

รายการคำนวณโครงสร้าง

อาคารพักอาศัยคนงาน 4 ชั้น

บริษัท ภูเก็ตเวิร์ค ครีเอชั่น จำกัด

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วิศวกรโครงสร้าง

นายประสาน จิ่งสงวนพรสุข สย. 5499

DESIGN NOTES

Design Code of Practice

E.I.T. Standard 1007-34 (Working Stress Design)
AISC ; Manual of Steel Construction Allowable Stress Design

Properties of Materials

Concrete :

fc'	Ultimate compressive strength	:	173	173 ksc
Factor		:	0.375	0.375
fc	= Factor x fc'	:	65	65 ksc
Ec	= $4,270w^{1.5} \text{ Sqrt}[fc]$:	2.1E+05	2.1E+05 ksc

Reinforcement :

	Steel Grade	:	Rounded	Deformed
fy	Yield strength	:	SR-24	SD-40
fs	Allowable strength	:	2,400	4,000 ksc
Es	Modulus of elasticity	:	1,200	1,700 ksc
		:	2.04E+06	2.04E+06 ksc

Steel Structure :

fy	Yield strength	:		2,400 ksc
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PC Pile :

Squ. 0.22 x 0.22 x 8.00 m. Safe Load	:		12 ton
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Design Parameter

n	= Es/Ec		10	10
k	= $1/[1+fs/(n*fc)]$		0.346	0.272
j	= $1 - k/3$		0.885	0.909
R	= $fc * j * k/2$		9.92	8.01 ksc
vc	Beam Shear	= $0.29 * \text{Sqrt}(fc')$		3.81 ksc
vp	Punching Shear	= $0.53 * \text{Sqrt}(fc')$		6.97 ksc

Design Loading

Dead Load :

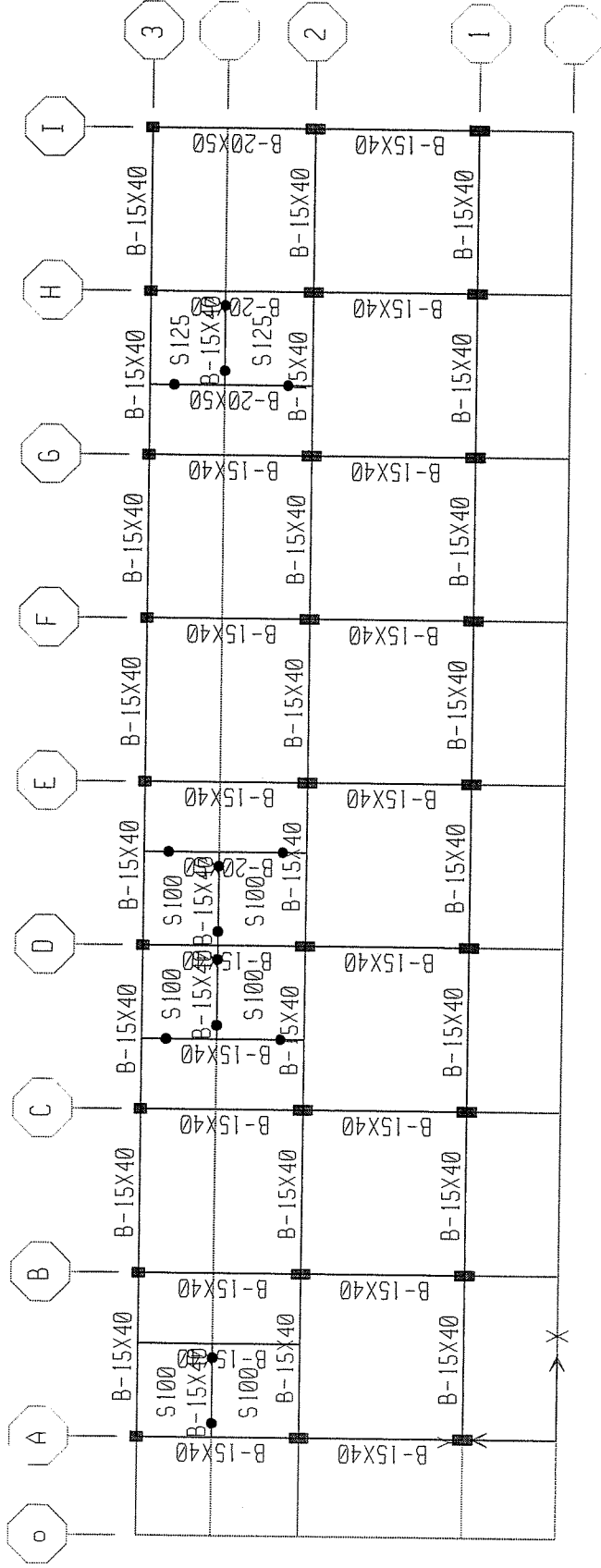
Steel	:	7,850 Kg/m ³
Concrete	:	2,400 Kg/m ³
Compact Sand	:	2,000 Kg/m ³
Water	:	1,000 Kg/m ³
Block partition	:	120 Kg/m ³
Roof Sheet	:	15 Kg/m ²

Live Load :

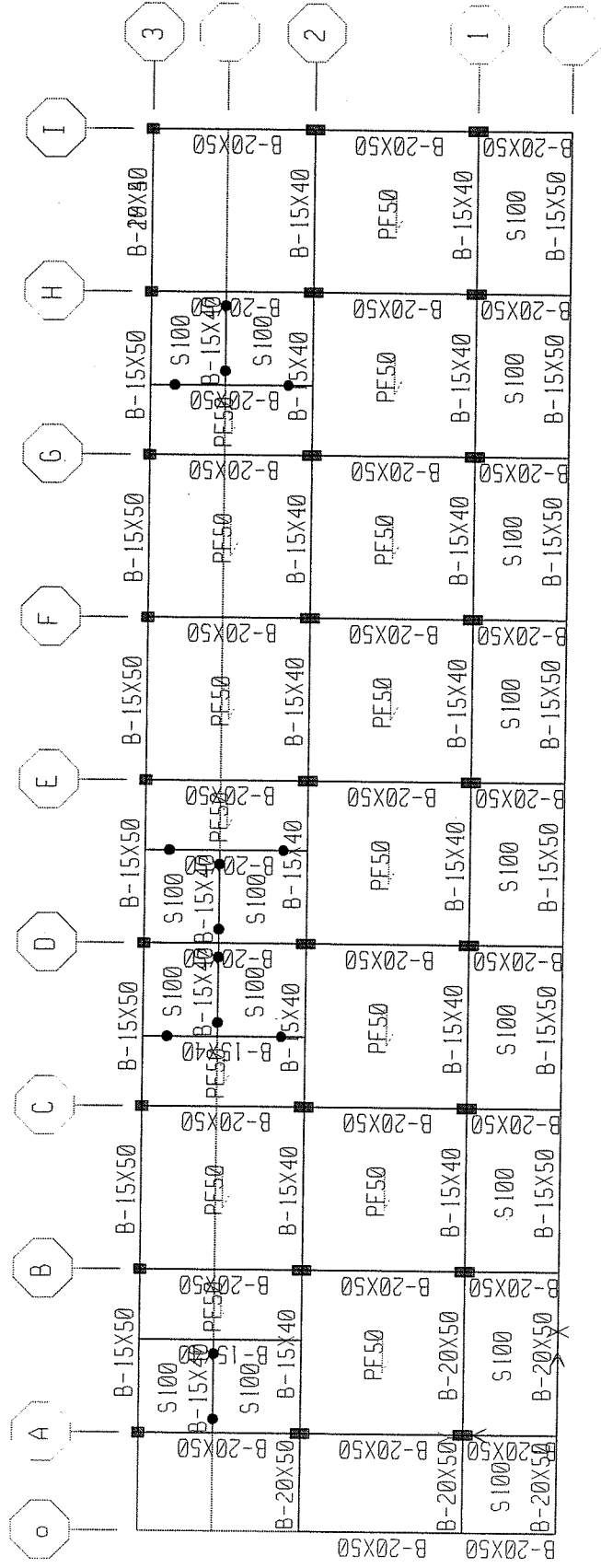
LL	:	150 Kg/m ²
Roof	:	50 Kg/m ²

Wind Load :

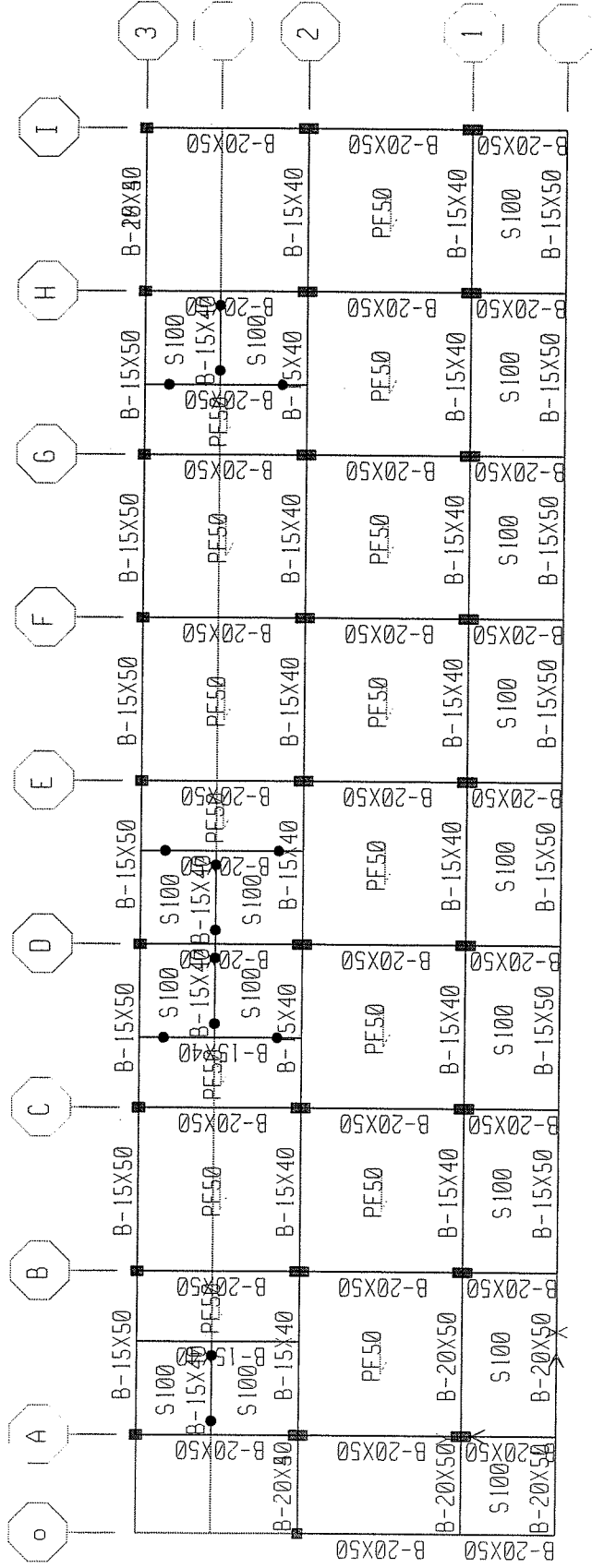
:	50 Kg/m ²	(H < 10 m.)
:	80 Kg/m ²	(10 < H < 20 m.)

