




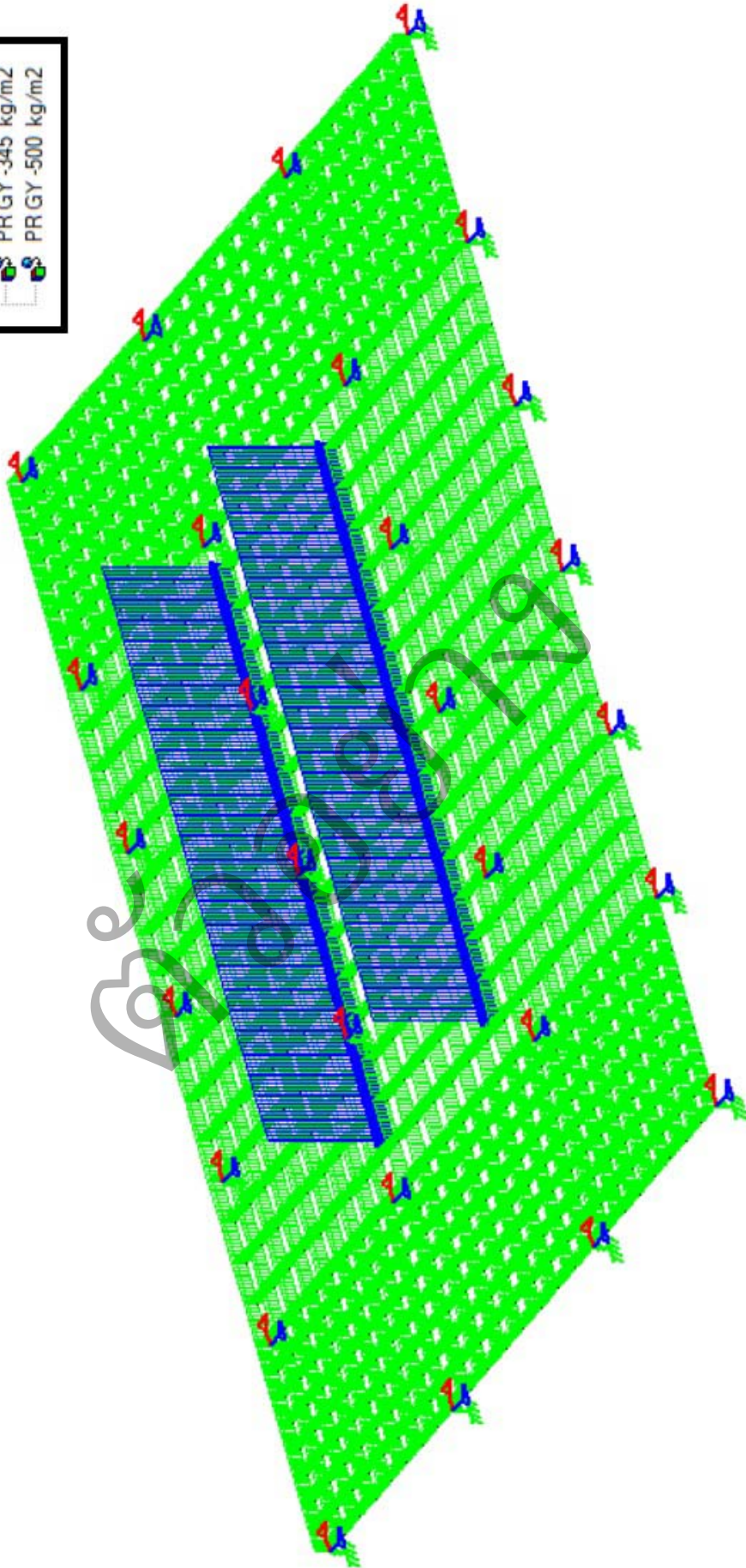
