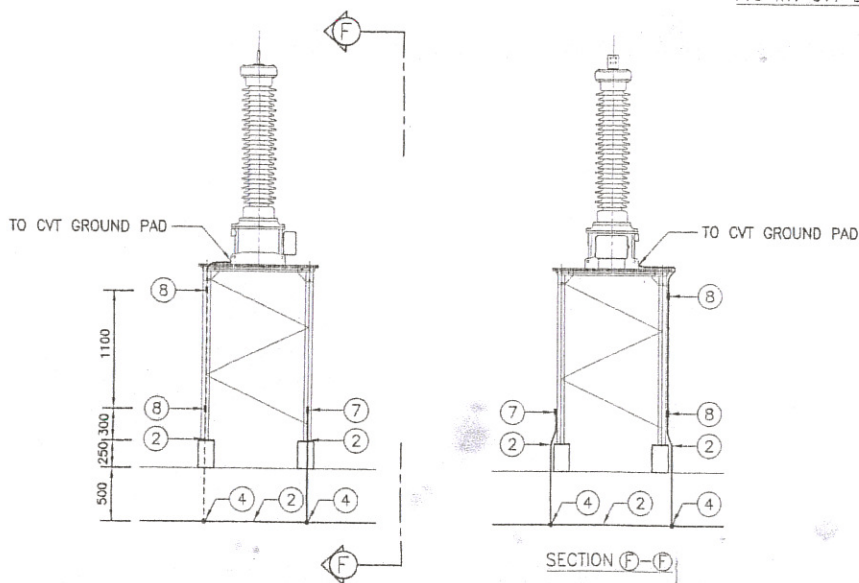
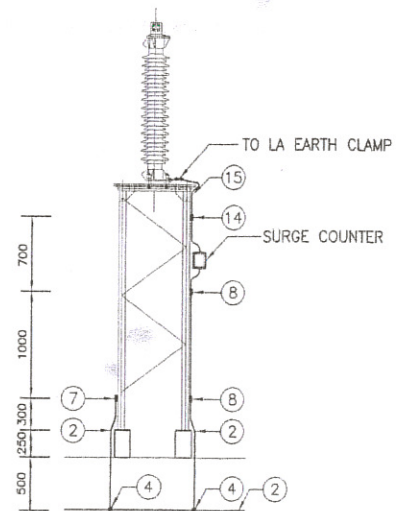


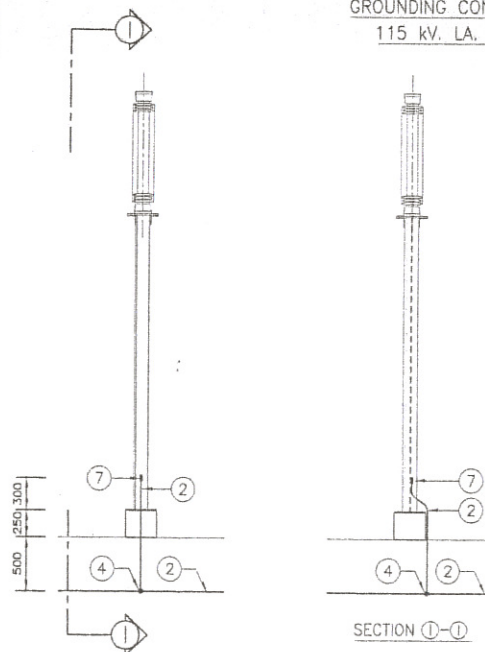
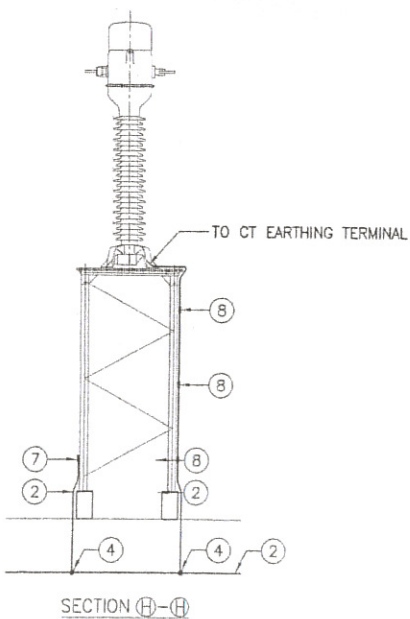
GROUNDING CONNECTION FOR  
115 kV. CVT LINE STRUCTURE