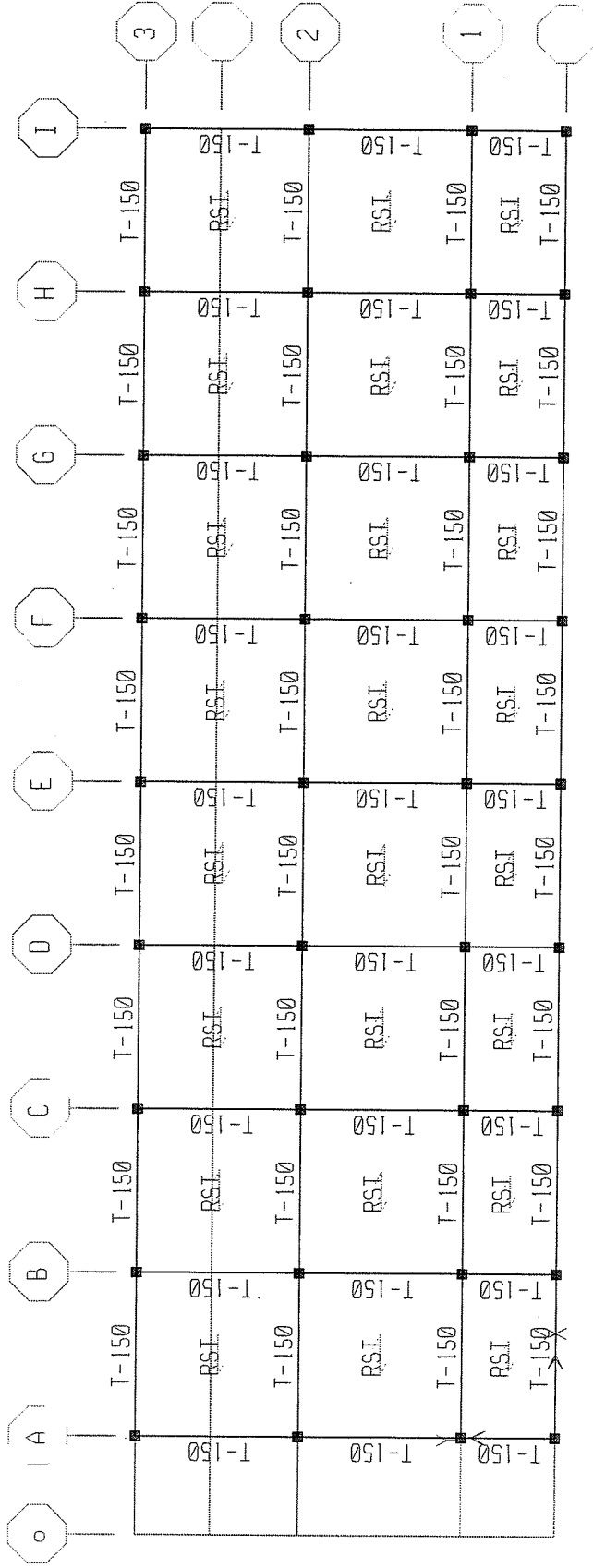


GROUND FL PLAN

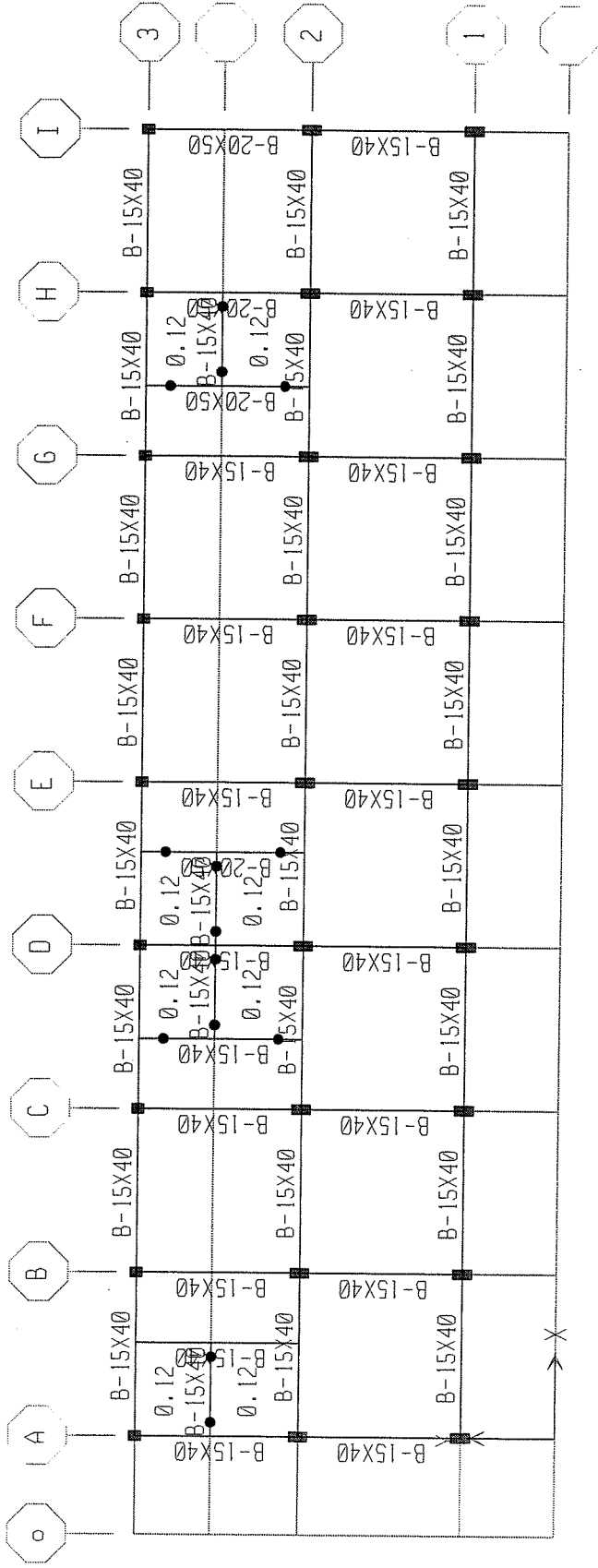


Handwritten: 2nd FL PLAN

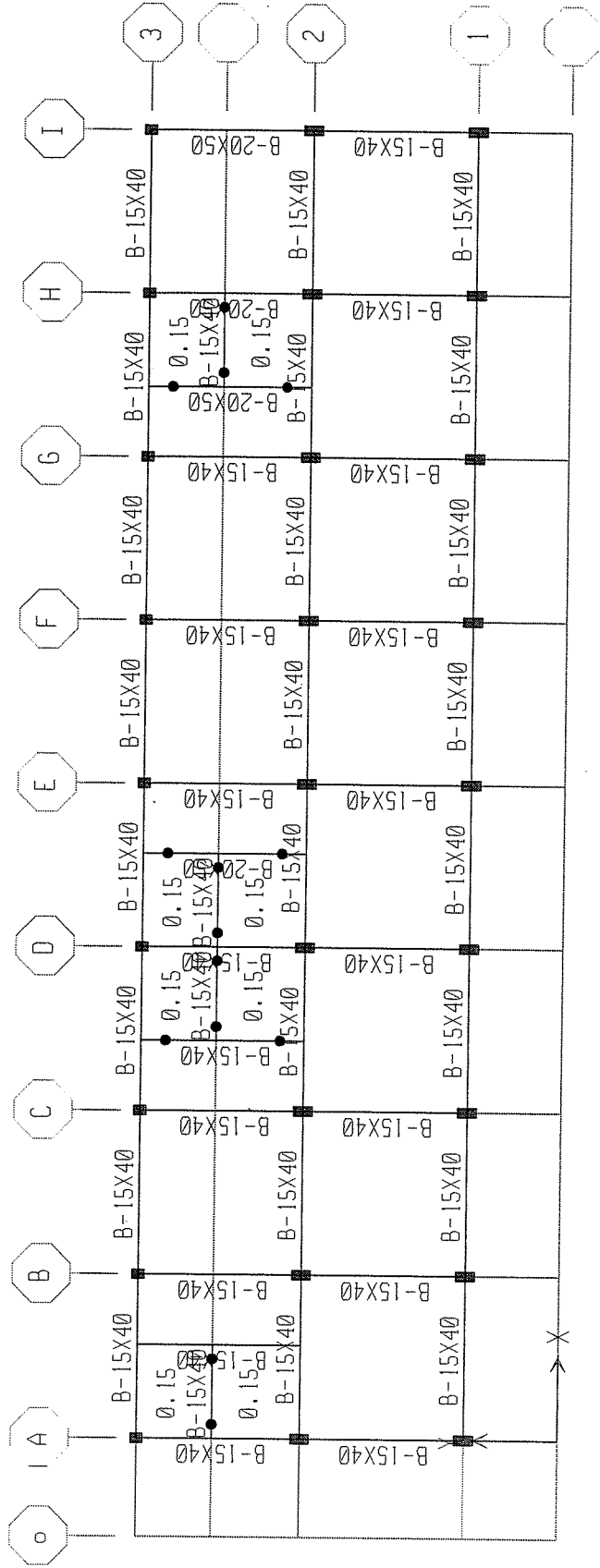




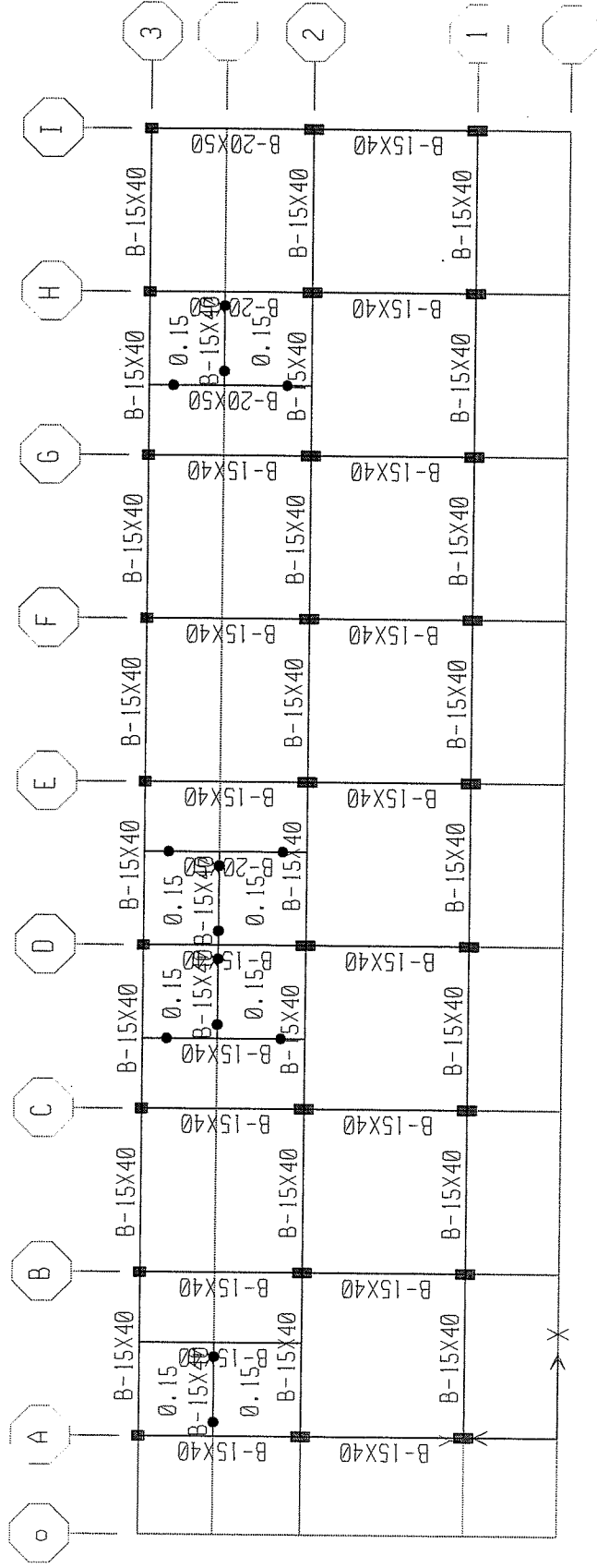
Roof PLAN

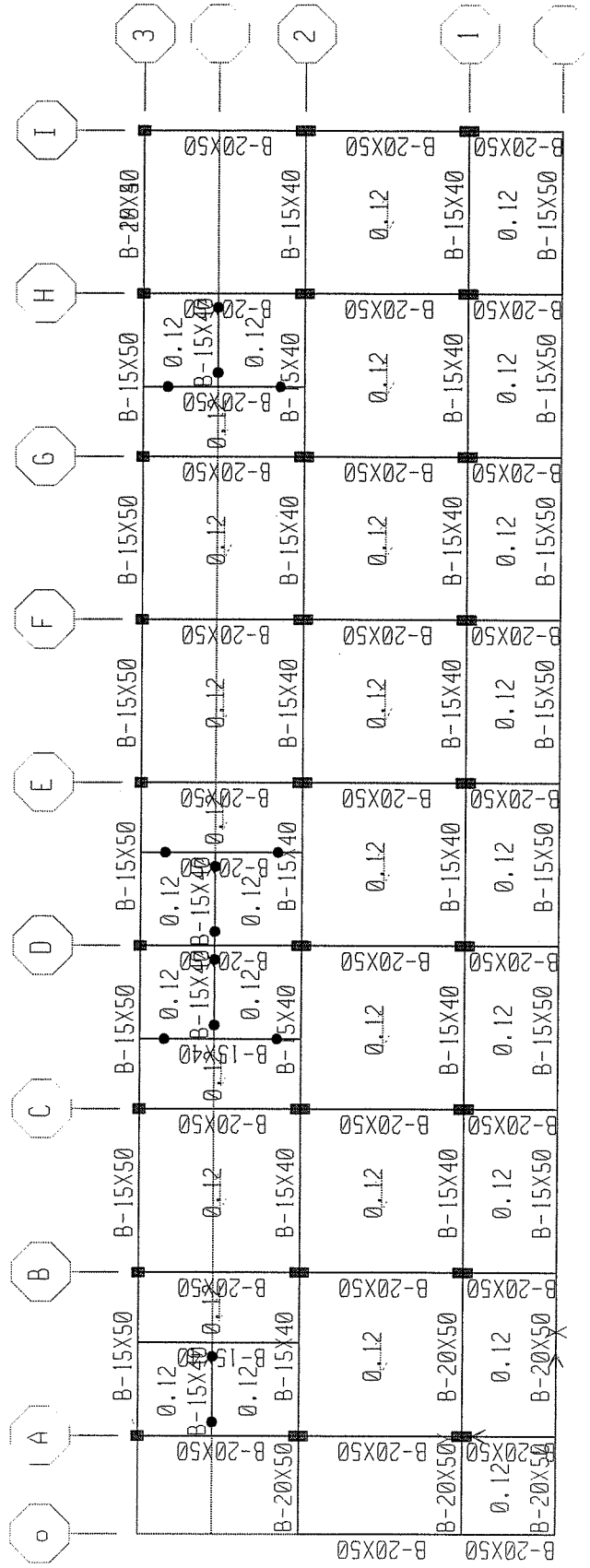


GROUND FL PLAN
 < Super Imposed DL

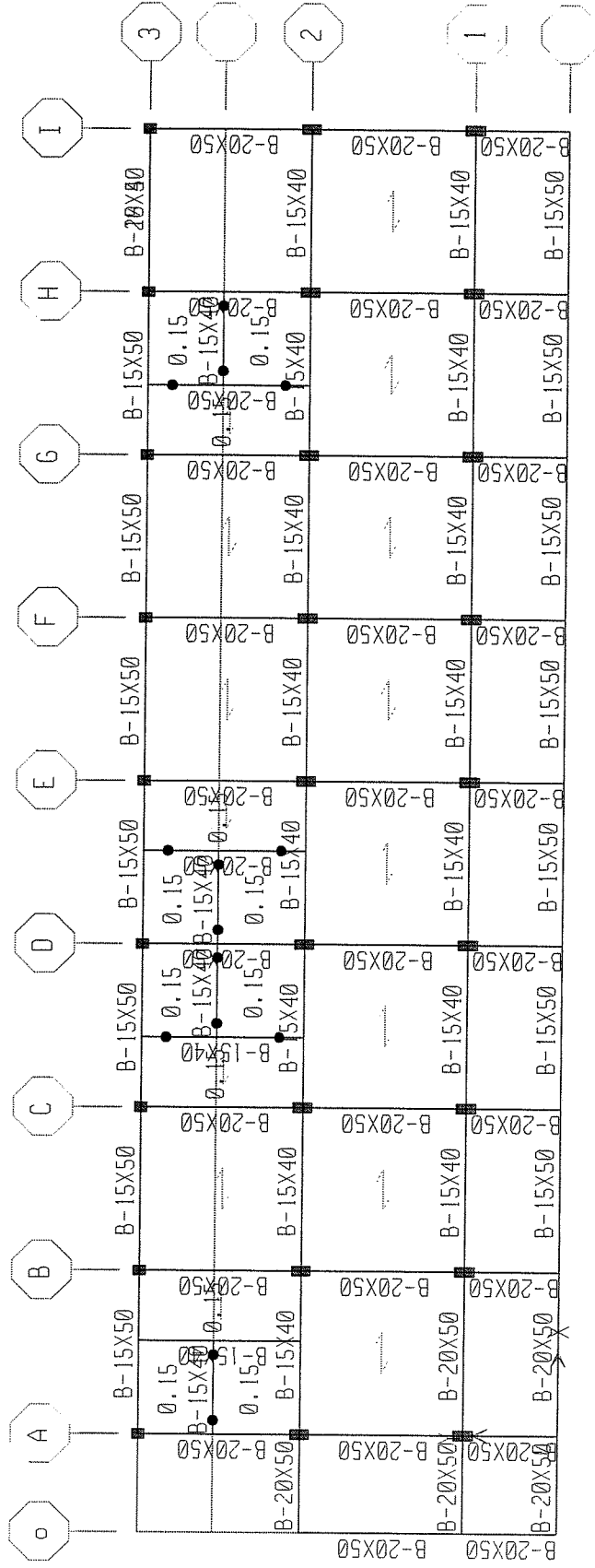


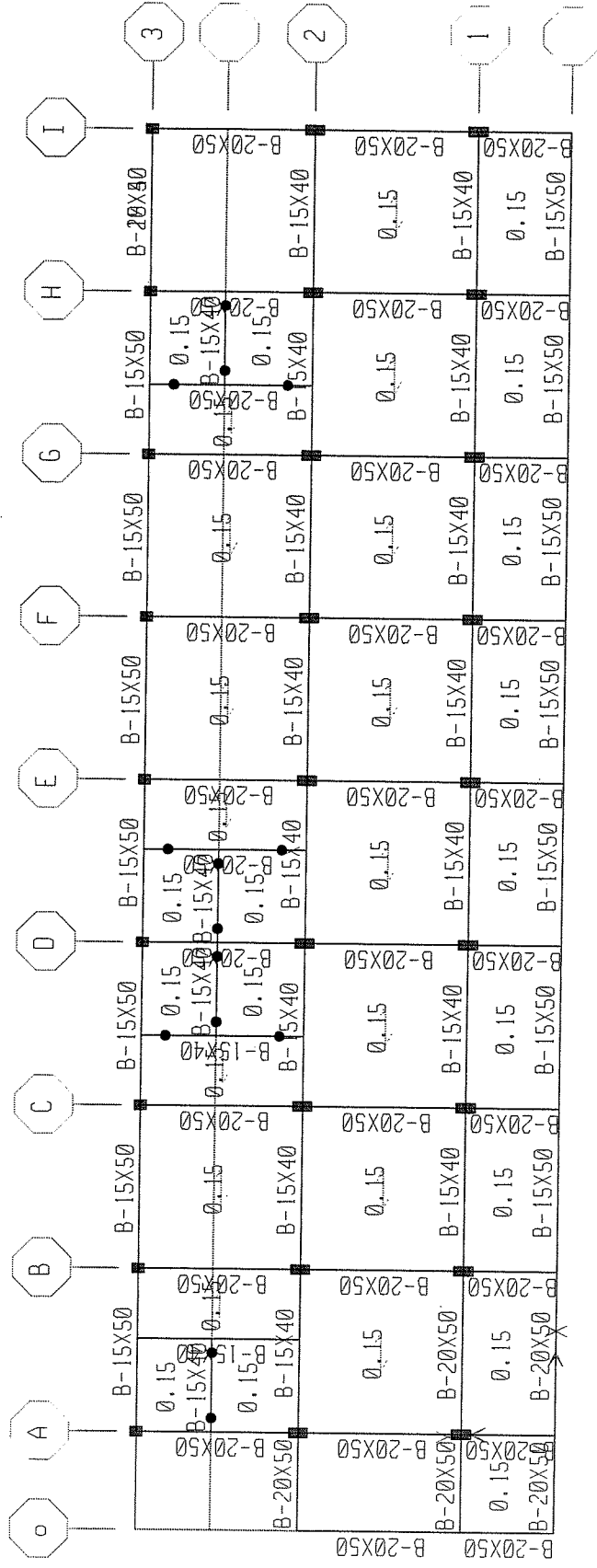
GROUND FL PLAN
(Partition load)



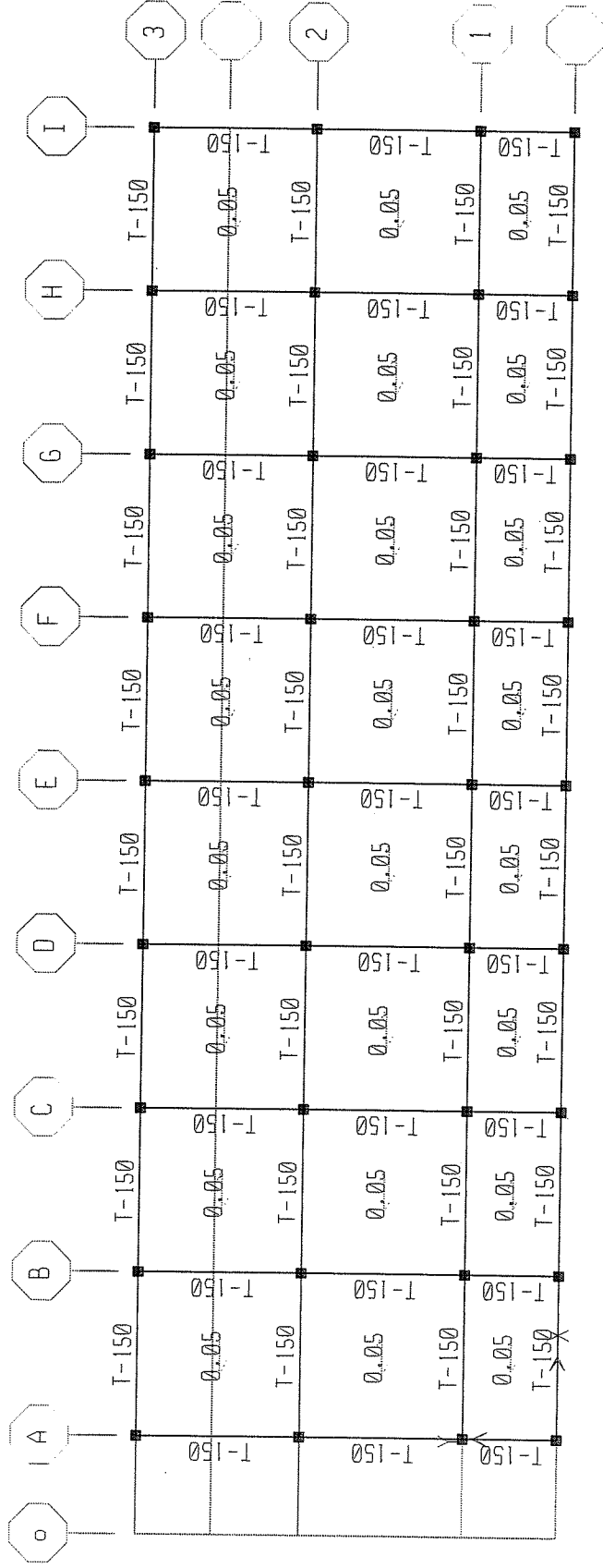


2nd Fl
 2-4 FL PLAN
 (Superimpose DL)





2nd fl
g-4 FL
CLL



Roof PLAN
(LL)

	A	B	C	D	E	F	G	H	I	
3	15 ⁵⁸	22 ⁶⁰	20 ⁶¹	37 ⁶⁹	22 ⁶⁵	18 ⁶⁶	23 ⁶⁷	33 ⁷⁰	20 ⁷⁰	
	38	37	37	49	38	33	39	54	33	
2	69	40	41	43	45 +202	46	47	49	50	
1	13	51	54	54	54	54	54	59	43	
		14	15	16	17	18	19	20	21	

Handwritten annotations: C4* (near A14), C2 (near D45), C3 (near H20), C3 (near H21).

Reaction Plan

Job Title : อาคารพักอาศัย 4 ชั้น	Subject : Reaction F01	
Designed : PSJ	Date : Feb-12	Sheet : Page :
Checked :	Date : Feb-12	

Pile Capacity = 12 ton

Story	Point	Load	FX [ton]	FY [ton]	FZ [ton]	MX [ton.m]	MY [ton.m]	MZ [ton.m]	No. of Piles-Req.	Provide Piles	R
BASE	13	S2DL	0.29	0.22	68.92	-0.14	0.14	0.00	5.74	6	0.96
BASE	14	S2DL	-0.12	0.22	50.58	-0.13	-0.06	0.00	4.22	5	0.84
BASE	15	S2DL	0.02	0.20	53.44	-0.12	0.01	0.00	4.45	5	0.89
BASE	16	S2DL	-0.02	0.12	53.71	-0.07	-0.01	0.00	4.48	5	0.90
BASE	17	S2DL	-0.03	0.21	53.70	-0.11	-0.01	0.00	4.48	5	0.90
BASE	18	S2DL	-0.02	0.19	53.18	-0.09	-0.01	0.00	4.43	5	0.89
BASE	19	S2DL	-0.01	0.21	53.85	-0.09	-0.01	0.00	4.49	5	0.90
BASE	20	S2DL	0.03	0.37	58.60	-0.16	0.01	0.00	4.88	5	0.98
BASE	21	S2DL	-0.25	0.32	42.34	-0.13	-0.13	0.00	3.53	4	0.88
BASE	38	S2DL	0.64	0.13	37.39	-0.10	0.31	0.00	3.12	4	0.78
BASE	40	S2DL	-0.37	-0.11	36.88	0.01	-0.18	0.00	3.07	4	0.77
BASE	41	S2DL	0.24	-0.14	36.68	0.04	0.12	0.00	3.06	4	0.76
BASE	43	S2DL	-0.01	0.72	48.11	-0.34	0.00	0.00	4.01	5	0.80
BASE	45	S2DL	-0.24	-0.18	37.67	0.07	-0.12	0.00	3.14	4	0.78
BASE	46	S2DL	-0.02	-0.27	32.50	0.11	-0.01	0.00	2.71	3	0.90
BASE	47	S2DL	0.25	-0.19	38.65	0.09	0.12	0.00	3.22	4	0.81
BASE	49	S2DL	0.05	0.26	53.93	-0.11	0.03	0.00	4.49	5	0.90
BASE	50	S2DL	-0.61	-0.13	32.58	0.07	-0.30	0.00	2.72	3	0.91
BASE	58	S2DL	0.47	-0.35	14.73	0.16	0.23	0.00	1.23	2	0.61
BASE	60	S2DL	-0.26	-0.12	21.35	0.05	-0.13	0.00	1.78	2	0.89
BASE	61	S2DL	0.20	-0.12	19.87	0.05	0.10	0.00	1.66	2	0.83
BASE	63	S2DL	0.00	-0.61	30.23	0.29	0.00	0.00	2.52	3	0.84
BASE	65	S2DL	-0.18	-0.11	21.23	0.05	-0.09	0.00	1.77	2	0.88
BASE	66	S2DL	-0.01	-0.11	15.60	0.05	0.00	0.00	1.30	2	0.65
BASE	67	S2DL	0.25	-0.12	23.22	0.06	0.12	0.00	1.94	2	0.97
BASE	69	S2DL	-0.24	-0.47	32.60	0.23	-0.11	0.00	2.72	3	0.91
BASE	70	S2DL	-0.05	-0.14	19.53	0.00	0.00	0.00	1.63	2	0.81