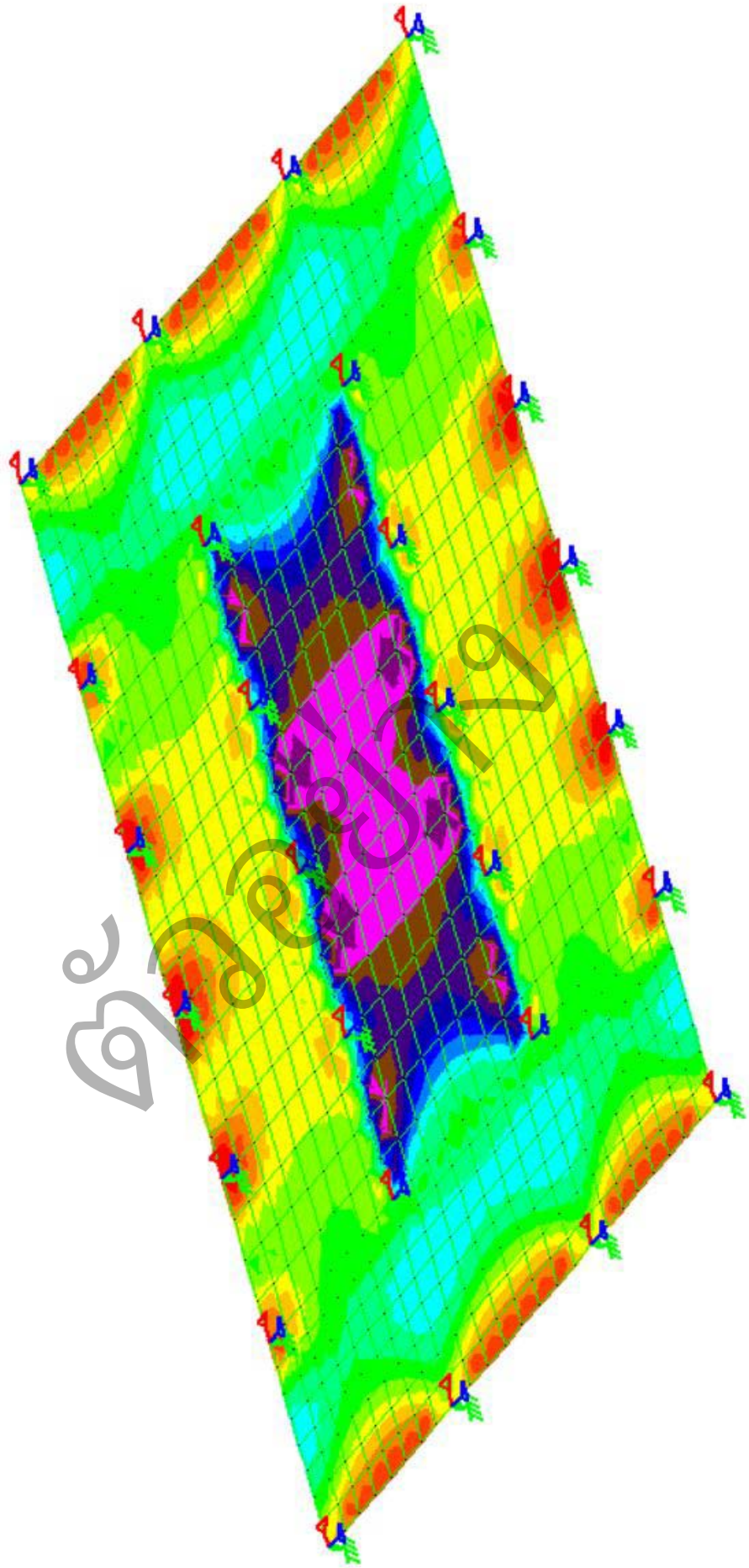
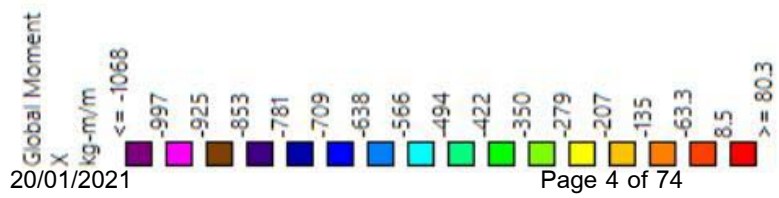