GROUNDING CONNECTION FOR  
115 kV. CVT BUS STRUCTURE (WITHOUT JUNCTION BOX)



GROUNDING CONNECTION FOR  
115 kV. LA. STRUCTURE



GROUNDING CONNECTION FOR  
115 kV. SUPPORT STRUCTURE FOR POST INSULATOR

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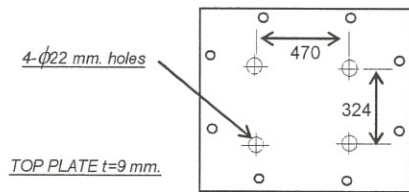
DESIGNED :  
CHECKED :

JOB NO.

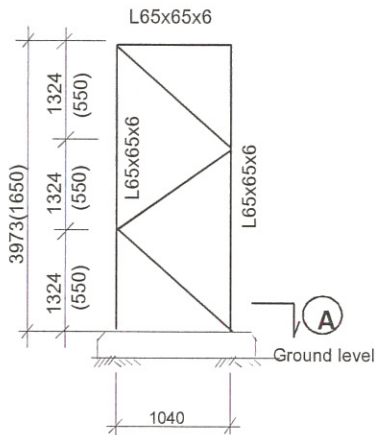
SUBJECT :115 KV. CAPACITOR VOLTAGE TRANSFORMER  
STRUCTURE

PAGE

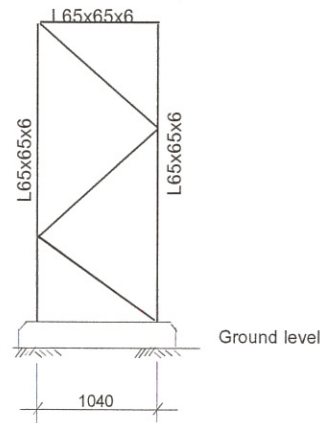
**1. STRUCTURAL DESIGN DRAWING**



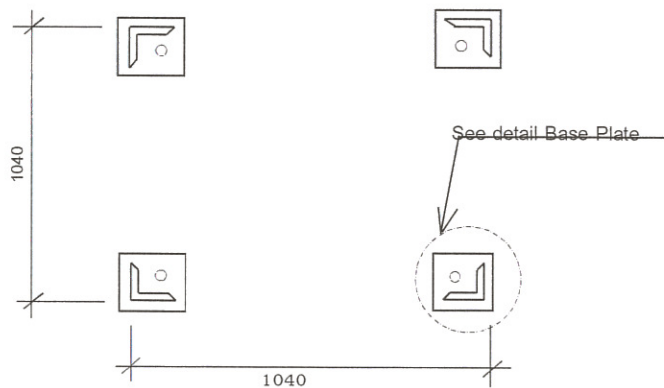
**TOP VIEW**



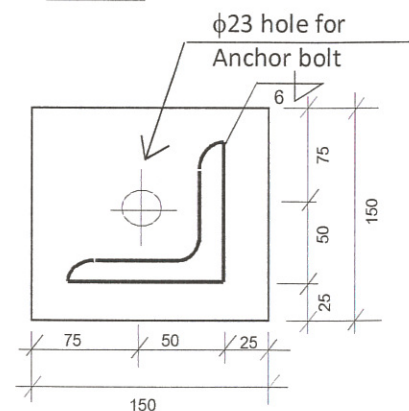
**FRONT VIEW**



**SIDE VIEW**



**SECTION A-A**



**BASE PLATE = 15 MM.**

**NOTES**

1. BLANK MEMBERS ARE L50x50x4
2. BLANK BOLTS ARE M16-1
3. NO INDICATED BOLT SIZE ARE M16
4. ALL DIMENSION ARE IN MILLIMETERS
5. ALL STRUCTURAL STEEL ARE JIS G3101 SS400
6. ALL BOLTS & NUTS ARE ASTM A394 TYPE 0