FOOTING ULTIMATE DESIGN
Number of Pile 3

FOOTING ULTIMATE DESIGN
Number of Pile 3

F3

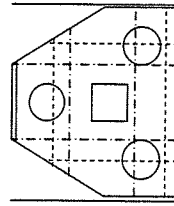
Design Data

Column Data	X-Dimension	Y-Dimension	Safe Load	Edge Distance	Thickness	Covering	m.	m.	m.	m.	m.	m.	Asc.
Concrete	0.20	0.20	12	0.20	0.50	0.08	173	4000	34	0	0	0	1.50
Steel													
Service Load													
Weight of Footing													
Average Load Factor													

Pile Coordinate and Loading

Pile No.	X-Coordinate			Y-Coordinate			Pile Service Loading					
	Original	Deviate	SQRT.	Original	Deviate	SQRT.	P	F	Mx	My	Total	
1	-0.30	0.09	0.31	-0.17	0.03	0.18	11	0	0	0	12	
2	0.30	0.09	0.31	-0.17	0.03	0.18	11	0	0	0	12	
3	0.00	0.00	0.00	0.35	0.12	0.37	11	0	0	0	12	
							0.18	34	1	0	0	35
							0.00	0.00	0.00	0.00	0.00	0.00

Corner	X	Y	Corner	X	Y
1	-0.1	-0.1	1	-0.50	-0.37
2	0.1	-0.1	2	0.50	-0.37
3	0.1	0.1	3	0.50	0.37
4	-0.1	0.1	4	0.50	0.03
			5	0.20	0.55
			6	-0.20	0.55
			7	-0.50	0.03
			8	-0.50	-0.37



Critical Section Line Coordinate

Beam Shear	X1	Y1	X2	Y2	Length	Deep Beam	X1	Y1	X2	Y2	Length
X-Negative	-0.52	-0.37	-0.52	0.55	0.92	X-Negative	-0.20	-0.37	-0.20	0.20	0.55
X-Positive	0.52	-0.37	0.52	0.55	0.92	X-Positive	0.20	-0.37	0.20	0.20	0.55
Y-Negative	-0.50	-0.52	0.50	-0.52	1.00	Y-Negative	-0.50	-0.14	0.50	-0.14	1.00
Y-Positive	-0.22	0.52	0.22	0.52	0.43	Y-Positive	-0.39	0.22	0.39	0.22	0.77
Punching	X1	Y1	X2	Y2	Length	Moment	X1	Y1	X2	Y2	Length
X-Negative	-0.31	-0.37	-0.31	0.36	0.73	X-Negative	-0.10	-0.37	-0.10	0.55	0.92
X-Positive	0.31	-0.37	0.31	0.36	0.73	X-Positive	0.10	-0.37	0.10	0.55	0.92
Y-Negative	-0.50	-0.31	0.50	-0.31	1.00	Y-Negative	-0.50	-0.10	0.50	-0.10	1.00
Y-Positive	-0.34	0.31	0.34	0.31	0.67	Y-Positive	-0.46	0.10	0.46	0.10	0.92

Ultimate Shear and Shear Stress at Critical Section

Pile No.	Beam Shear			Deep Beam Shear			Punching Shear				
	X-Neg	X-Pos	Y-Neg	X-Neg	X-Pos	Y-Neg	X-Neg	X-Pos	Y-Neg	Y-Pos	Perf
1	0	0	0	0	17	0	0	8	0	0	8
2	0	0	0	0	17	12	0	0	8	0	0
3	0	0	0	0	0	0	17	0	0	0	12
Shear											
0 0 0 0 17 17 24 17 6 6 0 12 28											
Moment											
2.50 2.50 2.50 2.50 2.50 2.50											
Length											
0.92 1.00 0.43 0.92 0.92 1.00 0.77 0.73 0.73 1.00 0.67 2.48											
Depth											
0.42 0.42 0.42 0.42 0.42 0.42 0.42 0.42 0.42 0.42 0.42 0.42											
Stress											
0.00 0.00 0.00 0.00 4.52 4.52 5.68 5.37 2.57 2.57 0.00 4.22 2.65											
Allow											
5.93 14.61 14.61 14.91 14.87 11.95											

Ultimate Moment and Reinforcement at Critical Section

Pile Number	X-Negative			X-Positive			Y-Negative			Y-Positive		
	a	V	M	a	V	M	a	V	M	a	V	M
1	0.20	17	3	-0.40	0	0	0.07	17	1	0.27	0	0
2	-0.40	0	0	0.20	17	3	0.07	17	1	-0.27	0	0
3	-0.10	0	0	-0.10	0	0	-0.45	0	0	0.25	17	4
Moment												
0.92 0.92 3 3 3 3 1.00 0.42 0.42												
Length												
0.42 0.42 2.3 2.3 1.7 1.7 14.7 13.5 12.5 12.5 73 66												
As(Req)												
13.5 13.5 11.5 11.5 67 67 11.5 11.5 11.44 11.44												
MinAs(Beam)												
13.5 13.5 11.5 11.5 67 67 11.5 11.5 11.44 11.44												
MinAs(Stab)												
13.5 13.5 11.5 11.5 67 67 11.5 11.5 11.44 11.44												
Conc. Moment												
13.5 13.5 11.5 11.5 67 67 11.5 11.5 11.44 11.44												

FOOTING ULTIMATE DESIGN
Number of Pile 4

FOOTING ULTIMATE DESIGN
Number of Pile 4

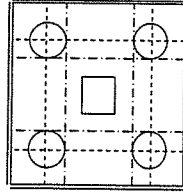
F4

F4

Design Data		Material Data		Concrete		Steel	
X-Dimension	0.20	m.	4000	asc.	173	asc.	
Y-Dimension	0.20	m.	4000	asc.	46	t.	
Safe Load	12	t.	Mx		0	f-m.	
Edge Distance	0.20	m.	My		0	t-m.	
Thickness	0.50	m.	Weight of Footing		1	t.	
Covering	0.08	m.	Average Load Factor		1.50		

Pile No.	X-Coordinate		Y-Coordinate		Pile Service Loading				
	Original	Deviate	Existing	SQRT.	P	F	Mx	My	Total
1	-0.30	0.09	-0.30	0.09	12	0	0	0	12
2	0.30	0.09	-0.30	0.09	12	0	0	0	12
3	0.30	0.09	0.30	0.09	12	0	0	0	12
4	-0.30	0.09	0.30	0.09	12	0	0	0	12
Total	0.00	0.00	0.00	0.00	48	0	0	0	48

Column Coordinate		Footing Coordinate			
Corner	X	Y	Corner	X	Y
1	-0.1	-0.1	1	-0.50	-0.50
2	0.1	-0.1	2	0.50	-0.50
3	0.1	0.1	3	0.50	0.50
4	-0.1	0.1	4	-0.50	0.50
			5	0.50	0.50
			6	-0.50	0.50
			7	-0.50	0.50
			8	0.50	-0.50



Ultimate Shear and Shear Stress at Critical Section

Pile No.	Beam Shear				Deep Beam Shear				Punching Shear			
	X-Neg	X-Pos	Y-Neg	Y-Pos	X-Neg	X-Pos	Y-Neg	Y-Pos	X-Neg	X-Pos	Y-Neg	Y-Pos
1	0	0	0	0	18	0	18	0	0	8	0	8
2	0	0	0	0	18	0	18	0	0	8	0	8
3	0	0	0	0	18	0	18	0	0	8	0	8
4	0	0	0	0	18	0	18	0	0	8	0	8
Shear	0	0	0	0	35	35	35	35	16	16	16	16
Moment					4	4	4	4				
Factor					2.50	2.50	2.50	2.50				
Length	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Depth	0.42	0.42	0.42	0.42	0.42	0.42	0.42	0.42	0.42	0.42	0.42	0.42
Stress	0.00	0.00	0.00	0.00	6.43	6.43	6.43	6.43	3.79	3.79	3.79	3.79
Allow.					14.61	14.61	14.61	14.61				

Ultimate Moment and Reinforcement at Critical Section

Pile Number	X-Negative				X-Positive				Y-Negative				Y-Positive			
	a	V	M	a	V	M	a	V	M	a	V	M	a	V	M	
1	0.20	18	4	-0.40	0	0	0.20	18	4	0.40	0	0	0.20	18	4	
2	-0.40	0	0	0.20	18	4	0.20	18	4	-0.40	0	0	-0.40	0	0	
3	-0.40	0	0	0.20	18	4	-0.40	0	0	0.20	18	4	0.20	18	4	
4	0.20	18	4	-0.40	0	0	-0.40	0	0	-0.40	0	0	0.20	18	4	
Moment							7						7			
Length							1.00						1.00			
Depth							0.42						0.42			
As(Req)							4.8						4.8			
MinAs(Beam)							14.7						14.7			
MinAs(Slab)							12.5						12.5			
Conc. Moment							73						73			

Critical Section Line Coordinate

Beam/Shear	X1		Y1		X2		Y2		Length		
	X1	Y1	X2	Y2	X1	Y1	X2	Y2			
X-Negative	-0.52	-0.50	-0.52	0.50	1.00	X-Negative	-0.20	-0.50	0.50	1.00	
X-Positive	0.52	-0.50	0.52	0.50	1.00	X-Positive	-0.20	-0.50	0.50	1.00	
Y-Negative	-0.50	-0.52	0.50	-0.52	1.00	Y-Negative	-0.50	-0.20	0.50	-0.20	1.00
Y-Positive	-0.50	0.52	0.50	0.52	1.00	Y-Positive	-0.50	0.20	0.50	0.20	1.00
Punching	X1	Y1	X2	Y2	Length	Moment	X1	Y1	X2	Y2	Length
X-Negative	-0.31	-0.50	-0.31	0.50	1.00	X-Negative	-0.10	-0.50	-0.10	0.50	1.00
X-Positive	0.31	-0.50	0.31	0.50	1.00	X-Positive	0.10	-0.50	0.10	0.50	1.00
Y-Negative	-0.50	-0.31	-0.50	-0.31	1.00	Y-Negative	-0.50	-0.10	0.50	-0.10	1.00
Y-Positive	-0.50	0.31	-0.50	0.31	1.00	Y-Positive	-0.50	0.10	0.50	0.10	1.00

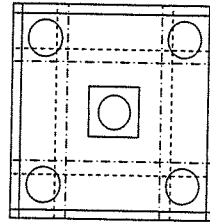
FOOTING ULTIMATE DESIGN
Number of Pile 5

FOOTING ULTIMATE DESIGN
Number of Pile 5

Column Data	X-Dimension	0.20	m.	Material Data	Concrete	173	ksc.
Y-Dimension	0.30	m. <td>Steel</td> <td>4000</td> <td>ksc.</td> <td></td> <td></td>	Steel	4000	ksc.		
Dimension	0.20	m. <td>Service Load</td> <td>56</td> <td>t.</td> <td></td> <td></td>	Service Load	56	t.		
Safe Load	12	t.	Mk	0	t-m.		
Edge Distance	0.20	m. <td>My</td> <td>0</td> <td>t-m.</td> <td></td> <td></td>	My	0	t-m.		
Thickness	0.50	m. <td>Weight of Footing</td> <td>2</td> <td>t.</td> <td></td> <td></td>	Weight of Footing	2	t.		
Covering	0.08	m. <td>Average Load Factor</td> <td>1.50</td> <td></td> <td></td> <td></td>	Average Load Factor	1.50			

Pile No.	X-Coordinate		Y-Coordinate		Pile Service Loading				
	Original	Deviate	Existing	SQRT.	P	F	Mx	My	Total
1	-0.42	0.18	-0.42	0.18	11	0	0	0	12
2	0.42	0.18	-0.42	0.18	11	0	0	0	12
3	0.00	0.00	0.00	0.00	11	0	0	0	12
4	-0.42	0.18	0.42	0.18	11	0	0	0	12
5	0.42	0.18	0.42	0.18	11	0	0	0	12
Eq.	0.00	0.00	0.00	0.00	0.72	56	2	0	58
Total									

Column Coordinate	X	Y	Corner	X	Y
1	-0.1	-0.15	1	-0.62	-0.62
2	0.1	-0.15	2	0.62	-0.62
3	0.1	0.15	3	0.62	0.62
4	-0.1	0.15	4	-0.62	0.62
5			5	0.62	0.62
6			6	-0.62	0.62
7			7	-0.62	0.62
8			8	-0.62	-0.62



Beam Shear	X1	Y1	X2	Y2	Length	Y2	Length
X-Negative	-0.52	-0.62	0.62	-0.29	-0.62	-0.29	0.62
X-Positive	0.52	-0.62	0.52	0.62	1.25	0.62	1.25
Y-Negative	-0.62	-0.57	0.62	-0.57	1.25	-0.29	1.25
Y-Positive	-0.62	0.57	0.62	0.57	1.25	0.62	1.25
Punching	X1	Y1	X2	Y2	Length <td>Y2</td> <td>Length</td>	Y2	Length
X-Negative	-0.31	-0.62	-0.31	0.62	1.25	-0.10	0.62
X-Positive	0.31	-0.62	0.31	0.62	1.25	0.10	0.62
Y-Negative	-0.62	-0.36	0.62	-0.36	1.25	-0.62	0.15
Y-Positive	-0.62	0.36	0.62	0.36	1.25	0.62	0.15

Ultimate Shear and Shear Stress at Critical Section

Pile No.	Beam Shear			Deep Beam Shear			Punching Shear					
	X-Neg	X-Pos	Y-Neg	Y-Pos	X-Neg	X-Pos	Y-Neg	Y-Pos	X-Neg	X-Pos	Y-Neg	Y-Pos
1	0	0	0	0	17	0	17	0	17	0	14	0
2	0	0	0	0	17	17	0	17	0	17	14	0
3	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	17	0	17	0	17	0	14	17
5	0	0	0	0	17	0	17	0	17	0	14	17
Shear	1	1	0	0	35	35	35	35	35	29	29	69
Moment					5	5	5	5	5			
Factor					2.50	2.50	2.50	2.50	2.50			
Length	1.25	1.25	1.25	1.25	1.25	1.25	1.25	1.25	1.25	1.25	1.25	2.68
Depth	0.42	0.42	0.42	0.42	0.42	0.42	0.42	0.42	0.42	0.42	0.42	0.42
Stress	0.14	0.14	0.00	0.00	6.62	6.62	6.62	6.62	6.62	6.62	5.44	5.17
Allow					5.93	14.61	14.61	14.61	14.61	11.85		

Ultimate Moment and Reinforcement at Critical Section

Pile Number	X-Negative			X-Positive			Y-Negative			Y-Positive		
	a	V	M	a	V	M	a	V	M	a	V	M
1	0.32	17	6	-0.52	0	0	0.27	17	5	-0.57	0	0
2	-0.52	0	0	0.32	17	6	0.27	17	5	-0.57	0	0
3	-0.10	0	0	-0.10	0	0	-0.15	0	0	-0.15	0	0
4	0.32	17	6	-0.52	0	0	-0.57	0	0	0.27	17	5
5	-0.52	0	0	0.32	17	6	-0.57	0	0	0.27	17	5
Moment												
Length							1.25			1.25		
Depth							0.42			0.42		
As (Req.)							7.6			7.6		6.4
MinAs (Beam)							18.4			18.4		18.4
MinAs (Slab)							15.61			15.61		15.61
Conc. Moment							91			91		91

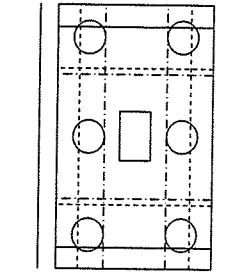
FOOTING ULTIMATE DESIGN
Number of Pile 6

Design Data		Material Data		Concrete	
X-Dimension	0.30 m.	Steel	173 ksc.	Concrete	4000 ksc.
Y-Dimension	0.20 m.	Service Load	68 t.		
Safe Load	12 t.	Weight of Footing	2 t.		
Edge Distance	0.20 m.	Average Load Factor	1.50		
Thickness	0.60 m.				
Covering	0.08 m.				

FOOTING ULTIMATE DESIGN
Number of Pile 6

Pile No.	X-Coordinate		Y-Coordinate		Pile Service Loading	
	Original	Deviate	Original	Deviate	P	Mx
1	-0.60	0.36	-0.30	0.09	11	0
2	0.00	0.00	-0.30	0.09	11	0
3	0.60	0.36	-0.30	0.09	11	0
4	-0.60	0.36	0.30	0.09	11	0
5	0.00	0.00	0.30	0.09	11	0
6	0.60	0.36	0.30	0.09	11	0
CG.	0.00	0.00	0.00	0.00	68	2
Total					0.54	0

Pile No.	X-Coordinate		Y-Coordinate		Pile Service Loading	
	Original	Deviate	Original	Deviate	P	Mx
1	-0.60	0.36	-0.30	0.09	11	0
2	0.00	0.00	-0.30	0.09	11	0
3	0.60	0.36	-0.30	0.09	11	0
4	-0.60	0.36	0.30	0.09	11	0
5	0.00	0.00	0.30	0.09	11	0
6	0.60	0.36	0.30	0.09	11	0
CG.	0.00	0.00	0.00	0.00	68	2
Total					0.54	0



Corner	X	Y	Corner	X	Y
1	-0.15	-0.1	1	-0.80	-0.50
2	0.15	-0.1	2	0.80	-0.50
3	0.15	0.1	3	0.80	0.50
4	-0.15	0.1	4	0.80	0.50
			5	0.80	0.50
			6	-0.80	0.50
			7	-0.80	0.50
			8	-0.80	0.50

Beam Shear	X1		X2		Length	Deep Beam		Y1	Y2	Length
	X-Negative	X-Positive	X-Negative	X-Positive						
X-Negative	-0.67	-0.50	-0.67	0.50	1.00	X-Negative	-0.38	-0.50	-0.38	0.50
X-Positive	0.67	-0.50	0.67	0.50	1.00	X-Positive	0.38	-0.50	0.38	0.50
Y-Negative	-0.80	-0.62	-0.80	-0.62	1.60	Y-Negative	-0.80	-0.20	0.80	-0.20
Y-Positive	-0.80	0.62	-0.80	0.62	1.60	Y-Positive	-0.80	0.20	0.80	0.20
Punching	X1	Y1	X2	Y2	Length	Moment	X1	Y1	X2	Y2
X-Negative	-0.41	-0.50	-0.41	0.50	1.00	X-Negative	-0.15	-0.50	-0.15	0.50
X-Positive	0.41	-0.50	0.41	0.50	1.00	X-Positive	0.15	-0.50	0.15	0.50
Y-Negative	-0.80	-0.36	-0.80	-0.36	1.60	Y-Negative	-0.80	-0.10	0.80	-0.10
Y-Positive	-0.80	0.36	-0.80	0.36	1.60	Y-Positive	-0.80	0.10	0.80	0.10

