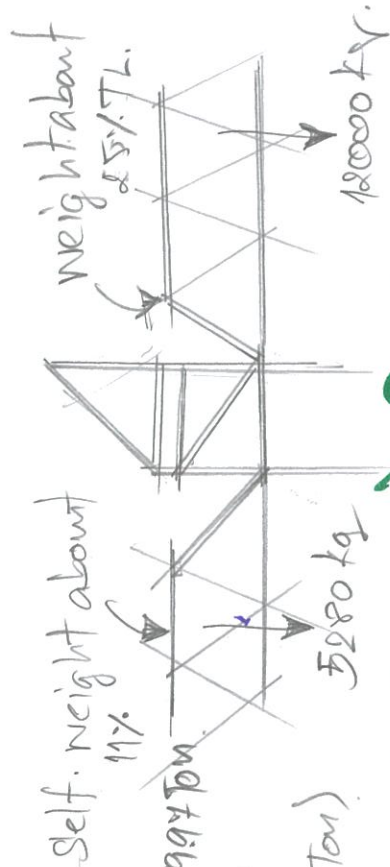
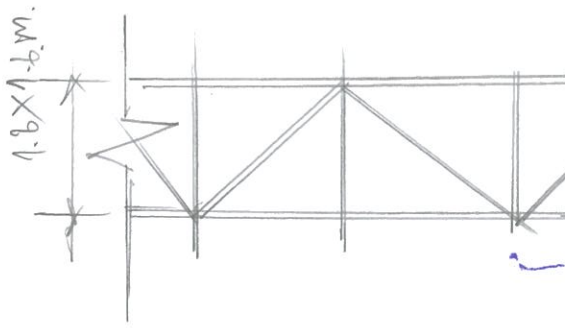
Summary:

$$\text{DSE Live load} = 5000 \text{ kg}$$

$$\text{Ballast} = 18900 \text{ kg}$$

Control.





Weight $\Rightarrow 10000 + 18900 + 48000$
 $\Rightarrow 76900 \text{ kg (76.9 Ton)}$

out of service Yoment (Chunminini 195m)

$$\left. \begin{aligned} Y_{P \text{ Ballast}} &= -18900 (8.5) = -169650 \text{ kg-m} \\ Y_{P \text{ self}} &= -5280 \left(\frac{8.5}{2}\right) = -22440 \text{ kg-m} \\ Y_{P \text{ self}} &= 10000 (8.05) = 96600 \text{ kg-m} \end{aligned} \right\} -26,490 \text{ kg-m}$$

In Service Yoment

$$Y = PL = 10000 (16.1) = 161000 \text{ kg-m} = 16000 - 86490$$

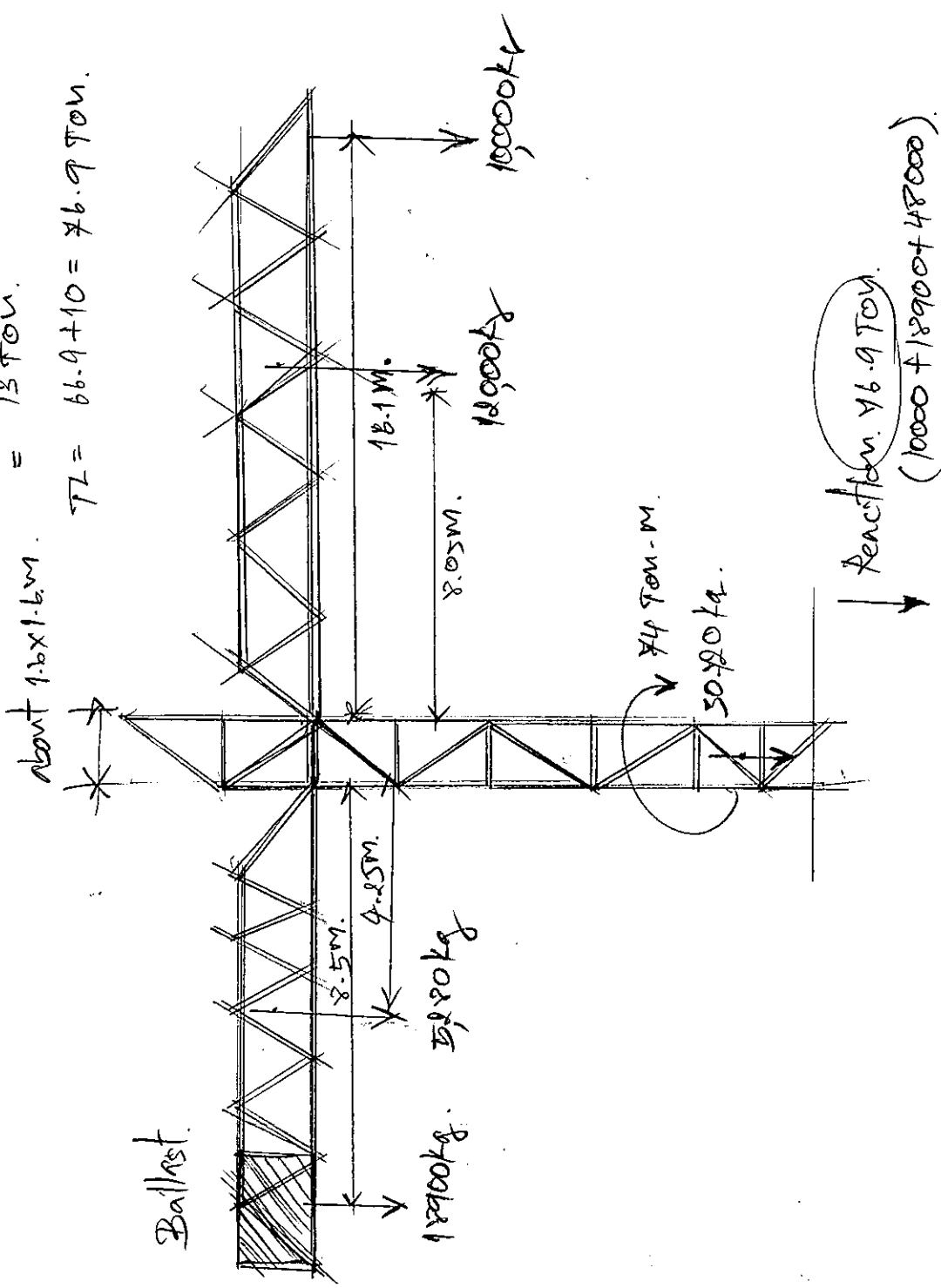
$$\text{Add Impact load } 50\% = 1.3 \times 76.9 \text{ Ton} = 747 \text{ T-m}$$