Dry weight(kg)  
2928.12

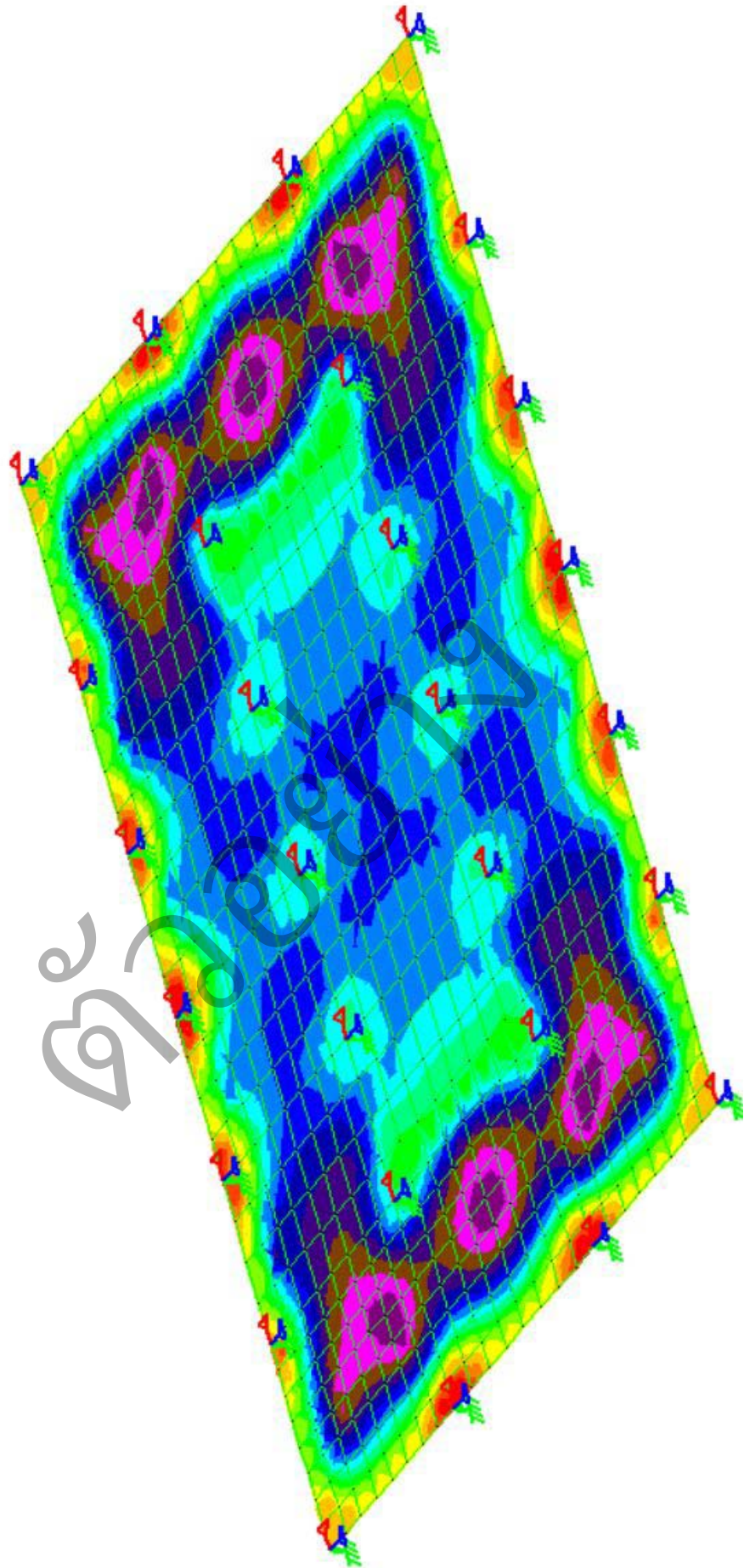
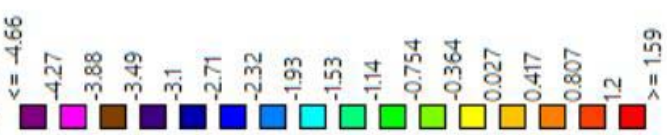
REV.	DATE	DETAILS	TITLE :	Scale:
0	2020-09-25	-	AC250S	NTS
			6LTAA8.9-G2 - UCID274K	Units:
			250 KVA	mm.
			Drawing No: INS-01	Sheet 1 Of 1

	1 : LOAD CASE 1
	SELFWEIGHT Y-1
	UNI GY -500 kg/m
	PR GY -345 kg/m2
	PR GY -500 kg/m2