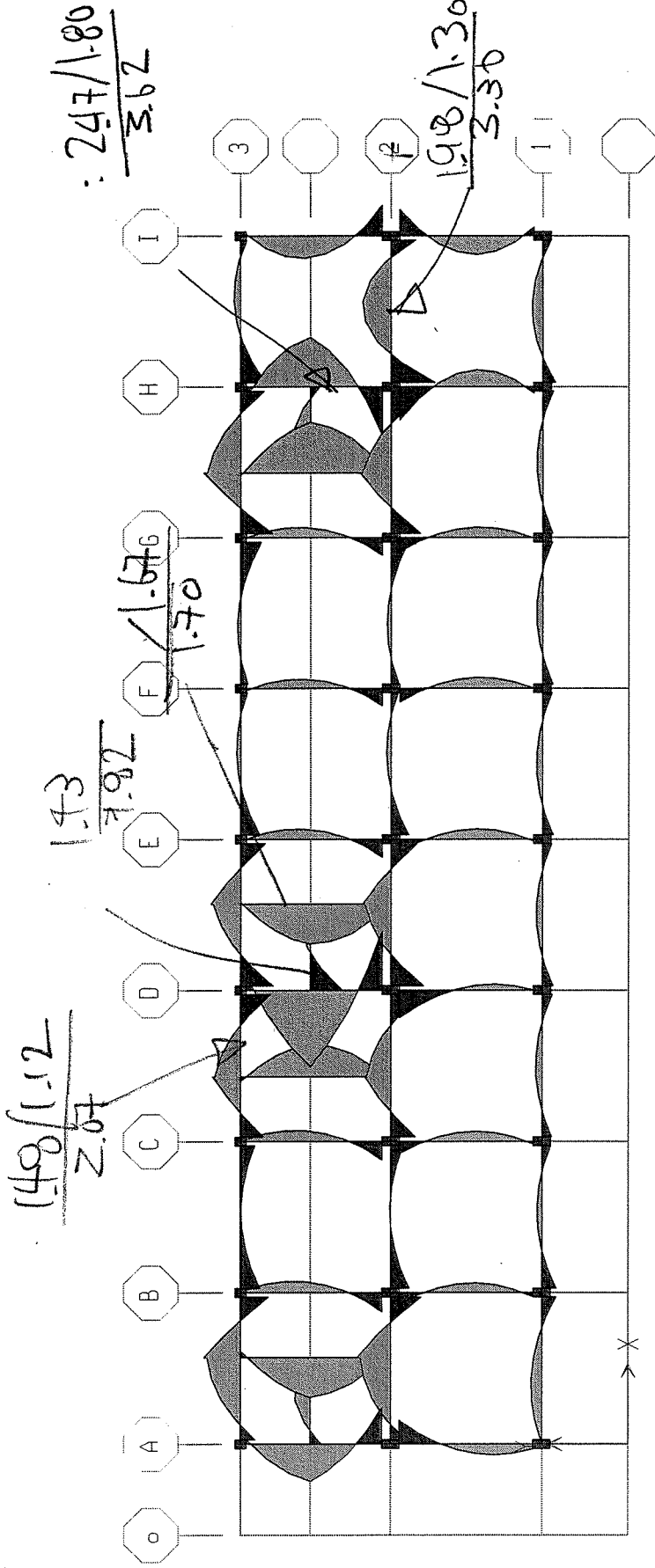
Ultimate Shear and Shear Stress at Critical Section

Pile No.	Beam Shear			Deep Beam Shear			Punching Shear		
	X-Neg	X-Pos	Y-Avg	X-Neg	X-Pos	Y-Avg	X-Neg	X-Pos	Y-Avg
1	3	0	0	18	0	18	0	0	4
2	0	0	0	0	0	18	0	0	4
3	0	3	0	18	18	0	18	0	4
4	3	0	0	18	0	0	18	0	4
5	0	0	0	0	0	18	0	0	4
6	0	3	0	0	18	0	18	0	4
Shear	5	5	0	35	35	53	35	35	11
Moment				8	8	5	5	5	5
Factor	2.42	2.42	2.50	2.50	2.50				
Length	1.00	1.00	1.60	1.00	1.60	1.60	1.00	1.60	1.60
Depth	0.52	0.52	0.52	0.52	0.52	0.52	0.52	0.52	0.52
Stress	1.01	1.01	0.90	6.76	6.76	6.34	6.76	6.76	1.27
Allow.	5.93			14.33	14.33	14.81	14.81	14.81	11.85

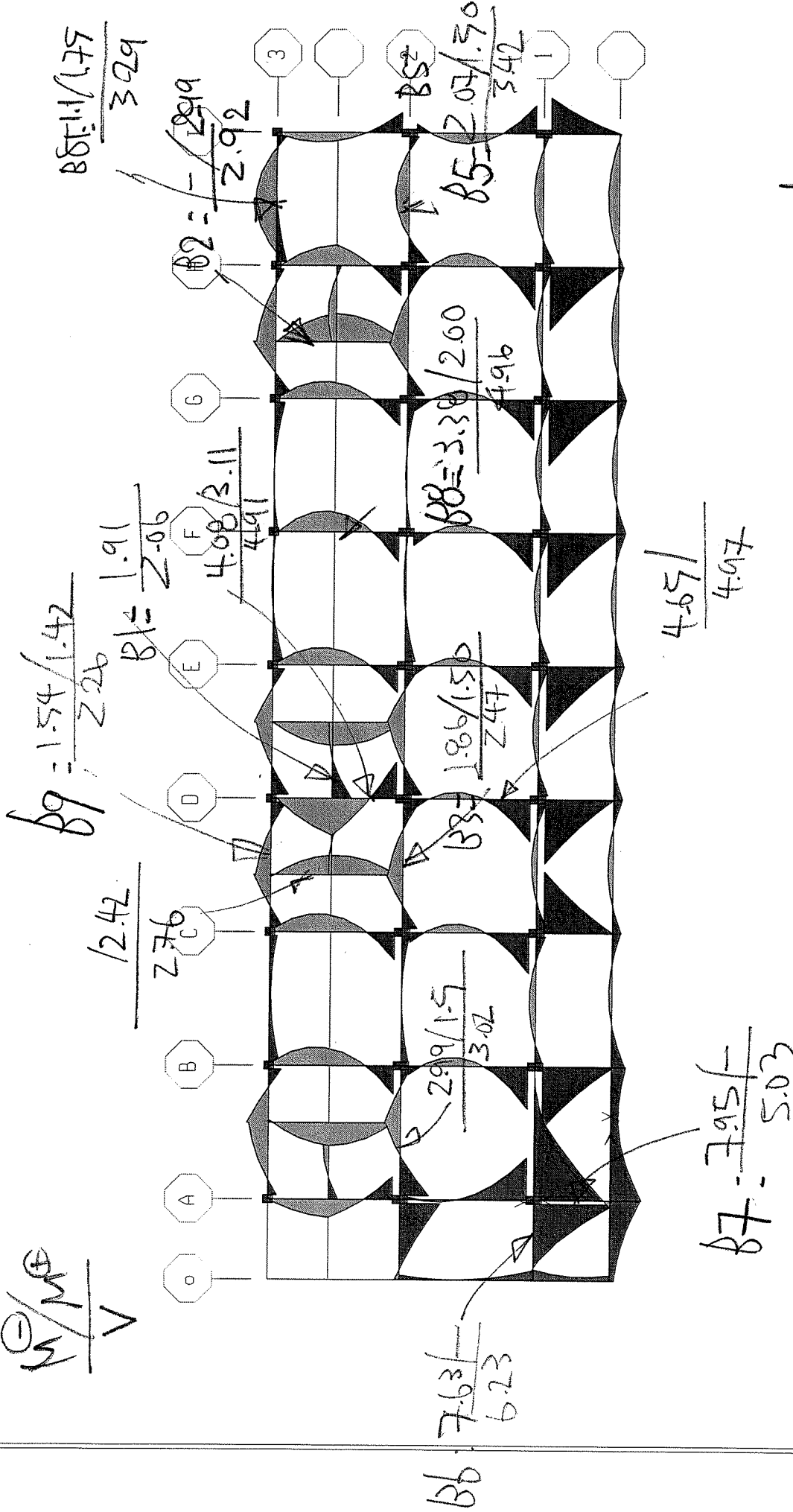
Ultimate Moment and Reinforcement at Critical Section

Pile Number	X-Negative			X-Positive			Y-Negative			Y-Positive		
	a	V	M	a	V	M	a	V	M	a	V	M
1	0.45	18	8	0	0	0	0.20	18	4	0.40	0	0
2	-0.15	0	0	-0.15	0	0	0.20	18	4	-0.40	0	0
3	-0.75	0	0	0.45	18	8	0.20	18	4	-0.40	0	0
4	0.45	18	8	-0.75	0	0	-0.40	0	0	0.20	18	4
5	-0.15	0	0	-0.15	0	0	-0.40	0	0	0.20	18	4
6	-0.75	0	0	0.45	18	8	-0.40	0	0	0.20	18	4
Moment				16			16			11		
Length	1.00			1.00			1.60			1.60		
Depth	0.52			0.52			0.52			0.52		
As (Req.)	8.6			8.6			5.7			5.7		
MinAs (Beam)	16.2			16.2			29.1			29.1		
MinAs (Slab)	15			15			24			24		
Conc. Moment	111			111			178			178		

$\frac{M^e/M^p}{V}$

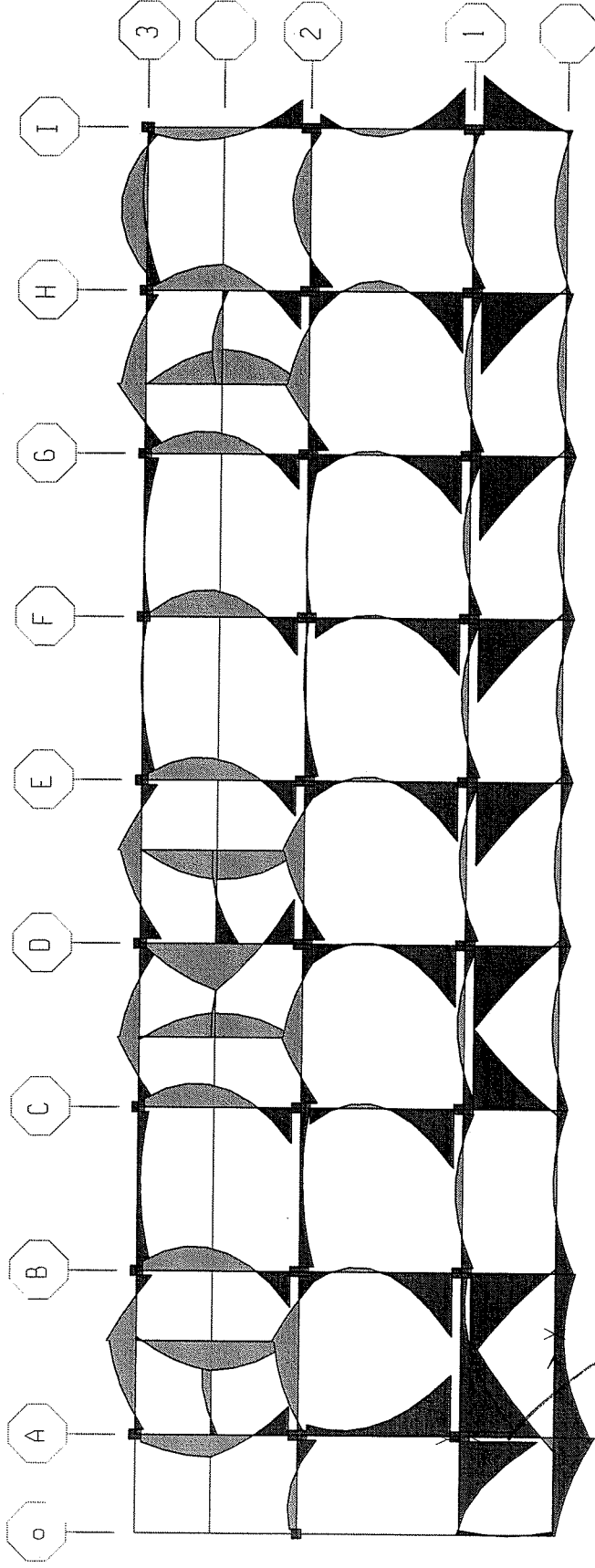


$$\frac{M/M_E}{V}$$



2nd FL

$$\frac{M_e/M_t}{V}$$



797/-
525

384
M_t #Z

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Beam No. : **B-1**

A) Properties of Materials

$f_c' = 240$ ksc
 $f_y = 4,000$ ksc : Grade : SD-40

B) Beam Configuration & Loading

Span Length, L = 3.50 m,
Width, b = 0.15 m,
Depth, D = 0.40 m,
Concrete Cover, d' = 0.035 m.

C) Bending Reinforcement

Neg. Bending, M- = 1,069 kg.m
Effective Depth, d = 0.36 m.
 $MR = Rbd^2 = 2,519$ kg.m
 $As' = 0.00$ cm²
 $Ast = 1.96$ cm²

Provided : **2 DB 12 mm (T)**
(As = 2.26 cm²)
2 DB 12 mm (B)
(As = 2.26 cm²)

Pos. Bending, M+ = 650 kg.m
Effective Depth, d = 0.36 m.
 $MR = Rbd^2 = 2,519$ kg.m
 $As' = 0.00$ cm²
 $Ast = 1.19$ cm²

Provided : **2 DB 12 mm (T)**
(As = 2.26 cm²)
2 DB 12 mm (B)
(As = 2.26 cm²)

D) Shear Reinforcement

V = 1,100 kg < V(max) = 11,043 kg ; Section OK.
 $V_c = 0.29 \sqrt{f_c'} b d = 2,426$ kg
Provided Shear Reinf. : RB 6 mm, $A_v = 0.283$ cm² 2 Legs
 $V_s = V_u - V_c = 0$ kg
Spacing, S = $\frac{A_v f_y d}{V_s} = 0$ cm
d/2 = 18.00 cm
S(min) = $A_v f_y / (3.5 b) = 25.85$ cm

Provided : **RB - 6 mm @ 20 cm (2 Legs)**

E) Section (W/O Checking of Deflection)

Beam Type : 1
Span Length, L = 3.50 m
Span/Depth ratio, L/D = 8.75
Allowable L/D = 1.00 * 16.00
= 16.00 > Actual L/D ratio OK.

Beam Type : 1. Simple Beam
2. One End Continuous Beam
3. Both End Continuous Beam
4. Cantilever Beam

Beam No. : **B-2**

A) Properties of Materials

$f_c' = 240$ ksc
 $f_y = 4,000$ ksc : Grade : 0.00

B) Beam Configuration & Loading

Span Length, L = 3.50 m,
Width, b = 0.15 m,
Depth, D = 0.40 m,
Concrete Cover, d' = 0.035 m.

C) Bending Reinforcement

Neg. Bending, M- = 0 kg.m
Effective Depth, d = 0.36 m.
 $MR = Rbd^2 = 2,519$ kg.m
 $As' = 0.00$ cm²
 $Ast = 0.00$ cm²

Provided : **2 DB 12 mm (T)**
(As = 2.26 cm²)
2 DB 12 mm (B)
(As = 2.26 cm²)

Pos. Bending, M+ = 2,980 kg.m
Effective Depth, d = 0.36 m.
 $MR = Rbd^2 = 2,519$ kg.m
 $As' = 1.40$ cm²
 $Ast = 5.55$ cm²

Provided : **2 DB 12 mm (T)**
(As = 2.26 cm²)
4 DB 16 mm (B)
(As = 8.04 cm²)

D) Shear Reinforcement

V = 2,992 kg < V(max) = 11,043 kg ; Section OK.
 $V_c = 0.29 \sqrt{f_c'} b d = 2,426$ kg
Provided Shear Reinf. : RB 6 mm, $A_v = 0.283$ cm² 2 Legs
 $V_s = V_u - V_c = 566$ kg
Spacing, S = $\frac{A_v f_y d}{V_s} = 43.16$ cm
d/2 = 18.00 cm
S(min) = $A_v f_y / (3.5 b) = 25.85$ cm

Provided : **RB - 6 mm @ 20 cm (2 Legs)**

E) Section (W/O Checking of Deflection)

Beam Type : 1
Span Length, L = 3.50 m
Span/Depth ratio, L/D = 8.75
Allowable L/D = 1.00 * 16.00
= 16.00 > Actual L/D ratio OK.

Beam Type : 1. Simple Beam
2. One End Continuous Beam
3. Both End Continuous Beam
4. Cantilever Beam

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Beam No. : **B3**

A) Properties of Materials

f_c' = 240 ksc
 f_y = 4,000 ksc : Grade : SD-40

B) Beam Configuration & Loading

Span Length , L = 3.50 m,
Width , b = 0.15 m.
Depth , D = 0.40 m.
Concrete Cover , d' = 0.035 m.

C) Bending Reinforcement

Neg. Bending , M- = 1,720 kg.m
Effective Depth , d = 0.36 m.
 $MR=Rbd^2$ = 2,519 kg.m
 As' = 0.00 cm^2
 Ast = 3.15 cm^2

Provided : 4 DB 12 mm (T)
(As = 4.52 cm^2)
2 DB 12 mm (B)
(As = 2.26 cm^2)

Pos. Bending , M+ = 1,270 kg.m
Effective Depth , d = 0.36 m.
 $MR=Rbd^2$ = 2,519 kg.m
 As' = 0.00 cm^2
 Ast = 2.33 cm^2

Provided : 2 DB 12 mm (T)
(As = 2.26 cm^2)
4 DB 12 mm (B)
(As = 4.52 cm^2)

D) Shear Reinforcement

V = 2,310 kg < $V(max)$ = 11,043 kg ; Section OK.
 $V_c=0.29*\sqrt{f_c'}*b*d$ = 2,426 kg
Provided Shear Reinf. : RB 6 mm , Av = 0.283 cm^2 2 Legs
 $V_s = V_u - V_c$ = 0 kg
Spacing , S = $Av*f_y*d/V_s$
= 18.00 cm
d/2 = 18.00 cm

S(min) = $Av*f_y/(3.5*b)$ = 25.85 cm Provided : RB - 6 mm @ 20 cm (2 Legs)

E) Section (W/O Checking of Deflection)

Beam Type : 2 Beam Type : 1. Simple Beam
Span Length , L = 3.50 m 2. One End Continuous Beam
Span/Depth ratio , L/D = 8.75 3. Both End Continuous Beam
Allowable L/D = 1.00 * 18.50 4. Cantilever Beam
= 18.50 > Actual L/D ratio OK.

Beam No. : **B4**

A) Properties of Materials

f_c' = 240 ksc
 f_y = 4,000 ksc : Grade : 0.00

B) Beam Configuration & Loading

Span Length , L = 3.50 m,
Width , b = 0.15 m.
Depth , D = 0.40 m.
Concrete Cover , d' = 0.035 m.

C) Bending Reinforcement

Neg. Bending , M- = 3,130 kg.m
Effective Depth , d = 0.36 m.
 $MR=Rbd^2$ = 2,519 kg.m
 As' = 1.24 cm^2
 Ast = 5.85 cm^2

Provided : 4 DB 16 mm (T)
(As = 8.04 cm^2)
2 DB 12 mm (B)
(As = 2.26 cm^2)

Pos. Bending , M+ = 2,880 kg.m
Effective Depth , d = 0.36 m.
 $MR=Rbd^2$ = 2,519 kg.m
 As' = 1.10 cm^2
 Ast = 5.34 cm^2

Provided : 2 DB 12 mm (T)
(As = 2.26 cm^2)
4 DB 16 mm (B)
(As = 8.04 cm^2)

D) Shear Reinforcement

V = 4,290 kg < $V(max)$ = 11,043 kg ; Section OK.
 $V_c=0.29*\sqrt{f_c'}*b*d$ = 2,426 kg
Provided Shear Reinf. : RB 6 mm , Av = 0.283 cm^2 2 Legs
 $V_s = V_u - V_c$ = 1,864 kg
Spacing , S = $Av*f_y*d/V_s$
= 13.11 cm
d/2 = 18.00 cm

S(min) = $Av*f_y/(3.5*b)$ = 25.85 cm Provided : RB - 6 mm @ 12.50 cm (2 Legs)

E) Section (W/O Checking of Deflection)

Beam Type : 2 Beam Type : 1. Simple Beam
Span Length , L = 3.50 m 2. One End Continuous Beam
Span/Depth ratio , L/D = 8.75 3. Both End Continuous Beam
Allowable L/D = 1.00 * 18.50 4. Cantilever Beam
= 18.50 > Actual L/D ratio OK.