$$= \underline{\underline{99,977 \text{ Ton (about)}}$$

Return. 74409.

DM (winche) case 1.

$$\begin{aligned}
 DL &= 48 \text{ Ton (self weight)} \\
 &= 18.9 \text{ Ton (Ballast)} \\
 &= 66.9 \text{ Ton.} \\
 LL &= 10 \text{ Ton} \times \text{Impact load } 50\% \\
 &= 13 \text{ Ton.} \\
 TL &= 66.9 + 10 = 76.9 \text{ Ton.}
 \end{aligned}$$



$$\begin{aligned}
 &\downarrow \text{Reaction (Impact load } 50\%) \\
 &13 \times 76.9 = 99.97 \text{ Ton.} \\
 &\uparrow \text{Moment} = 161000 - 26490 \\
 &= 74 \text{ Ton-m.}
 \end{aligned}$$

Summary:
 DSE Reaction (Impact) 99.9 Ton.
 Moment 74 Ton-m. #

ANALYSIS AND DESIGN OF PILE FOOTING (SDM)

Project :	F Square
Building :	TOWER CRANE
By :	Mr. KITTIKUN P.
Location :	TOWER CRANE
Date :	

A. Material Properties

Step 1 Ultimate Compressive Strength (fc') :

Steel Grade (SD-xx or SR-xx) : SR-24

Yield Strength, fy : 2,400

β_1 :

$$\beta_1 = \begin{cases} 0.85 & \text{for } f_y \leq 6120 \\ \frac{6120}{f_y} & \text{for } f_y > 6120 \end{cases}$$

ρ_b :

$$\rho_b = 0.75 \rho_{b, max}$$

ρ_{max} :

0.0197

ρ_{min} :

0.00350

B. Estimate Size of Footing

Step 2 Column Load :

MD

ML

kg.m

DL

LL

kg

Total Load (include assume footing & Soil.) 10-30 % :

SPUN PILE 0.3 x 0.3 x 19.00 m.

No. of Pile Required - No. of Pile Used :

Length

0.30 m.

1.50 m.

4.00 m.

Actual Pile Load

$$P_u = 1.4DL + 1.6LL$$

Step 3 Number of pile Line 1 or A

Resistance from Pile (Shear)

Moment of Footing

$$R_u = \rho_b \cdot f_y \cdot (1 - 0.59 \rho_b) \cdot f_y \cdot l \cdot c'$$

Maximum Thickness Footing (ρ_{min} Control)

$$d = \sqrt{\frac{M_{max}}{\phi_b \cdot R_u \cdot B}}$$

Effective Depth

$$d = \sqrt{\frac{M_{max}}{\phi_b \cdot R_u \cdot B}}$$

Minimum Thickness Footing (ρ_{max} Control)

Effective Depth

Thickness Footing

Use Thickness (Recommended less thane 40 cm. for Pile footing)

Step 4 Punching Shear @ Distance d/2 around Edge of Column

Effective Depth Section

Line Critical of Punching Shear

Dp(Pile Size)

Pile 2B No.