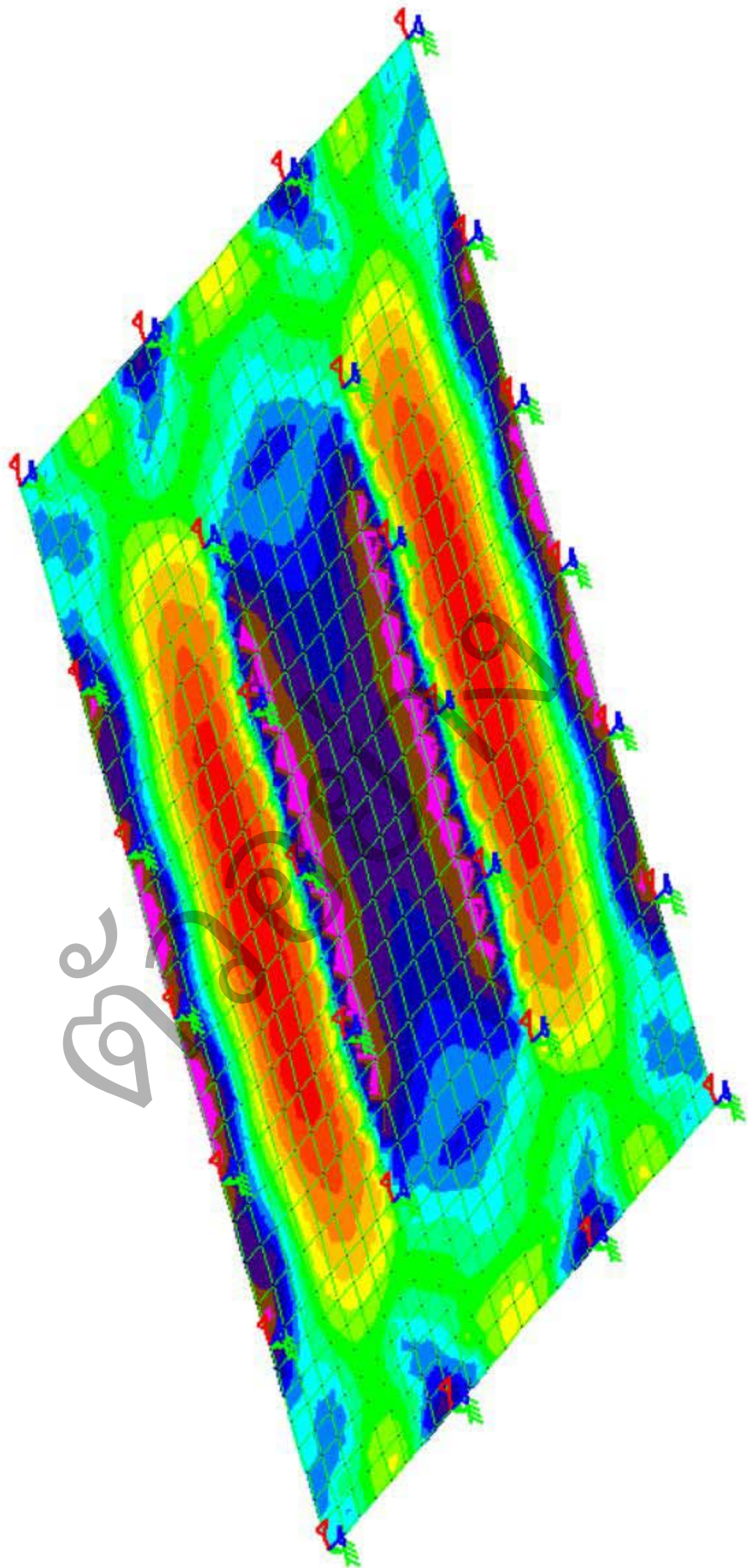
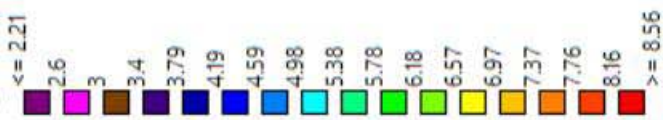


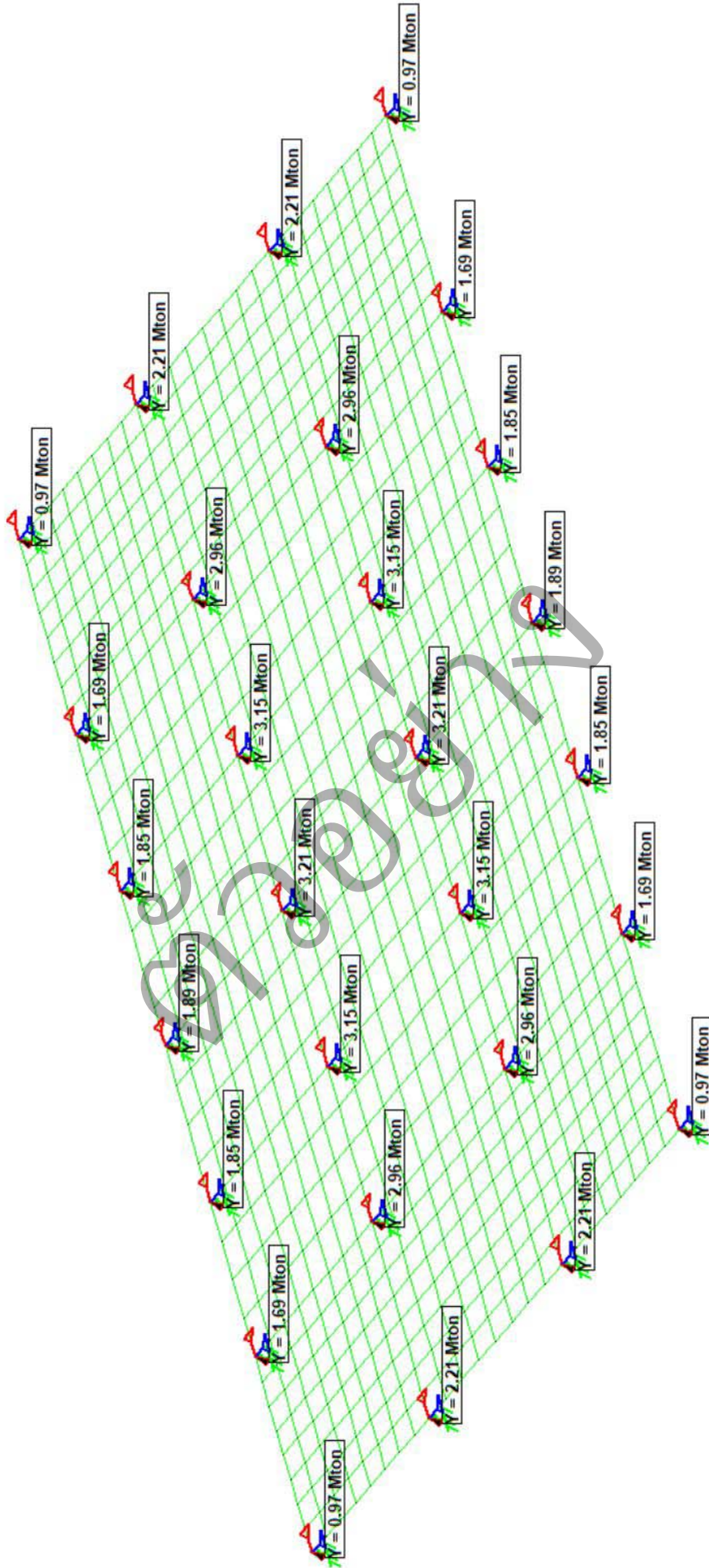
20/01/2021  
Max Bottom (Prin  
(Principal Major St  
Stress)  
kg/cm2