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Beam No. : **B4a**

A) Properties of Materials

$f_c' = 240$ ksc
 $f_y = 4,000$ ksc : Grade : SD-40

B) Beam Configuration & Loading

Span Length , L = 3.50 m,
Width , b = 0.20 m,
Depth , D = 0.40 m,
Concrete Cover , d' = 0.035 m.

C) Bending Reinforcement

Neg. Bending , M- = 3,800 kg.m
Effective Depth , d = 0.36 m.
 $MR=Rbd^2 = 3,359$ kg.m
 $As' = 0.80$ cm²
 $Ast = 7.04$ cm²

Provided : **4 DB 16 mm (T)**
(As = 8.04 cm²)
2 DB 12 mm (B)
(As = 2.26 cm²)

Pos. Bending , M+ = 1,600 kg.m
Effective Depth , d = 0.36 m.
 $MR=Rbd^2 = 3,359$ kg.m
 $As' = 0.00$ cm²
 $Ast = 2.93$ cm²

Provided : **2 DB 12 mm (T)**
(As = 2.26 cm²)
4 DB 12 mm (B)
(As = 4.52 cm²)

D) Shear Reinforcement

V = 3,800 kg < V(max) = 14,724 kg ; Section OK.
 $Vc=0.29*\text{Sqrt}(f_c')*b*d = 3,235$ kg
Provided Shear Reinf. : RB 6 mm , $Av = 0.283$ cm² 2 Legs
 $Vs = Vu-Vc = 565$ kg
Spacing , S = $Av*f_v*d/Vs = 43.22$ cm
= 18.00 cm
d/2 = 18.00 cm
 $S(\text{min}) = Av*f_y/(3.5*b) = 19.39$ cm

Provided : **RB - 6 mm. @ 12.50 cm (2 Legs)**

E) Section (W/O Checking of Deflection)

Beam Type : 2
Span Length , L = 3.50 m
Span/Depth ratio , L/D = 8.75
Allowable L/D = 1.00 * 18.50
= 18.50 > Actual L/D ratio OK.

Beam Type : 1. Simple Beam
2. One End Continuous Beam
3. Both End Continuous Beam
4. Cantilever Beam

Beam No. : **B5**

A) Properties of Materials

$f_c' = 240$ ksc
 $f_y = 4,000$ ksc : Grade : 0.00

B) Beam Configuration & Loading

Span Length , L = 3.50 m,
Width , b = 0.15 m,
Depth , D = 0.36 m,
Concrete Cover , d' = 0.035 m.

C) Bending Reinforcement

Neg. Bending , M- = 2,070 kg.m
Effective Depth , d = 0.36 m.
 $MR=Rbd^2 = 3,359$ kg.m
 $As' = 0.00$ cm²
 $Ast = 3.79$ cm²

Provided : **4 DB 12 mm (T)**
(As = 4.52 cm²)
2 DB 12 mm (B)
(As = 2.26 cm²)

Pos. Bending , M+ = 1,500 kg.m
Effective Depth , d = 0.36 m.
 $MR=Rbd^2 = 3,359$ kg.m
 $As' = 0.00$ cm²
 $Ast = 2.75$ cm²

Provided : **2 DB 12 mm (T)**
(As = 2.26 cm²)
4 DB 12 mm (B)
(As = 4.52 cm²)

D) Shear Reinforcement

V = 3,420 kg < V(max) = 11,043 kg ; Section OK.
 $Vc=0.29*\text{Sqrt}(f_c')*b*d = 2,426$ kg
Provided Shear Reinf. : RB 6 mm , $Av = 0.283$ cm² 2 Legs
 $Vs = Vu-Vc = 994$ kg
Spacing , S = $Av*f_v*d/Vs = 24.58$ cm
= 18.00 cm
d/2 = 18.00 cm
 $S(\text{min}) = Av*f_y/(3.5*b) = 25.85$ cm

Provided : **RB - 6 mm. @ 20 cm (2 Legs)**

E) Section (W/O Checking of Deflection)

Beam Type : 2
Span Length , L = 3.50 m
Span/Depth ratio , L/D = 9.72
Allowable L/D = 1.00 * 18.50
= 18.50 > Actual L/D ratio OK.

Beam Type : 1. Simple Beam
2. One End Continuous Beam
3. Both End Continuous Beam
4. Cantilever Beam

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Beam No. : **B6**

A) Properties of Materials

fc' = 240 ksc
 fy = 4,000 ksc : Grade : SD-40

B) Beam Configuration & Loading

Span Length , L = 3.50 m,
 Width , b = 0.20 m,
 Depth , D = 0.50 m,
 Concrete Cover , d' = 0.035 m.

C) Bending Reinforcement

Neg. Bending , M- = 7,630 kg.m
 Effective Depth , d = 0.46 m.
 MR=Rbd² = 5,485 kg.m
 As' = 3.05 cm²
 Ast = 11.19 cm²

Provided : **5 DB 20 mm (T)**
 (As = 15.71 cm²)
3 DB 20 mm (B)
 (As = 9.42 cm²)

Pos. Bending , M+ = 650 kg.m
 Effective Depth , d = 0.46 m.
 MR=Rbd² = 5,485 kg.m
 As' = 0.00 cm²
 Ast = 0.93 cm²

Provided : **2 DB 20 mm (T)**
 (As = 6.28 cm²)
2 DB 20 mm (B)
 (As = 6.28 cm²)

D) Shear Reinforcement

V = 6,230 kg < V(max) = 18,813 kg ; Section OK.
 Vc=0.29*sqrt(fc')*b*d = 4,133 kg
 Provided Shear Reinf. : RB 6 mm , Av = 0.283 cm² 2 Legs
 Vs = Vu-Vc = 2,097 kg
 Spacing , S = Av*fv*d/Vs = 14.89 cm
 = 23.00 cm
 d/2 = 19.39 cm
 S(min) = Av*fy/(3.5*b) = 19.39 cm

Provided : **RB - 6 mm @ 12.5 cm (2 Legs)**

E) Section (W/O Checking of Deflection)

Beam Type : 2
 Span Length , L = 3.50 m
 Span/Depth ratio , L/D = 7.00
 Allowable L/D = 1.00 * 18.50
 = 18.50 > Actual L/D ratio OK.

Beam Type : 1. Simple Beam
 2. One End Continuous Beam
 3. Both End Continuous Beam
 4. Cantilever Beam

Beam No. : **B7**

A) Properties of Materials

fc' = 240 ksc
 fy = 4,000 ksc : Grade : 0.00

B) Beam Configuration & Loading

Span Length , L = 3.50 m,
 Width , b = 0.20 m,
 Depth , D = 0.50 m,
 Concrete Cover , d' = 0.035 m.

C) Bending Reinforcement

Neg. Bending , M- = 7,950 kg.m
 Effective Depth , d = 0.46 m.
 MR=Rbd² = 5,485 kg.m
 As' = 3.82 cm²
 Ast = 11.68 cm²

Provided : **2 DB 12 mm (T)**
 (As = 2.26 cm²) *Increase Rebars !*
2 DB 12 mm (B)
 (As = 2.26 cm²) *Increase Rebars !*

Pos. Bending , M+ = 1,500 kg.m
 Effective Depth , d = 0.46 m.
 MR=Rbd² = 5,485 kg.m
 As' = 0.00 cm²
 Ast = 2.15 cm²

Provided : **2 DB 12 mm (T)**
 (As = 2.26 cm²)
4 DB 16 mm (B)
 (As = 8.04 cm²)

D) Shear Reinforcement

V = 5,030 kg < V(max) = 18,813 kg ; Section OK.
 Vc=0.29*sqrt(fc')*b*d = 4,133 kg
 Provided Shear Reinf. : RB 6 mm , Av = 0.283 cm² 2 Legs
 Vs = Vu-Vc = 897 kg
 Spacing , S = Av*fv*d/Vs = 34.81 cm
 = 23.00 cm
 d/2 = 19.39 cm
 S(min) = Av*fy/(3.5*b) = 19.39 cm

Provided : **RB - 6 mm @ 12.5 cm (2 Legs)**

E) Section (W/O Checking of Deflection)

Beam Type : 2
 Span Length , L = 3.50 m
 Span/Depth ratio , L/D = 7.00
 Allowable L/D = 1.00 * 18.50
 = 18.50 > Actual L/D ratio OK.

Beam Type : 1. Simple Beam
 2. One End Continuous Beam
 3. Both End Continuous Beam
 4. Cantilever Beam

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Beam No. : **B8**

A) Properties of Materials

fc' = 240 ksc
 fy = 4,000 ksc : Grade : SD-40

B) Beam Configuration & Loading

Span Length , L = 3.50 m,
 Width , b = 0.20 m.
 Depth , D = 0.50 m.
 Concrete Cover , d' = 0.035 m.

C) Bending Reinforcement

Neg. Bending , M- = 3,380 kg.m
 Effective Depth , d = 0.46 m.
 MR=Rbd² = 5,485 kg.m
 As' = 0.00 cm²
 Ast = 4.84 cm²

Provided : **2 DB 20 mm (T)**
 (As = 6.28 cm²)
2 DB 16 mm (B)
 (As = 4.02 cm²)

Pos. Bending , M+ = 2,000 kg.m
 Effective Depth , d = 0.46 m.
 MR=Rbd² = 5,485 kg.m
 As' = 0.00 cm²
 Ast = 2.87 cm²

Provided : **2 DB 16 mm (T)**
 (As = 4.02 cm²)
2 DB 16 mm (B)
 (As = 4.02 cm²)

D) Shear Reinforcement

V = 4,960 kg < V(max) = 18,813 kg ; Section OK.
 Vc=0.29*sqrt(fc')*b*d = 4,133 kg
 Provided Shear Reinf. : RB 6 mm , Av = 0.283 cm² 2 Legs
 Vs = Vu-Vc = 827 kg
 Spacing , S = Av*fv*d/Vs = 37.76 cm
 d/2 = 23.00 cm
 S(min) = Av*fy/(3.5*b) = 19.39 cm

Provided : **RB - 6 mm @ 20 cm (2 Legs)**

E) Section (W/O Checking of Deflection)

Beam Type : 1
 Span Length , L = 3.50 m
 Span/Depth ratio , L/D = 7.00
 Allowable L/D = 1.00 * 16.00
 = 16.00 > Actual L/D ratio OK.

Beam Type : 1. Simple Beam
 2. One End Continuous Beam
 3. Both End Continuous Beam
 4. Cantilever Beam

Beam No. : **B9**

A) Properties of Materials

fc' = 240 ksc
 fy = 4,000 ksc : Grade : 0.00

B) Beam Configuration & Loading

Span Length , L = 3.50 m,
 Width , b = 0.15 m.
 Depth , D = 0.50 m.
 Concrete Cover , d' = 0.035 m.

C) Bending Reinforcement

Neg. Bending , M- = 1,540 kg.m
 Effective Depth , d = 0.46 m.
 MR=Rbd² = 5,485 kg.m
 As' = 0.00 cm²
 Ast = 2.21 cm²

Provided : **2 DB 12 mm (T)**
 (As = 2.26 cm²)
2 DB 12 mm (B)
 (As = 2.26 cm²)

Pos. Bending , M+ = 1,750 kg.m
 Effective Depth , d = 0.46 m.
 MR=Rbd² = 5,485 kg.m
 As' = 0.00 cm²
 Ast = 2.51 cm²

Provided : **2 DB 12 mm (T)**
 (As = 2.26 cm²)
4 DB 12 mm (B)
 (As = 4.52 cm²)

D) Shear Reinforcement

V = 3,290 kg < V(max) = 14,110 kg ; Section OK.
 Vc=0.29*sqrt(fc')*b*d = 3,100 kg
 Provided Shear Reinf. : RB 6 mm , Av = 0.283 cm² 2 Legs
 Vs = Vu-Vc = 190 kg
 Spacing , S = Av*fv*d/Vs = 164.23 cm
 d/2 = 23.00 cm
 S(min) = Av*fy/(3.5*b) = 25.85 cm

Provided : **RB - 6 mm @ 20 cm (2 Legs)**

E) Section (W/O Checking of Deflection)

Beam Type : 1
 Span Length , L = 3.50 m
 Span/Depth ratio , L/D = 7.00
 Allowable L/D = 1.00 * 16.00
 = 16.00 > Actual L/D ratio OK.

Beam Type : 1. Simple Beam
 2. One End Continuous Beam
 3. Both End Continuous Beam
 4. Cantilever Beam

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Beam No. : **bst**

A) Properties of Materials

fc' = 240 ksc
 fy = 4,000 ksc : Grade : SD-40

B) Beam Configuration & Loading

Span Length , L = 3.50 m,
 Width , b = 0.20 m.
 Depth , D = 0.40 m.
 Concrete Cover , d' = 0.035 m.

C) Bending Reinforcement

Neg. Bending , M- = 1,100 kg.m
 Effective Depth , d = 0.36 m.
 MR=Rbd² = 3,359 kg.m
 As' = 0.00 cm²
 Ast = 2.01 cm²

Provided : **2 DB 12 mm (T)**
 (As = 2.26 cm²)
2 DB 12 mm (B)
 (As = 2.26 cm²)

Pos. Bending , M+ = 1,750 kg.m
 Effective Depth , d = 0.36 m.
 MR=Rbd² = 3,359 kg.m
 As' = 0.00 cm²
 Ast = 3.20 cm²

Provided : **2 DB 12 mm (T)**
 (As = 2.26 cm²)
4 DB 12 mm (B)
 (As = 4.52 cm²)

D) Shear Reinforcement

V = 3,290 kg < V(max) = 14,724 kg ; Section OK.
 Vc=0.29*sqrt(fc')*b*d = 3,235 kg
 Provided Shear Reinf. : RB 6 mm , Av = 0.283 cm² 2 Legs
 Vs = Vu-Vc = 55 kg
 Spacing , S = Av*fv*d/Vs = 441.88 cm
 d/2 = 18.00 cm
 S(min) = Av*fy/(3.5*b) = 19.39 cm

Provided : **RB- 6 mm @ 20 cm (2 Legs)**

E) Section (W/O Checking of Deflection)

Beam Type : 1
 Span Length , L = 3.50 m
 Span/Depth ratio , L/D = 8.75
 Allowable L/D = 1.00 * 16.00
 = 16.00 > Actual L/D ratio OK.

Beam Type : 1. Simple Beam
 2. One End Continuous Beam
 3. Both End Continuous Beam
 4. Cantilever Beam

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Slab No. : S-1

Type : Two-way slab (Method 2)

A) Properties of Materials & Design Parameter

fy	Yield strength of steel	=	2,400 ksc
fs	Allowable strength of steel	=	1,200 ksc
fc'	Ult. compressive strength of concrete	=	240 ksc
	Factor	=	0.375
fc	Allowable strength of concrete , $fc = \text{Factor} * fc'$	=	90 ksc
k	$k = 1/(1+(fs/(n*fc)))$	=	0.379
j	$j = 1-k/3$	=	0.874
R	$R = 0.50 * fc * j * k$	=	14.89 ksc

B) Slab Configuration

	Slab case	:	4
S	Short span	=	1.90 m
L	Long span	=	2.00 m
t	Thickness , $t(\text{min}) = 0.043 \text{ m}$.	=	0.100 m
m	S/L ratio	=	0.95
dc	Concrete covering	=	0.020 m

Slab case
 1 Interior
 2 Discort. 1 side
 3 Discort. 2 side
 4 Discort. 3 side
 5 Discort. 4 side

C) Loading

SW	Self weight , $SW = t * 2400$	=	240 kg/m ²
DL	Superimposed dead load	=	150 kg/m ²
LL	Live load	=	150 kg/m ²
wt	Total load , $wt = SW + DL + LL$	=	540 kg/m ²

D) Bending Reinforcement

D.1) Short Span :

d	Effective depth	=	0.077 m
MR	Resisting Moment , $Mr = R * (d * 100)^2$	=	883 kg-m/m

	Coefficient C	Moment $C * wt * S^2$ [kg-m/m]
M- sup (cont.)	0.064	125
M- sup (discont.)	0.032	62
M+ mid. Span	0.049	95

As(req)
 $M / (fs * j * d)$
 [cm²/m]

Provided reinforcement

1.55	RB	6 mm. @	0.175 m
	(As =	1.62 cm ² /m)	
0.77	RB	6 mm. @	0.20 m
	(As =	1.41 cm ² /m)	
1.17	RB	6 mm. @	0.20 m
	(As =	1.41 cm ² /m)	

D.2) Long Span :

d	Effective depth	=	0.071 m
MR	Resisting Moment , $Mr = R * (d * 100)^2$	=	751 kg-m/m

	Coefficient C	Moment $C * wt * S^2$ [kg-m/m]
M- sup (cont.)	0.058	113
M- sup (discont.)	0.029	57
M+ mid. Span	0.044	86

As(req)
 $M / (fs * j * d)$
 [cm²/m]

Provided reinforcement

1.52	RB	6 mm. @	0.175 m
	(As =	1.62 cm ² /m)	
0.76	RB	6 mm. @	0.20 m
	(As =	1.41 cm ² /m)	
1.15	RB	6 mm. @	0.20 m
	(As =	1.41 cm ² /m)	

Ast(min) Temp. steel , $Ast(\text{min}) = 0.0025 * b * t$

= 2.50 cm²/m

E) Transfer shear to support

V-S	Shear short span	=	1 kg/m
V-L	Shear long span	=	1 kg/m

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Slab No. : S-2

Type : Two-way slab (Method 2)

A) Properties of Materials & Design Parameter

fy	Yield strength of steel	=	2,400 ksc
fs	Allowable strength of steel	=	1,200 ksc
fc'	Ult. compressive strength of concrete	=	240 ksc
	Factor	=	0.375
fc	Allowable strength of concrete , fc = Factor*fc'	=	90 ksc
k	$k = 1/(1+(fs/(n*fc)))$	=	0.379
j	$j = 1-k/3$	=	0.874
R	$R = 0.50*fc*j*k$	=	14.89 ksc

Slab case	
1	Interior
2	Discont. 1 side
3	Discont. 2 side
4	Discont. 3 side
5	Discont. 4 side

B) Slab Configuration

	Slab case	:	3
S	Short span	=	2.00 m
L	Long span	=	3.50 m
t	Thickness , t(min) = 0.061 m.	=	0.125 m
m	S/L ratio	=	0.57
dc	Concrete covering	=	0.025 m

C) Loading

SW	Self weight , SW = t*2400	=	300 kg/m ²
DL	Superimposed dead load	=	150 kg/m ²
LL	Live load	=	150 kg/m ²
wt	Total load , wt = SW+DL+LL	=	600 kg/m ²

D) Bending Reinforcement

D.1) Short Span :

d	Effective depth	=	0.096 m
MR	Resisting Moment , Mr = R*(d*100) ²	=	1,358 kg-m/m

	Coefficient C	Moment C*wt*S ² [kg-m/m]	As(req) M/(fs*j*d) [cm ² /m]	Provided reinforcement
M- sup.(cont.)	0.084	202	2.01	RB 9 mm. @ 0.200 m (As = 3.18 cm ² /m)
M- sup (discont.)	0.042	101	1.01	RB 9 mm. @ 0.20 m (As = 3.18 cm ² /m)
M+ mid. Span	0.064	152	1.52	RB 9 mm. @ 0.20 m (As = 3.18 cm ² /m)

D.2) Long Span :

d	Effective depth	=	0.087 m
MR	Resisting Moment , Mr = R*(d*100) ²	=	1,114 kg-m/m

	Coefficient C	Moment C*wt*S ² [kg-m/m]	As(req) M/(fs*j*d) [cm ² /m]	Provided reinforcement
M- sup (cont.)	0.049	118	1.30	RB 9 mm. @ 0.200 m (As = 3.18 cm ² /m)
M- sup (discont.)	0.025	60	0.66	RB 9 mm. @ 0.20 m (As = 3.18 cm ² /m)
M+ mid. Span	0.037	89	0.98	RB 9 mm. @ 0.20 m (As = 3.18 cm ² /m)
Ast(min)	Temp. steel , Ast(min) = 0.0025 *b*t			= 3.13 cm ² /m

E) Transfer shear to support

V-S	Shear short span	=	1 kg/m
V-L	Shear long span	=	1 kg/m

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Stair No. : ST-1

A) Properties of Materials and Design Parameter

fy (Main Reinf.)	=	4,000 ksc
fs	=	1,700 ksc
fy (Temp. Reinf.)	=	2,400 ksc
fc' (Cyl.)	=	173 ksc
Factor	=	0.375
fc	=	65 ksc
Es	=	2.04E+06 ksc
Ec	=	2.09E+05 ksc
n	=	10
k	=	0.27
j	=	0.91
R	=	8.01 ksc
vc	=	3.81 ksc

B) Stair Configuration

Span Length, L	=	3.50 m
Thickness, t	=	0.150 m
Horizontal size of step, b	=	0.300 m
Vertical size of step, h	=	0.175 m
Concrete Cover	=	0.025 m

C) Loading

Superimpose Deadload, FL	=	50 kg/m ²
Landing+FL, DL1	=	710 kg/m ²
Stair+FL, DL2	=	994 kg/m ²
LL	=	300 kg/m ²
wt-1	=	1,060 kg/m ² (Landing+FL+LL)
wt-2	=	1,344 kg/m ² (Step + FL+LL)

D) Bending Reinforcement

d	=	0.119 m
MR	=	1,135 kg-m/m
Asr	=	6.17 cm ² /m
M	=	1,367 kg-m/m

As'	=	1.60 cm ² /m	12 mm. @ 0.20 m. (T)
			(Ast = 5.65 cm ² /m)
Ast	=	7.76 cm ² /m	12 mm. @ 0.13 m. (B)
			(Ast = 9.05 cm ² /m)
As-temp.	=	0.0025 *b*t	9 mm. @ 0.20 m. (T&B)
	=	3.75 cm ² /m	(Ast = 6.36 cm ² /m)

E) Load Transfer to Support

Serviced Load :	R1	=	1,648 kg/m	
	R2	=	1,405 kg/m	Vc = 4,539 kg/m ; > Vu OK.