Total weight of steel structure = 350 kg.. (Approx. and included weight of bolts, plates nut, zinc)  
 Wind load on steel structure = 1x100x1.75 = 175 kg. (Shape factor = 1.75)

**2. Detail of equipment**

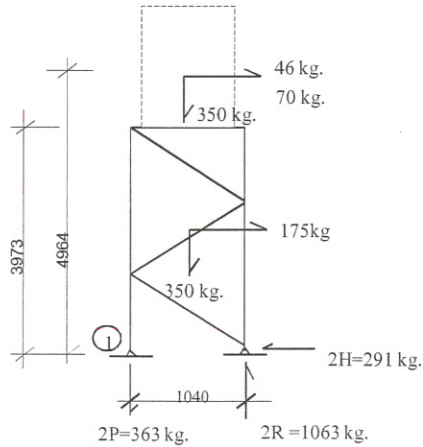
Item no.	Total height (mm.)	Height of equipment (mm.)	Height of steel structure (mm.)	Weight of equipment (kg.)
A5.3	5,954	1,981	3,973	350
	3,631	(1,981)	(1,650)	(APPROX.)

  
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DESIGNED :		JOB NO.	SUBJECT :115 KV. CAPACITOR VOLTAGE TRANSFORMER	PAGE
CHECKED :			STRUCTURE,	

Weight of equipment = 350 kg.  
Wind load on equipment = 1.981x0.35x67 (Approx. diameter equipment = 350 mm.)  
= 46 kg.  
Short circuit or dynamic load = 0.2xG  
= 0.2x350 = 70 kg.  
Center of gravity = 991 mm.

### 3. Analysis and design



$$\sum M \text{ AROUND } 1 = 0$$

$$2R \times 1.04 = (350+350) \times 1.04/2 + (46+70) \times 5.091 + 175 \times 3.973/2$$

$$2R = 1,238 \text{ kg.}$$

$$\sum F_y = 0$$

$$2P = 1,238 - (350+350)$$

$$= 538 \text{ kg.}$$

$$\sum F_x = 0$$

$$2H = (46+70+175)$$

$$= 291 \text{ kg.}$$

Maximum compression in bracing =  $H/(1,040/1,684)$   
=  $(291/2)/(1,040/1,684)$   
= 236 kg./bracing

Maximum compression in post = C  
= 1,238/2  
= 619 kg./leg

#### 3.1 Design post

Assume post size L65x65x6, unit weight = 5.91 kg/m., sectional area = 7.527 cm<sup>2</sup>.

radius of gyration Rx = 1.98 cm. Rv = 1.27 cm.

Maximum unsupported length Lx = 273 cm. Lv = 273 cm.

Maximum compression in post = 619 kg.

$$KL_x/R_x = (1)(265)/1.98 = 133.84$$

$$KL_v/R_v = (1)(133)/1.27 = 104.72$$

$$C_c = \sqrt{\frac{2\pi^2 E}{F_y}} = 126.91 < KL/R$$

Allowable compressive stress

Fa = 586 ksc. (AISC 1.5-2)

Allowable compressive strength = FaxArea = 586x7.527 = 4,411 kg.  
> 619 kg.. OK.