20/01/2021

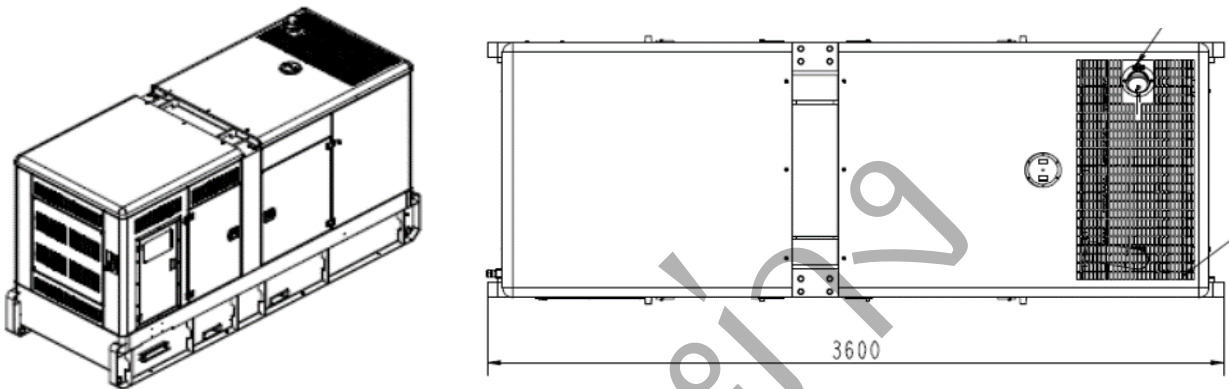
Max Top (Principi  
(Principal Major S  
Stress)  
Stress)  
kg/cm2



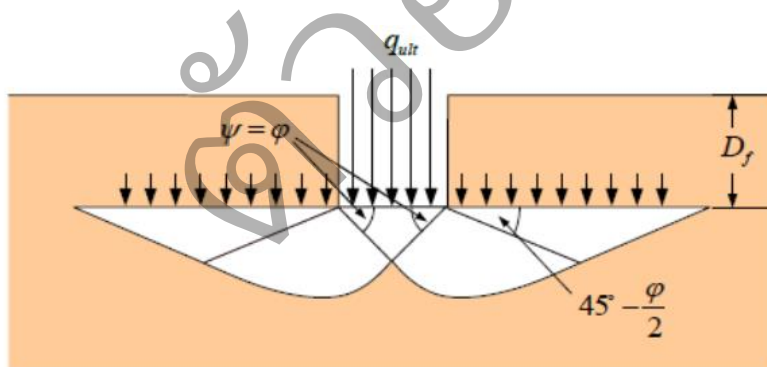


## RECHECK SOIL BEARING CAPACITY OF **DIESEL GENERATOR FOUNDATION**

foundation W = 1.80 m., L = 4.00 m.  
 area, A = 7.20 m<sup>2</sup>  
 equipment weight = 2.928 t  
 average weight = 0.41 t/m<sup>2</sup>  
 used W<sub>avg</sub> = 1.00 t/m<sup>2</sup>  
 line load = 0.41 t/m, used 0.50 t/m