F) Deflection

Es	=	2.04E+06 ksc	
Ec	=	2.09E+05 ksc	
n = Es/Ec	=	10	
ρ'	=	0.0048	
ρ	=	0.0076	
B = b/(n.As)	=	1.13 /cm	
r = (n-1)As'/(n.As)	=	0.56	
Kd	=	[Sqrt(2dB(1+rd'/d)+(1+r)^2)]-(1+r)/B	
	=	3.66 cm	
Ig	=	28,125 cm ⁴ /m	
Icr	=	b(Kd) ³ /3+nAs(d-kd) ² +(n-1)As'(kd-d') ²	
	=	7,702 cm ⁴ /m	< Ig OK.
Mcr = fr*Ig/(t/2)	=	986 kg-m/m	
M(service), Ms	=	1,367 kg-m/m	
(Mcr/Ms) ³	=	0.376	
Ie	=	(Mcr/Ms) ³ .Ig+[1-(Mcr/Ms) ³].Icr	
	=	15,385 cm ⁴ /m	< Ig OK.
Ec*Ie	=	3.21E+09 ksc	
Δ = 5*wL ⁴ /(384*Ec*Ie)	=	0.43 cm	
Δ-allowable = L/240	=	1.46 cm	OK.

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A) Properties of Materials

Fy	Yield Strength	=	2,400 ksc
Es	Modulus of Elasticity	=	2.10E+06 ksc

Section Properties

Section	:	C-100x50x20x2.3
Jnit Weight	=	4.06 kg/m
Ix	=	80.70 cm ⁴
Iy	=	19.00 cm ⁴
SX	=	16.10 cm ³
SY	=	6.06 cm ³

B) Roof Configuration & Loading

Asbestos Cement Roofing Tile or Steel Roof Sheet ;

L	Span , L	=	3.50 m	
@	Spacing of Purlin	=	1.00 m	
θ	Angle of Roof	=	20 °	(Slope ≥ 10 °)
SW	Purlin DL	=	4.06 kg/m	
DL	Deal load of Roof Sheet	=	8 kg/m ²	
LL	Live Load	=	30 kg/m ²	
WL	Wind Pressure	=	80 kg/m ²	

C) Check Bending Stresses

SW	Self weight of Purlin	=	4.06 kg/m
dl	Roof Sheet = DL*@	=	7.50 kg/m
ll	Live Load = LL*@	=	30.00 kg/m
wt	Total load		
	wt = SW+dl+ll	=	41.56 kg/m
wl	Wind Load Perpen. to Purlin		
	wl = WL*@*Sin θ	=	27.36 kg/m
wy	Wy = wt*cos θ +wl	=	66.42 kg/m
wx	Wx = wt*sin θ	=	14.21 kg/m
cmx	Moment coefficient for X-axis	=	0.125
cmy	Moment coefficient for Y-axis	=	0.125
Mx	Mx = cmx*wy*L ²	=	102 kg.m
My	My = cmy*wx*L ²	=	22 kg.m
fb	fb =(Mx/SX)+(My/(SY/2))	=	1,350 ksc
Fb	Alloable Stress		
	Fb = 0.6*Fy	=	1,440 ksc

fb < Fb OK.

D) Check Deflection

cd	Deflection coefficient	=	0.013
Δy	Deflection		
	Δy = (cd*wy*L ³)/(Es*Ix)	=	0.77 cm
Δ-all	Allowable Deflection		
	Δ-all = L/240	=	1.46 cm

dy < d-all OK.

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A) Properties of Materials

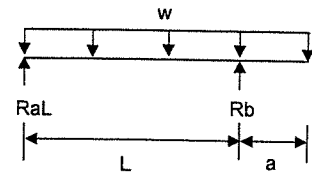
Fy	Yield Strength	=	2,400 ksc
Es	Modulus of Elasticity	=	2.10E+06 ksc

Section Properties	
Section	: Rec-150x50x2.3
Jnit Weight	= 6.95 kg/m
Ix	= 235.28 cm ⁴
Iy	= 42.00 cm ⁴
SX	= 31.37 cm ³
SY	= 16.80 cm ³

B) Roof Configuration & Loading

Asbestos Cement Roofing Tile or Steel Roof Sheet ;

L	Span , L	=	2.25 m
a	Cantilever Span, a	=	1.30 m
@	Spacing of Rafter	=	3.50 m
θ	Angle of Roof	=	20 °
SW	Rafter DL	=	6.95 kg/m
DL	Deal load of Roof Sheet+Purlin	=	15 kg/m ²
LL	Live Load	=	30 kg/m ²
WL	Wind Pressure	=	80 kg/m ²



C) Check Bending Stresses

SW	Self weight of Purlin	=	6.95 kg/m
dl	Roof Sheet = DL*@	=	52.50 kg/m
ll	Live Load = LL*@	=	105.00 kg/m
wl	Wind Load = WL*@	=	280.00 kg/m
wt	Total load	=	
	$wt = (SW+dl+ll+wl)/\cos \theta$	=	472.97 kg/m
Mc	$Mc = -0.50*wt*a^2$	=	-400 kg.m
M+max	$M+max = Ra*Xo-wt*Xo^2/2$	=	
	$Xo = (L^2-a^2)/(2*L)$	=	0.13 m
	M+max	=	41 kg.m
fb max	$fb = \text{Max}(\text{abs}(Mc, M+max))/SX$	=	1,274 ksc
Fb	Alloable Stress	=	
	$Fb = 0.6*Fy$	=	1,440 ksc

fb < Fb OK.

D) Check Deflection

Δo	Deflection in span		
	$\Delta_o = (5*wt*L^3)/(384*Es*Ix) - Mc*L^2/(16*Es*Ix)$	=	0.06 cm
Δ-all	Allowable Deflection		
	$\Delta\text{-allowable} = L/240$	=	0.94 cm
Δc	Deflection		
	$\Delta_c = (wt*a^3)/(8*Es*Ix) + wt*L*a*(4a^2-L^2)/(24*Es*Ix)$	=	0.34 cm
Δ-all	Allowable Deflection		
	$\Delta\text{-allowable} = a/120$	=	1.08 cm

dy < d-all OK.

Recheck Formuls

dy < d-all OK.

D) Reaction

Ra		=	354 kg
Rb		=	1,325 kg

1.02

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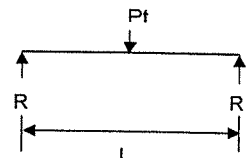
A) Properties of Materials

Fy	Yield Strength	=	2,400 ksc
Es	Modulus of Elasticity	=	2.10E+06 ksc

Section Properties	
Section	: Rec-150x100x3.2
Jnit Weight	= 15.33 kg/m
Ix	= 487.20 cm ⁴
SX	= 64.96 cm ³

B) Roof Configuration & Loading

L	Span , L	=	3.50 m
θ	Angle of Roof	=	20 °
SW	Rafter DL	=	15.33 kg/m
Pt	Pt from Steel Post	=	1,040 kg
wt	Total load	=	
	wt = (SW+W)	=	15.33 kg/m



C) Check Bending Stresses

M+max	$M+max = 0.125*wt*L^2$	=	933.47 kg.m
fb	$fb = M+max/SX$	=	1,437 ksc
Fb	Alloable Stress	=	
	$Fb = 0.6*Fy$	=	1,440 ksc

fb < Fb OK.

D) Check Deflection

Δo	Deflection in span	=	
	$Δo = (Pt*L^3)/(48*Es*Ix)$	=	0.91 cm
Δ-all	Allowable Deflection	=	
	$Δ-all = L/240$	=	1.46 cm

dy < d-all OK.

D) Reaction

R		=	547 kg
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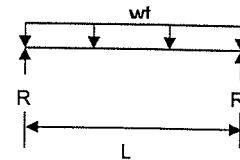
A) Properties of Materials

Fy	Yield Strength	=	2,400 ksc
Es	Modulus of Elasticity	=	2.10E+06 ksc

Section Properties	
Section	: Rec-150x100x3.2
Jnit Weight	= 15.33 kg/m
Ix	= 487.20 cm ⁴
SX	= 64.96 cm ³

B) Roof Configuration & Loading

L	Span , L	=	3.50 m
θ	Angle of Roof	=	20 °
SW	Rafter DL	=	15.33 kg/m
W	Total Load from Rafter	=	550 kg/m
wt	Total load	=	
	wt = (SW+W)	=	15.33 kg/m



C) Check Bending Stresses

M+max	$M+max = 0.125*wt*L^2$	=	23.47 kg.m
fb	$fb = M+max/SX$	=	36 ksc
Fb	Alloable Stress		
	$Fb = 0.6*Fy$	=	1,440 ksc

fb < Fb OK.

D) Check Deflection

Δo	Deflection in span		
	$Δo = (5*wt*L^3)/(384*Es*Ix)$	=	0.03 cm
Δ-all	Allowable Deflection		
	$Δ-all = L/240$	=	1.46 cm

dy < d-all OK.

D) Reaction

R		=	27 kg
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Job Title : Resident 4	Date : Mar-12	Subject : ตั้งเหล็ก, เสาคเหล็ก	
Designed : PSJ	Date :	Sheet :	Page :
Checked :			

Steel Post

A) Properties of Materials

Fy = 2,400 ksc

Es = 2.10E+06 ksc

C) Loading

Axial Force = 1,040 kg

D) Check Allowable Compression Force

Length of Member , L = 250 cm

K = 1.00

KL/r = 63.78

Cc = Sqrt(2π²*Es/Fy) = 131.42

KL/r < Cc ;

Fa = (1-(KL/r)²/(2*Cc²))*Fy/(5/3+3*(KL/r)/(8*Cc)-(KL/r)³/(8*Cc³))

= 1,154 ksc

Pa = Fa*A = 14,002 kg P < Pa OK.

B) Properties of Section

USE Section : Squ. 100x100x3.2 mm.

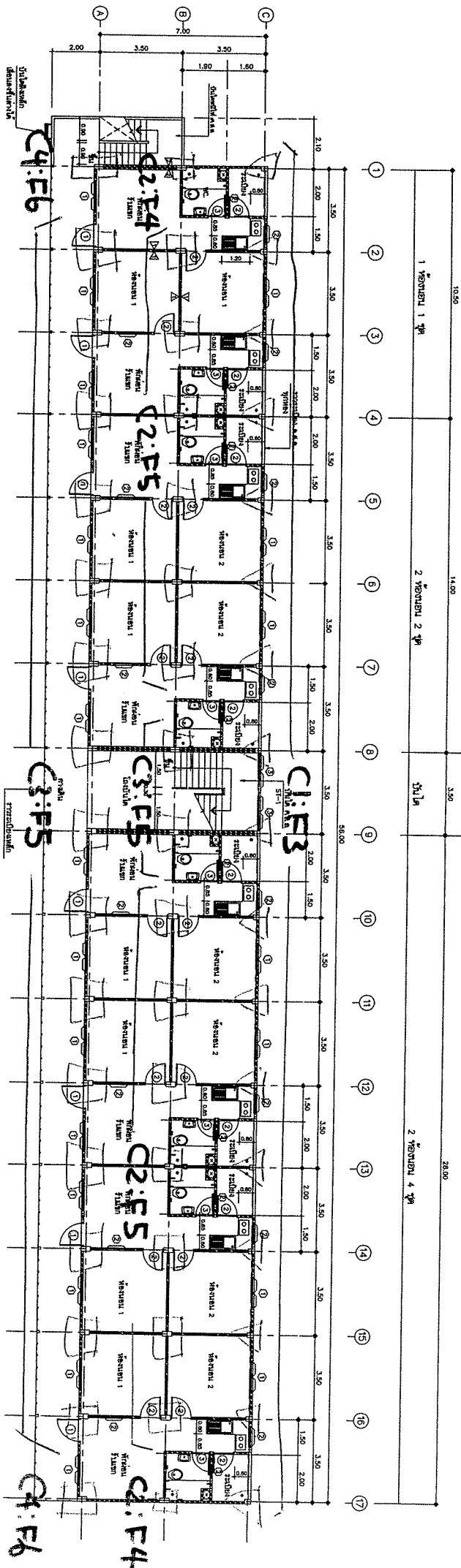
Section Area , A = 12.13 cm²

rx = 3.92 cm

ry = 3.92 cm

Notes : Effective Length Coefficient

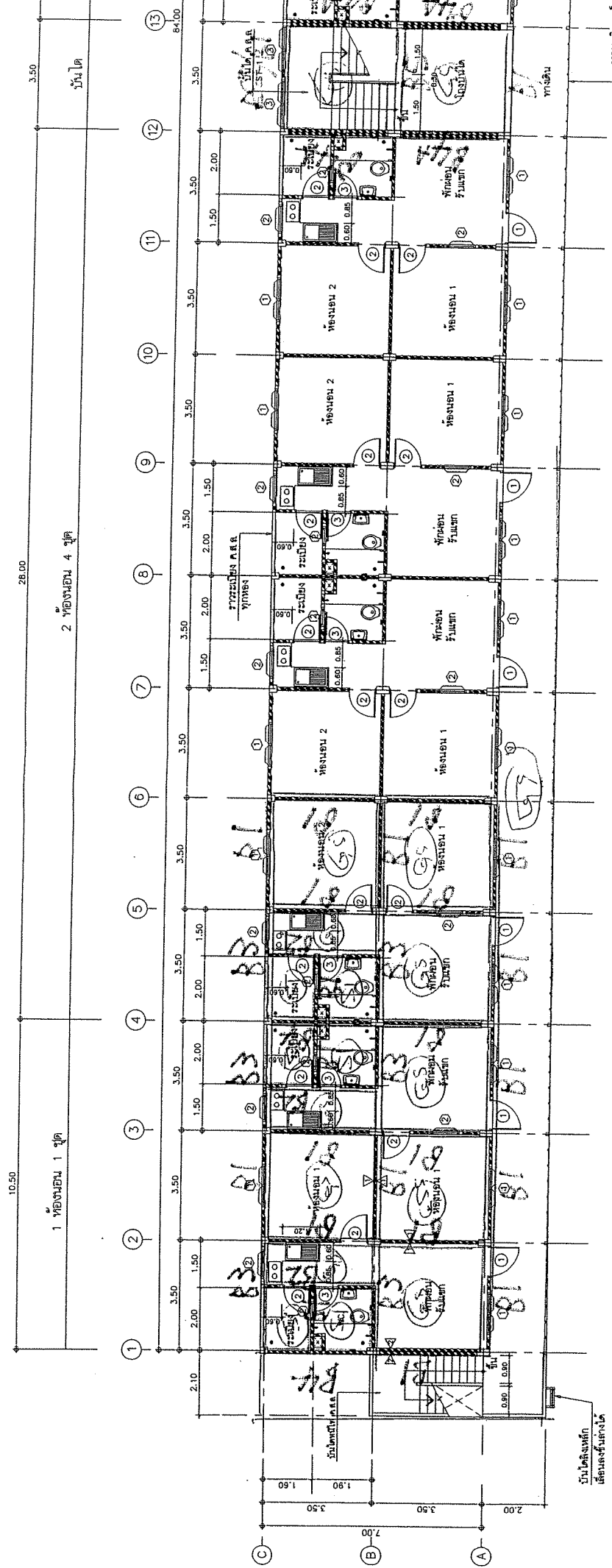
K	Condition
1.00	Pined with Pined Base
2.00	Guided with Pined Base
0.65	Fixed with Fixed Base
0.80	Pined with Fixed Base
1.20	Guided with Fixed Base
2.10	Free with Fixed Base