So we can use post size L65x65x6

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DESIGNED :		JOB NO.	SUBJECT :115 kV. CAPACITOR VOLTAGE TRANSFORMER	PAGE
CHECKED :			STRUCTURE,	

### 3.2 Design bracing

Assume bracing size L50x50x4, unit weight =3.06 kg/m, sectional area =3.892 cm<sup>2</sup>.

,radius of gyration Rx = 1.53 cm. Rv = 0.983 cm.

Maximum unsupported length Lx = 172cm. Lv = 172 cm.

Maximum compression in bracing	=	236	kg.
$KLx/Rx$	=	$(1)(168)/1.53$	= 109.8
$KLv/Rv$	=	$(1)(164)/0.983$	= 166.84
$Cc$	=	$\sqrt{2\pi^2 E/Fy}$	= 126.91 < KL/R

Allowable compressive stress

$Fa$	=	378 ksc.	.....	(AISC 1.5-2)
------	---	----------	-------	--------------

Allowable compressive strength	=	$Fa \times Area$	=	$378 \times 3.892$	=	1471	kg.
			>	236	kg.		OK.

So we can use bracing size L50x50x4

### Check bolts connection

Assume use bolt connection size M16-1

Allowable bearing strength (on the contact area)	=	$0.9 \times 2,500 \times 1.6 \times 0.4$	
		= 1,440	kg. > 236 OK.

Allowable shear on bolt	=	$0.22 \times 5,203 \times \pi \times (1.6)^2 / 4$	
		= 2,300	kg. > 236 OK.

Allowable bearing on bolt	=	$0.6 \times 5,203 \times 1.6 \times 0.4$	
		= 1,998	kg. > 236 OK.

So we can use bolt connection size M16-1

### 3.3 Design base plate and anchor bolt

Maximum compression	=	C	=	619	kg./post
---------------------	---	---	---	-----	----------

Maximum tension	=	T	=	269	kg./post
-----------------	---	---	---	-----	----------

Allowable bearing stress on concrete $Fc$	=	43.75	ksc.
---	---	-------	------

Bearing stress on base plate	=	$619 / (15 \times 15)$	= 2.75	ksc.
			< 43.75	OK.

Uniform load on base plate (from tension)	=	$269 / (12.5^2)$	ksc.
		= 1.72	ksc.

Max. bending moment	=	$0.29 \times 1.72 \times 12.5^2$	
		= 77.94	kg-cm/cm.

Min. plate thickness	=	$\sqrt{6 \times 77.94 / (0.75 \times 2500)}$	
		= 0.50	cm.

So we can use base plate 15 mm. Thickness

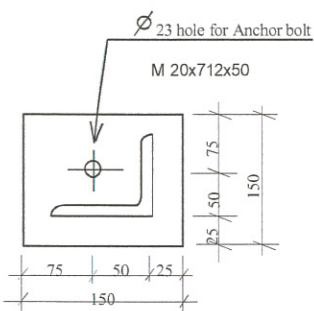
Assume use anchor bolt size M20x712x50, embeded length = 60 cm.,JIS G3101 SS400  $Fu = 4,100$  ksc.

Allowable bonding stress	=	10	ksc.
--------------------------	---	----	------

Allowable bonding strength	=	$\pi \times 2.0 \times 60 \times 10$	=	3,768	kg. > 269	kg. Ok.
----------------------------	---	--------------------------------------	---	-------	-----------	---------

Allowable tensile strength	=	$0.33 \times Fu \times Area$	=	$0.33 \times 4,100 \times \pi \times 2.0^2 / 4$		
			=	4,248	kg. > 269	kg. Ok.

So we can use anchor bolt size M20x712x50 per leg.