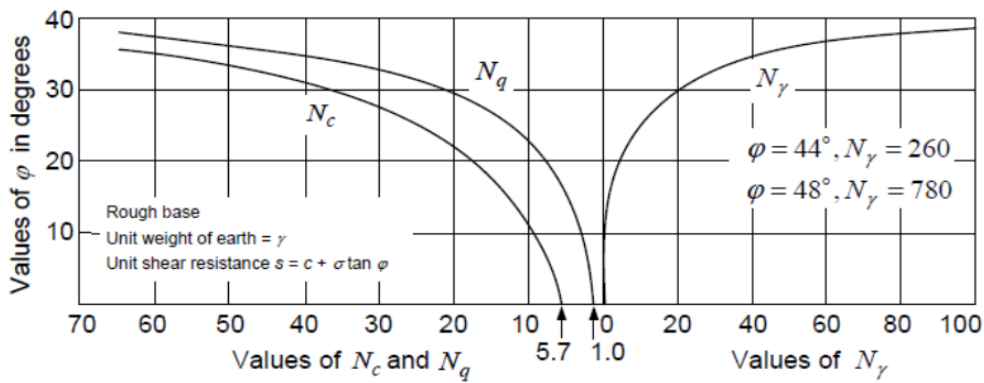
### Failure mechanism of Terzaghi



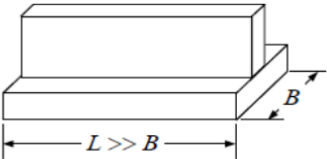
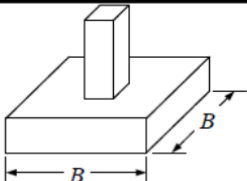
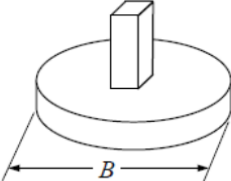
### Bearing capacity and bearing capacity factor equation of Terzaghi

Terzaghi	$q_{ult} = cN_c + qN_q + \frac{1}{2} \gamma BN_\gamma$	
$N_c = (N_q - 1) \cot \varphi$	$N_q = \exp^{2\left(\frac{3}{4}\pi - \frac{\varphi}{2}\right) \tan \varphi}$	$N_\gamma = \frac{\tan \varphi}{2} \left( \frac{K_{p\gamma}}{\cos^2 \varphi} - 1 \right)$

The relationship between bearing capacity factor and  $\phi$  (Terzaghi 1943)



Shape factors for bearing capacity equation

Footing type	Equation
 <p>Strip</p>	$q_{ult} = cN_c + qN_q + \frac{1}{2}\gamma BN_\gamma$
 <p>Square</p>	$q_{ult} = (1.3)cN_c + qN_q + (0.8)\frac{1}{2}\gamma BN_\gamma$
 <p>Circular</p>	$q_{ult} = (1.3)cN_c + qN_q + (0.6)\frac{1}{2}\gamma BN_\gamma$



### Bearing capacity equation

$\phi$	$N_c$	$N_q$	$N_\gamma$	$\phi$	$N_c$	$N_q$	$N_\gamma$
0	5.14	1.0	0.0	26	22.3	11.9	12.6
1	5.4	1.1	0.1	27	23.9	13.2	14.5
2	5.6	1.2	0.2	28	25.8	14.7	16.7
3	5.9	1.3	0.2	29	27.8	16.4	19.3
4	6.2	1.4	0.3	30	30.1	18.4	22.4
5	6.5	1.6	0.4	31	32.6	20.6	26.0
6	6.8	1.7	0.6	32	35.5	23.2	30.2
7	7.2	1.9	0.7	33	38.7	26.1	35.2
8	7.5	2.1	0.9	34	42.1	29.4	41.0
9	7.9	2.3	1.0	35	46.1	33.3	48.0
10	8.3	2.5	1.2	36	50.7	37.8	56.4
11	8.8	2.7	1.4	37	55.6	42.9	66.2
12	9.3	3.0	1.7	38	61.3	48.9	78.0
13	9.8	3.3	2.0	39	67.9	56.0	92.3
14	10.4	3.6	2.3	40	75.3	64.2	109.4
15	10.8	3.9	2.6	41	83.9	73.9	130.2
16	11.5	4.3	3.0	42	93.7	85.4	155.6
17	12.4	4.8	3.5	43	105.1	99.0	186.5
18	13.2	5.3	4.1	44	118.4	115.3	224.6
19	13.9	5.8	4.7	45	133.9	134.9	271.8
20	14.8	6.4	5.4	46	152.1	158.5	330.3
21	15.9	7.1	6.2	47	173.6	187.2	403.6
22	16.8	7.8	7.1	48	199.3	222.3	496.0
23	18.1	8.7	8.2	49	229.9	265.5	613.1
24	19.3	9.6	9.4	50	266.9	319.1	763.0
25	20.8	10.7	10.9	51	311.8	386.0	955.8