57,00

1/2017/1/1/1-4
 1 : 100
 1 2 3 4

Creation
Ilustrasi

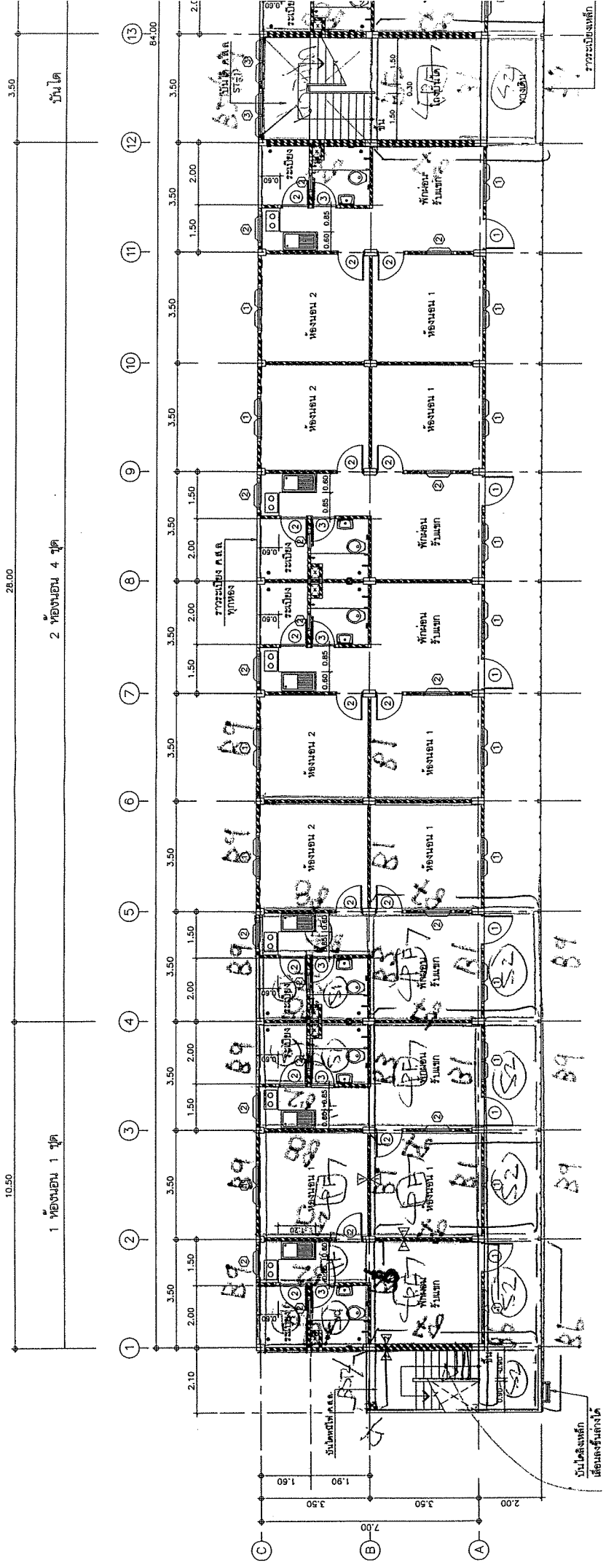


2 ห้องนอน 4 ชุด

1 ห้องนอน 1 ชุด

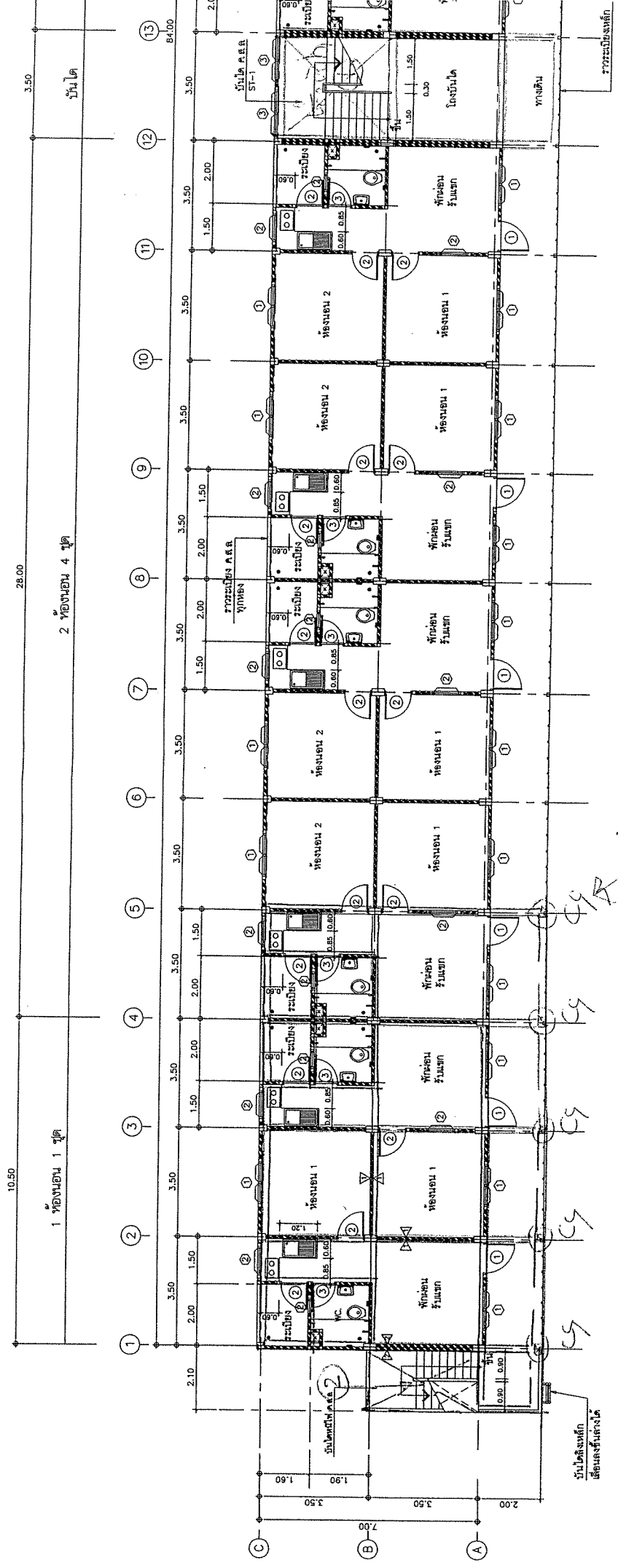
11.24.01-11.24.01.1

บันไดลงถ้ำ
เดินลงบันได



ดูที่ หน้า 2
 22/11/2564

พื้นที่ 2
 11/11/2564



1 ห้องนอน 1 ชุด
28.00
2 ห้องนอน 4 ชุด

Handwritten notes in Thai:

WU...

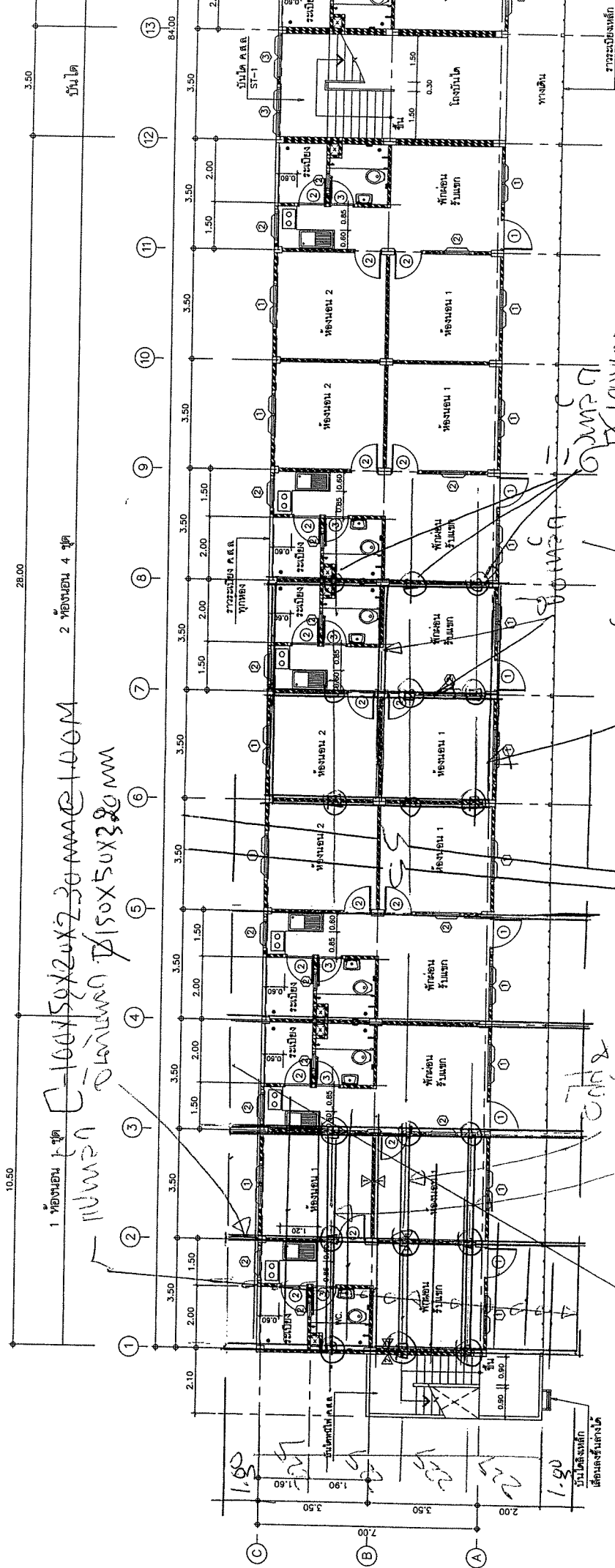
...

1000 CS

Handwritten number: 1104701214

บันไดขึ้นหลัก
เลื่อนลงบันได

บันไดขึ้นหลัก
เลื่อนลงบันได



1 ห้องนอน 1 10.50
 100x50x2x2.30mm @ 100mm
 2 ห้องนอน 4 29.00

2 ห้องนอน 4 29.00
 100x50x2x2.30mm @ 100mm

100x50x2x2.30mm

150x50x2.30mm

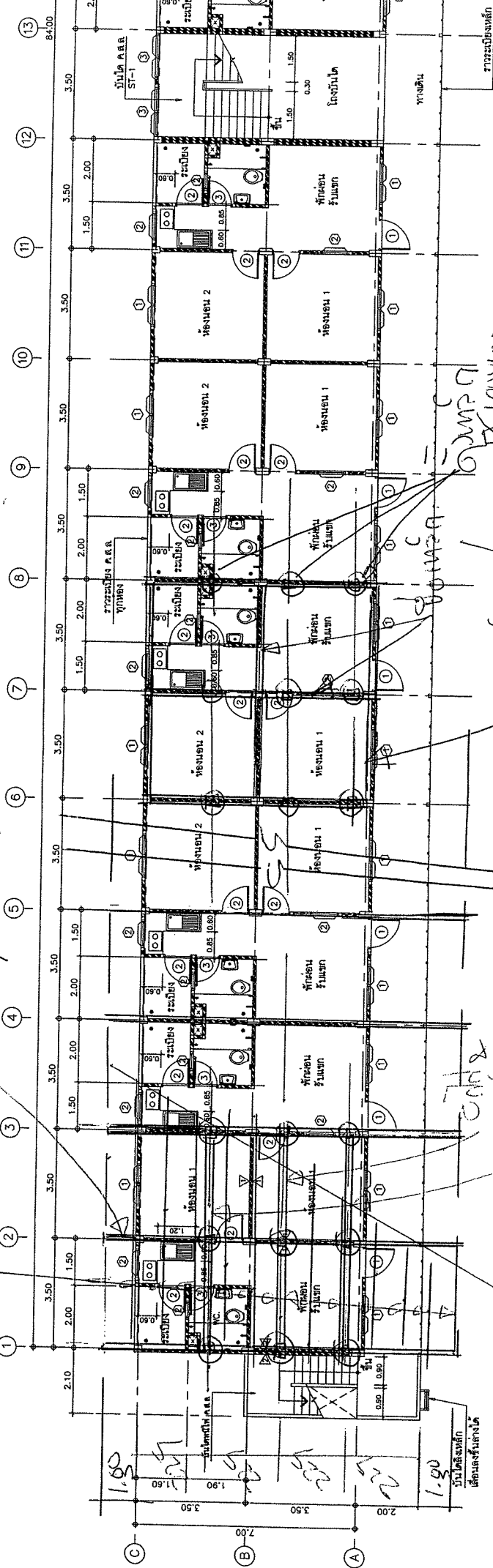
100x100x3.2mm

150x50x2.30mm

100x50x2x2.30mm

150x50x2.30mm

100x50x2x2.30mm



100x50x2x2.30mm

150x50x2.30mm

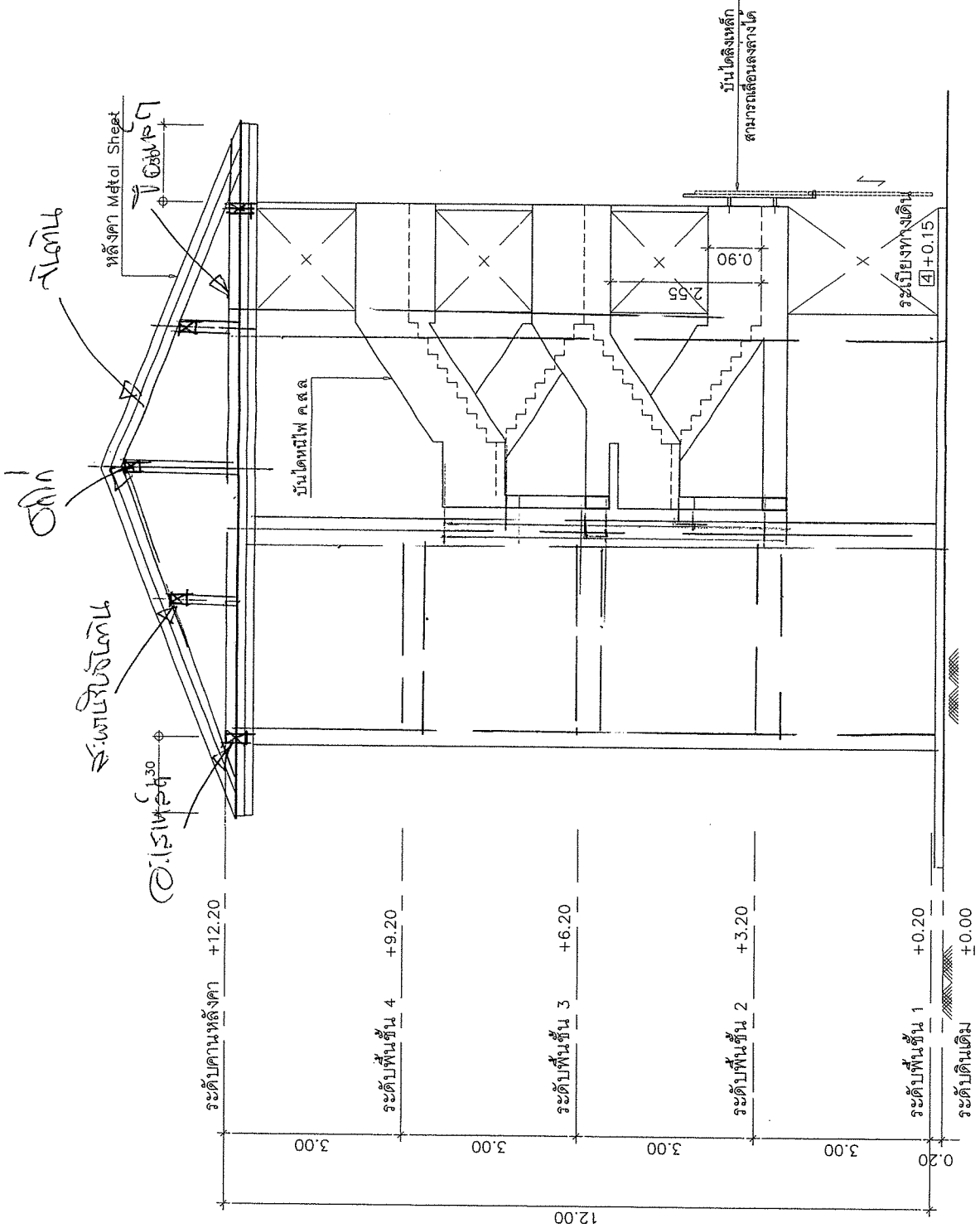
100x100x3.2mm

150x50x2.30mm

100x50x2x2.30mm








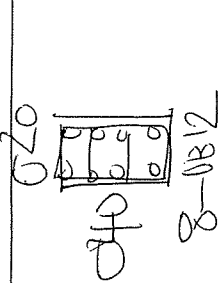


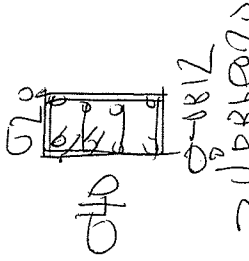
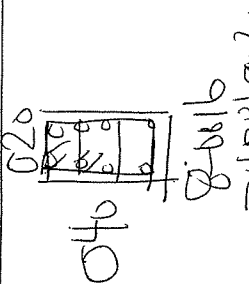




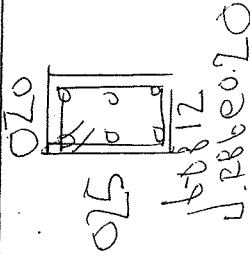
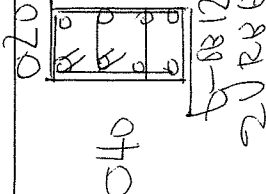
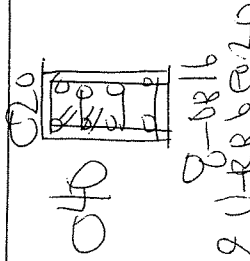
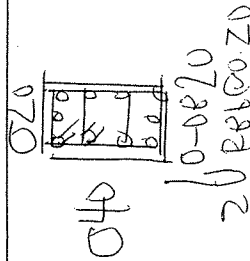
150x50x2.30mm