Load Resistanc

Pile 1A, 1C, 3A, 3C No.

Load Resistanc

Pile 1B, 2A, 2C, 3B No.

Load Resistanc

V_p Punching Shear

b_o

$B_c = b/a$

α

Allowable Shear force ; V_c

ΦV_c

Step 5 Beam Shear @ Distance d from Edge of Column

Effective Depth Section

Line Critical of Punching Shear

Dp(Pile Size)

Pile 2A, 2B, 2C No.

Load Resistanc

Pile 1A, 1B, 1C No.

Load Resistanc

Rounded

Deformed

240 ksc

SD-40 ksc

4,000 ksc

0.85

0.0262

0.0197

0.00350

136514 kg.m

99970 kg

129961 kg

56000 kg/pile

4 pile

0.30 m.

1.50 m.

4.00 m.

142558 kg

58392 kg

2 Nos

116784 kg

8758775 kg.cm

13.52 ksc.

42 cm.

63.44 ksc.

20 cm.

20 cm.

42 cm.

130 cm.

121.5 cm.

60.75 cm.

15.0 cm.

-75.75 cm.

0.0 kg

20.15 cm.

233567 kg

14.25 cm.

0 kg

233567 kg

1086.0 cm.

1.0

40.0

2166794 kg

2166794 kg

1841775 kg

OK

d

121.5 cm.

d

121.5 cm.

Dp/2

15.0 cm.

X

-196.5 cm.

ϕ_1

0.0 kg

X

-46.5 cm.

ϕ_1

-122623 kg

ANALYSIS AND DESIGN OF PILE FOOTING (SDM)

Project : **F Square**
Building : **TOWER CRANE**
By : **Mr. KITTIKUN P.**

Footing No. :

Location :

Date :

V_b Beam Shear : $V_b = \sum q_l$: V_b -122623 kg
 Allowable Shear force ; V_c : $V_c = 0.53 \sqrt{f_c} \cdot B \cdot d$: V_c 399041 kg
 ΦV_c : ΦV_c 339185 kg OK

Step 6 Check Capacity of Pile

P (DL+LL) $q = \frac{P + W_f + W_p + W_x}{N_p}$

$W_{footing}$: H 0.8 m
 $W_{pedestal}$: Y 1690 kg/m3
 W_{soil} : $q = \frac{P + W_f + W_p + W_x + M d_{x_2}}{N_p} + \sum d_{x_2}^2 \leq q_u$
 Load Resistanc of pile

D. Determine Reinforcement

Step 7 R_u : $R_u = \frac{M_u}{\phi b d^2}$: R_u 1.65 ksc
 ρ : $\rho = \frac{0.85 f_c'}{f_y} \left[1 - \sqrt{1 - \frac{2 R_u}{0.85 f_c'}} \right]$: ρ 0.00041
 Main Steel (Long Side), A_{sL} : $A_s = 1.33 \phi b d$: A_{sL} 26.74 sq.cm.
 Temp Steel (Short Side), A_{sS} : $(0.0020 \text{ or } 0.0018) b t$: A_{sS} 93.60 sq.cm.

Steel Rebar	As,req cm ²	DB12		DB16		DB20		DB25		DB28		DB32	
		No.	As	No.	As	No.	As	No.	As	No.	As	No.	As
Main Steel, A_{sL}	26.74	24	27.12	14	28.14	9	28.26	6	29.46	5	30.75	4	32.2
Temp Steel, A_{sS}	93.60	83	93.79	47	94.47	30	94.2	20	98.2	16	98.4	12	96.5
l_{db} (Theory)	$l_{db} = 0.06 A_s \sqrt{\frac{f_c}{f_y}}$	14		31		49		76		95		125	
l_{db} (Actually)	$l_{db} = \frac{L}{2} - \frac{a}{2} - 0.075$	118		117.5		118		118		118		118	
Status		OK		OK		OK		OK		OK		Reduce.Rebar	

Dowel bar at Case 2 A_j 900 sq.cm.
 $A_{s,req} = 0.005 A_j = 4.5$ sq.cm. Used Db 25 A_s /pcs 6.16 sq.cm.
 no. 8 $A_{s,use}$ 49.28 sq.cm. OK
 $l_{db} = 20.00$ cm. $l_{brace} = 70$ cm. $l_c = 30$ cm. $l_{total} = 120.00$ cm.