$$\gamma = 2.20 \text{ t/m}^3$$

$$\phi = 40.00$$

$$c = 0.00 \text{ t/m}^2$$

$$N_c = 75.31$$

$$N_q = 64.19$$

$$N_\gamma = 109.41$$

$$\text{foundation thickness} = 0.20 \text{ m.}$$

$$\gamma_c = 2.40 \text{ t/m}^3$$

$$cN_c = 0.00 \text{ t/m}^2$$

$$\text{shape factor} = 1.3$$

$$qN_q = 30.81 \text{ t/m}^2$$

$$\text{shape factor} = 1.8$$

$$1/2 \gamma B N_\gamma = 120.35 \text{ t/m}^2$$

$$Q_{ult} = (1.3)0 + (1.8)30.81 + 120.35$$

$$= 175.81 \text{ t/m}^2$$

$$\text{F.S.} = 3.00$$

$$Q_{all} = 58.60 \text{ t/m}^2$$

> Wavg OK

## Soil Spring

$$K_s = K_b \cdot A \quad \text{kg/m}$$

### Soil Subgrade Reaction

No	Subgrade	K (lb/in <sup>2</sup> )	Avg.	K <sub>b</sub> (kg/m <sup>3</sup> )
1	Plastic Clay	50 - 100	75	2,076,000
2	Silt and Silty Clay	100 - 200	150	4,152,000
3	Sands, Clayey Gravels	200 - 300	250	6,920,000
4	Gravel	300 or more	400	11,072,000
1 lb/in <sup>2</sup> = 27.68 g/cm <sup>3</sup> = 27,680 kg/m <sup>3</sup>				

$$W = 1.00 \quad \text{m}$$

$$L = 1.00 \quad \text{m}$$

$$A = 1.00 \quad \text{m}^2$$

$$K_b = 6,920,000 \quad \text{kg/m}^3$$

$$K_s = \boxed{6,920,000} \quad \text{kg/m}$$

Ks = 6,920,000 kg/m

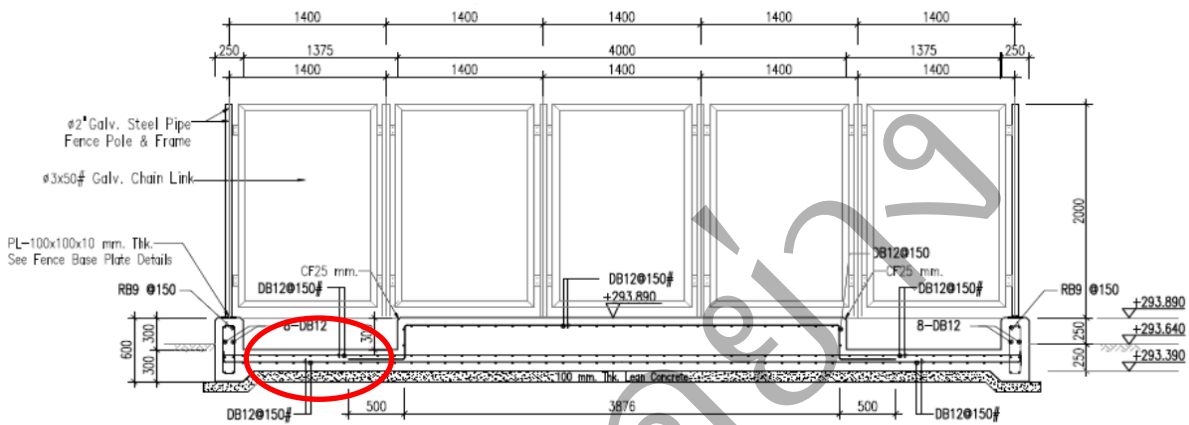
## DIESEL GENERATOR REINFORCEMENT

slab thickness = 0.20 m  
Mc =  $7.421 \times 1.00 \times (17^2)$  = 2,145 kg-m  
Mmax = 1,068 kg-m < Mc OK  
As =  $[(1068 \times 100)] / [(1700 \times 0.917 \times 17)]$   
= 4.03 cm<sup>2</sup>  
used DB- 12 mm @ 0.28 m , S = 0.15 m  
As = 7.54 cm<sup>2</sup>