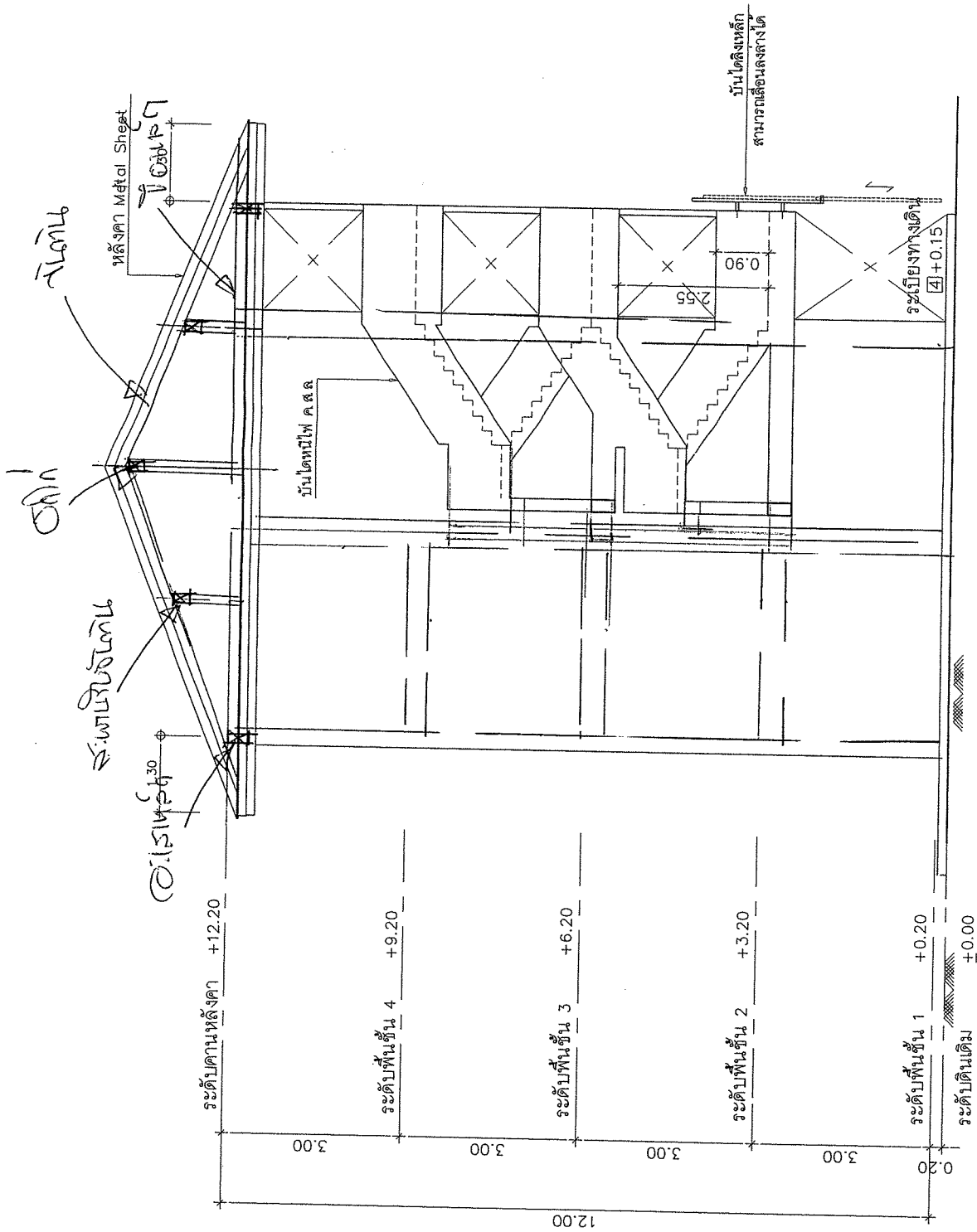
100x50x2x2.30mm



รูปด้าน 4

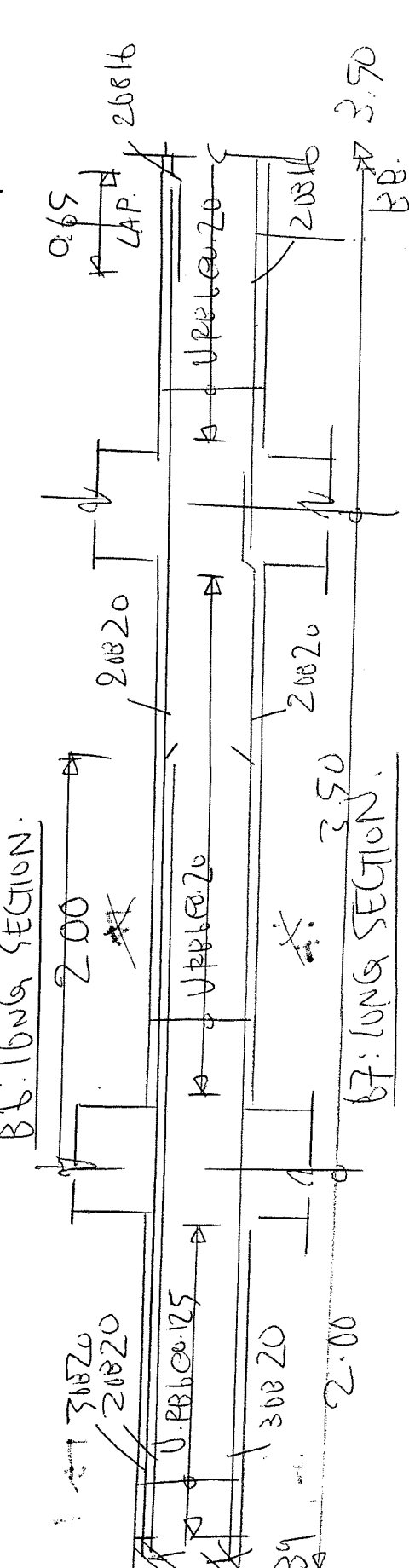
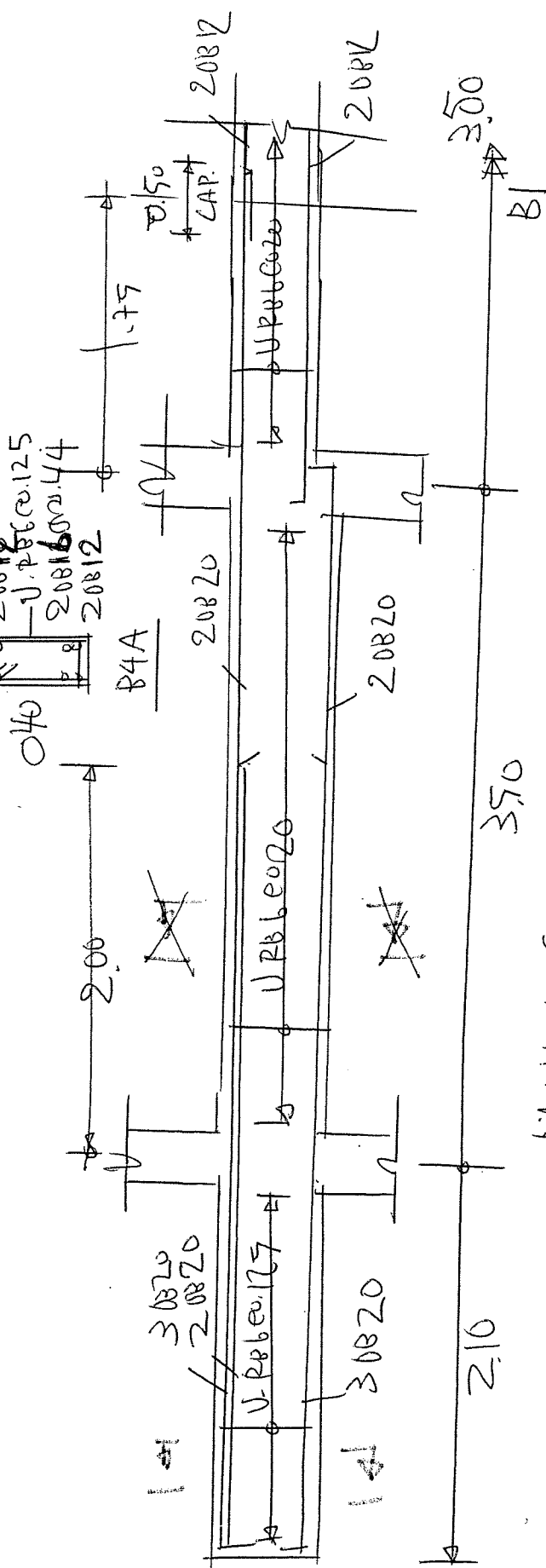
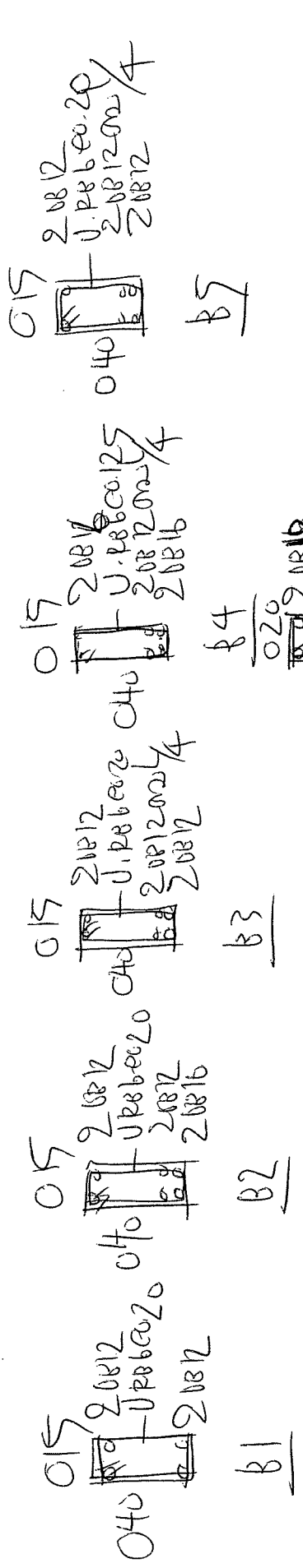
มาตราส่วน 1 : 75

பேர் / பி	C1	C2	C3	C4
வேலா டீலர் டீலர்				
சீலர் டீலர்				
சீலர் டீலர்				
சீலர் டீலர்				
சீலர் டீலர்				



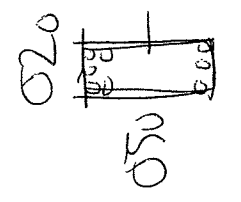
รูปด้าน 4

มาตราส่วน 1 : 75

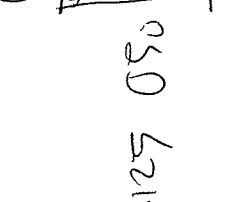


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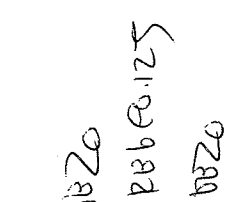
B7: LONG SECTION.



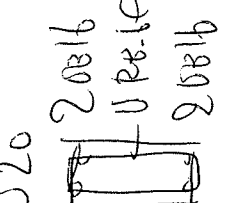
86:1-1



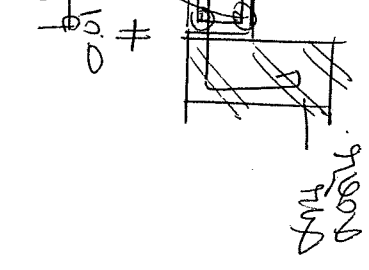
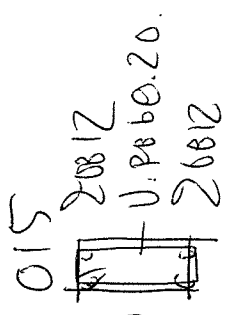
87:1-1



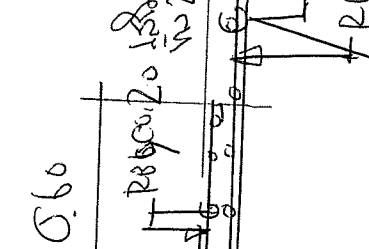
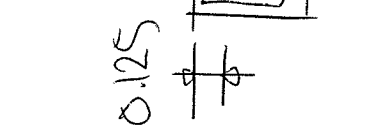
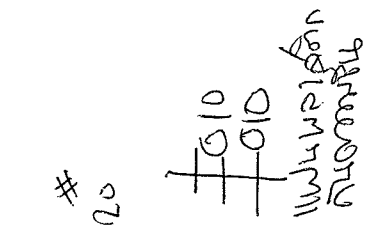
88



89

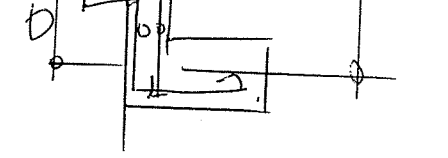


85



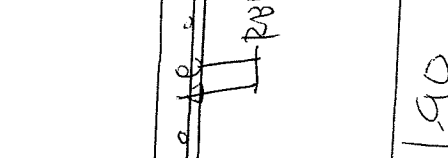
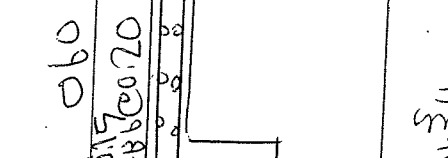
1.925

S2: 0.1434

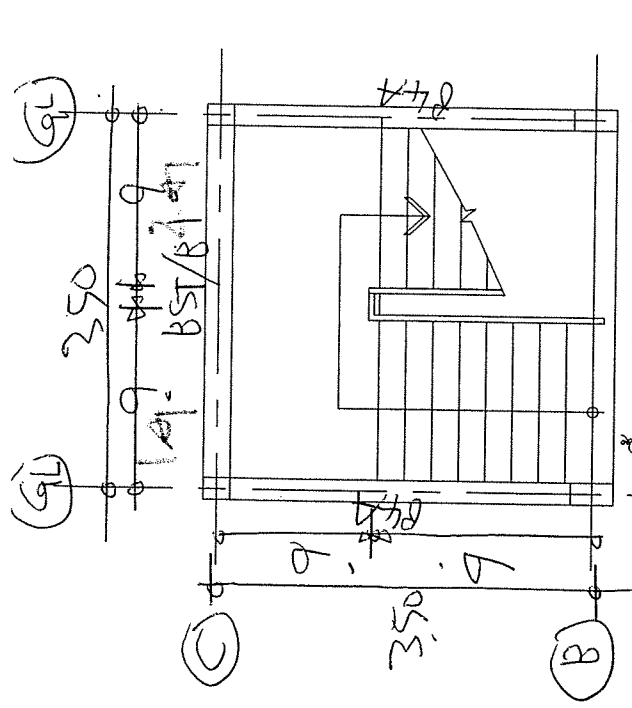


1.60

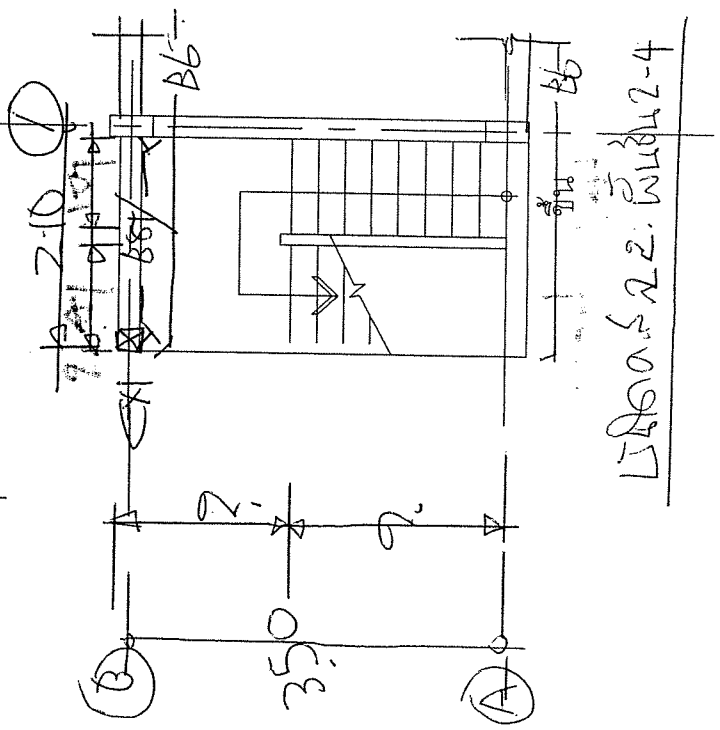
S1: 0.1434



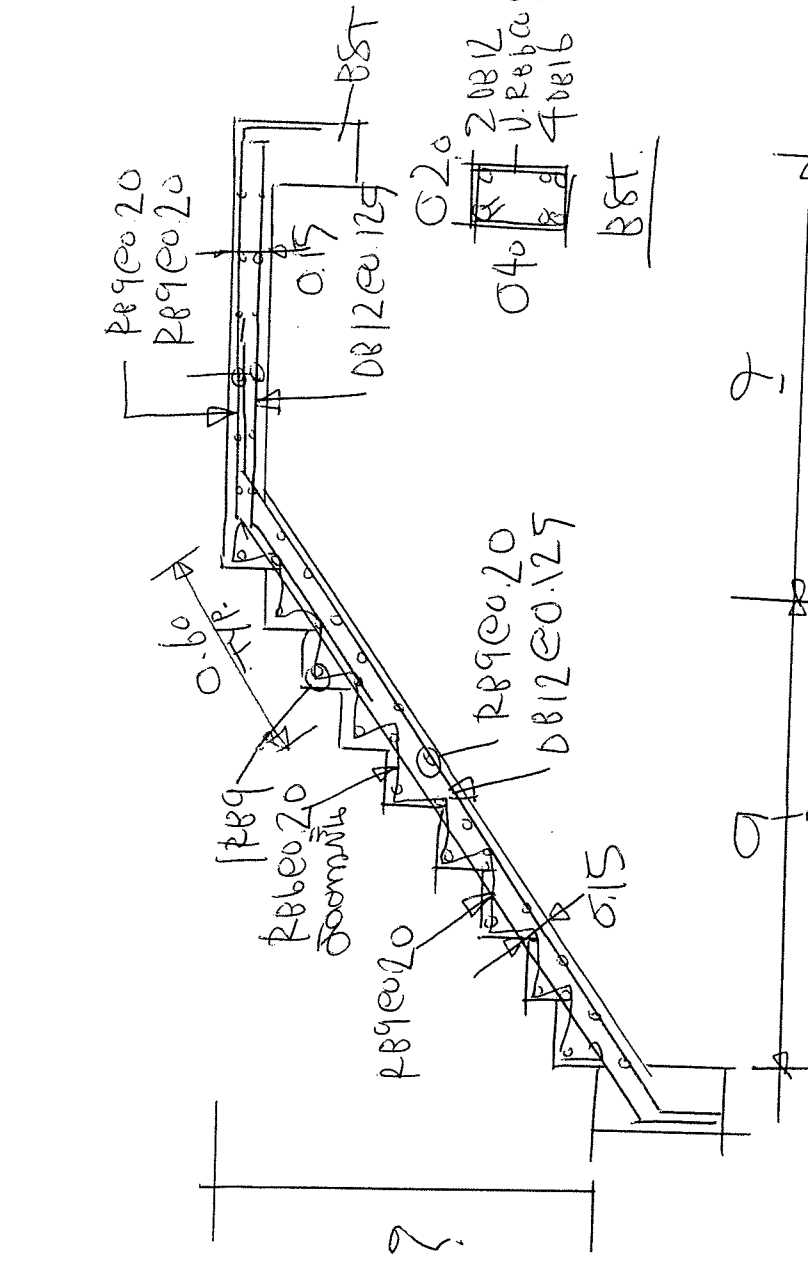
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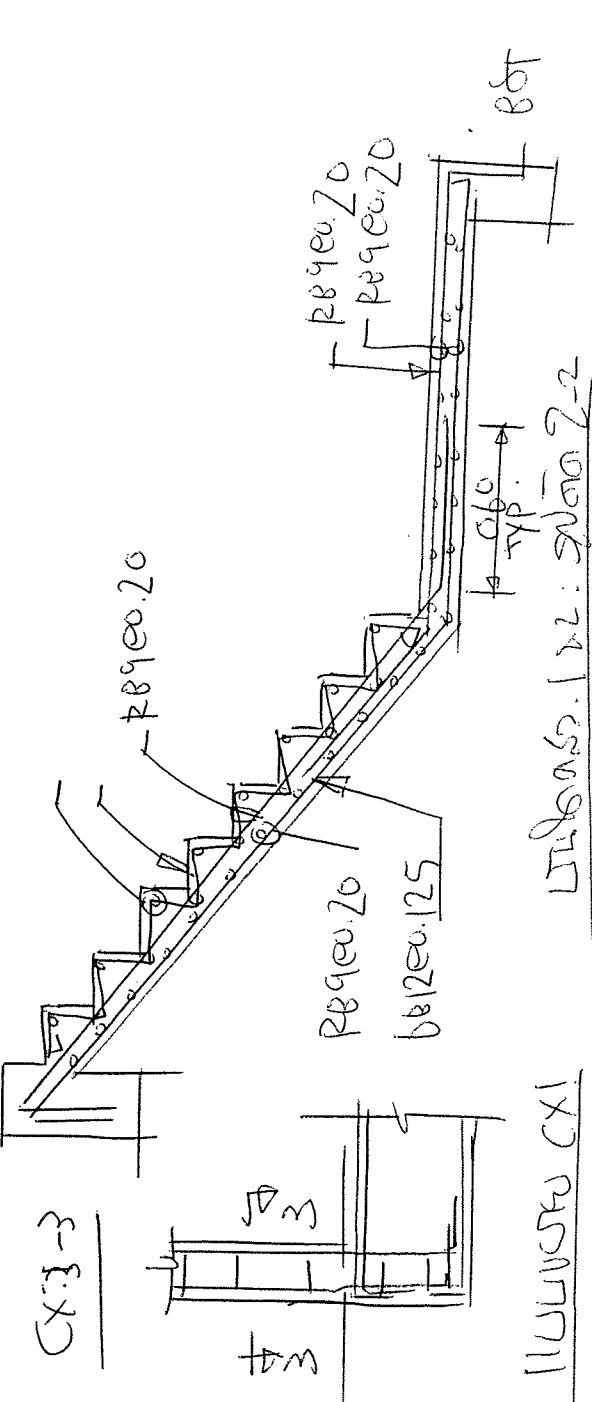
BS 2-4
 LINDAS. 1: 2-4



LINDAS. 2: 2-4



020 4 BB12 U. R860.20
 CX 3-3
 LINDAS. 1 x 2: 2-4



LINDAS. 1 x 2: 2-4