คำนวณ

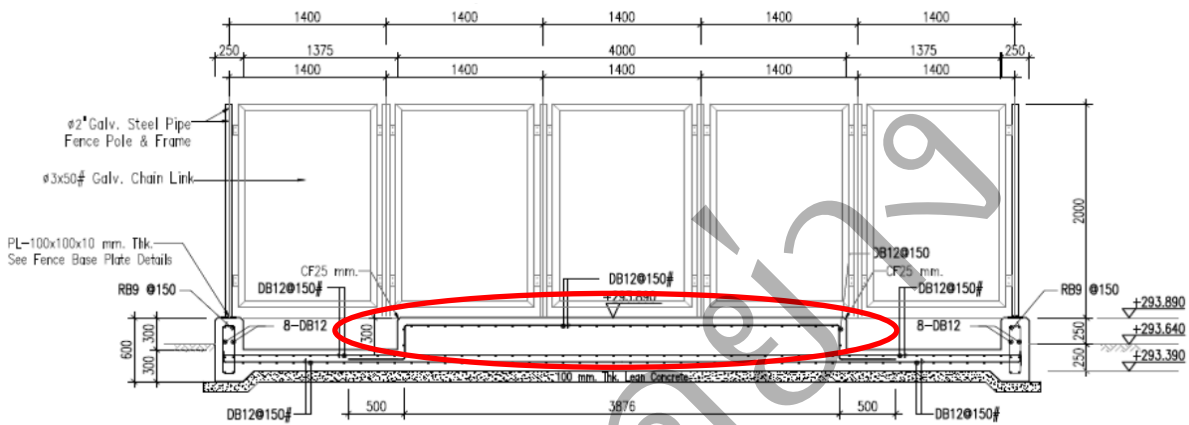
**Minimum Reinforcement for Slab 0.20 m.,thk.**

Wide =	1.00	m	thk. =	0.20	m
Area , A =	20x100	cm			
	= 2,000.00	cm <sup>2</sup>			
As-min =	2000x0.0018	cm	(จ.ส.ท.3407, SD40)		
	= 3.60	cm <sup>2</sup>			
Try DB-	12	mm @	3.18	bars	
Spacing	31.42	cm			
Used	15.00	cm			



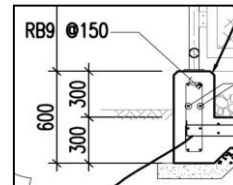
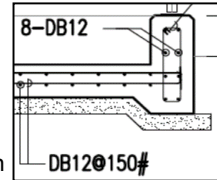
**Minimum Reinforcement for Slab 0.30 m.,thk.**

Wide =	1.00	m	thk. =	0.30	m
Area , A =	30x100	cm			
	= 3,000.00	cm <sup>2</sup>			
As-min =	3000x0.0018	cm	(จ.ส.ท.3407, SD40)		
	= 5.40	cm <sup>2</sup>			
Try DB-	12	mm @	4.77	bars	
Spacing	20.94	cm			
Used	15.00	cm			



**FENCE BEAM**

$W = 0.25$  m,  $D = 0.60$  m,  $d = 57$  cm  
 $L = 1.00$  m  
 selfweight =  $0.25 \times 0.6 \times 2,400 = 360$  kg/m  
 $SDL = 150$  kg/m (chain link weight)  
 Total load =  $510$  kg/m  
 $Mc = 12.646 \times 0.25 \times (57^2) = 10,272$  kg-m  
 $M_{max} = 64$  kg-m **< Mc OK**  
 $As = (63.75 \times 100) / (1700 \times 0.895 \times 57)$   
 $= 0.07$  cm<sup>2</sup>  
 $As_{-min} = (14 / 4000) \times 0.25 \times 57$   
 $= 4.99$  cm<sup>2</sup> **8-DB 12 mm. for As-min**  
 $DB- 12$  mm, no. of bar **2** bar  
 $As = 2.26$  cm<sup>2</sup>  
 used **2 - DB 12**  $As = 2.26$  cm<sup>2</sup> **> As OK**  
 $Vc = 0.29 \times \text{SQRT}(240) \times 0.25 \times 57$   
 $= 6,402$  kg  
 $V_{max} = 255$  kg **< Vc OK**  
 Used RB- **9** mm, Str. = **1** set  
 $As_{,str} = 1.27$  cm<sup>2</sup>  
 $S = (1.27 \times 1200 \times 57) / (255 - 6402)$   
 $= -14.1$  Cm **15** Cm  
 Used **1 RB-9 mm @ 15** cm



Chain link size	1"	1 1/2"	2"	2 1/2"
No.10 (3.2mm.)	5.20	3.65	2.74	2.36
No.11 (2.8mm.)	4.27	2.93	2.34	1.85
No.12 (2.2mm.)	3.41	2.38	1.93	1.21

\* unit-kg/m<sup>2</sup>