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DESIGNED :		JOB NO.	SUBJECT :115 kV. CAPACITOR VOLTAGE TRANSFORMER	PAGE
CHECKED :			STRUCTURE,	

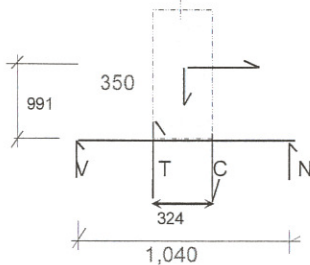
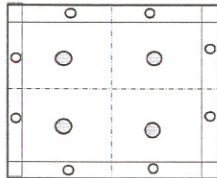
### Check welding

Assume use welding 6 mm fillet

Max. horizontal force	=	291/2	=	146	kg.
Max. tension	=	538/2	=	269	kg.
Welding length			=	26	cm.
Shearing stress Fv1			=	146/(26x0.6x0.707)	
			=	13.2	ksc.
Shearing stress Fv2			=	269/(26x0.6x0.707)	
			=	24.4	ksc.
Combine shearing stress			=	$\sqrt{13.2^2 + 24.4^2}$	
			=	27.8	ksc.
Allowable shearing stress Fv			=	1260	ksc. > 27.8
					ksc. <b>Ok.</b>

So we can use 6 mm. Fillet weld

### 3.4 Design top plate and beam

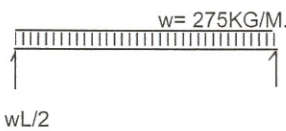


From load diagram				
C	=	(46+70)x0.991/0.324+350/2		kg.
	=	530		kg.
T	=	(46+70)x0.991/0.324-350/2		kg.
	=	180		kg.
Uniform load on top plate	=	530/(104x104/2)		
	=	0.10		ksc.
Bending moment M=wL <sup>2</sup> /8		0.10x104 <sup>2</sup> /8		kg-cm/cm.
	=	135		kg-cm/cm.
t	=	(6x135/(0.75x2,500)) <sup>0.5</sup>		cm.
	=	0.66		cm.

So we can use top plate 9. mm thickness

Assume beam size L65x65x6, unit weight =5.91 kg/m., sectional area =7.527 cm<sup>2</sup>.,modulus of section

Zx = Zy = 6.26 cm<sup>3</sup>., moment of inertia Ix = Iy =29.4 cm<sup>4</sup>.



Uniform load on beam	=	((46+70)x0.991/1.04+350/2)/1.04		kg/m				
	=	275		kg/m				
Max. moment	=	wL <sup>2</sup> /8		kg-m				
	=	(275+5.91)x1.04 <sup>2</sup> /8		kg-m				
	=	38		kg-m				
Bending stress fb	=	M/Z	=	38x100/6.26	=	607	ksc.	
Allowable bending stress Fb			=	0.66Fy	=	1,650	> 607	ksc. <b>OK.</b>
Allowable deflection	=	L/360	=	104/360	=	0.289	cm.	
Actual deflection	=	5WL <sup>4</sup> /384EI	=	5x(275+5.91)/100x104 <sup>4</sup> /384EI				
			=	0.071	<	0.289	<b>OK.</b>	

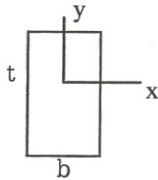
So we can use beam size L65x65x6

Structure : CVT Column

Project :

Date :

Location : Han Ka Substation



Square Section

**INPUT:**

**Material Properties**

Concrete  $f_c'$  (Cylinder) 210 ksc  
 Reinforcing Steel SD 30 and SR 24

**Loading**

Axial load , P 400 kg  
 Moment ,  $M_x$  0 kg-m  
 Moment ,  $M_y$  0 kg-m  
 Reduction Factor 1.00

**Dimension**

Length of Column 1.25 m

Section

Thickness; t 0.15 m

Width; b 0.15 m

$A_g$  0.02  $m^2$

% steel ,  $p_g$  0.020

Total Steel required ,  $A_{st}$  4.5  $cm^2$

Input:  $A_{st} = 4 \text{ DB } 12$  4.5  $cm^2$

$h/b$  8.3 <15

**COMPUTATION: <<Consider as Short Column>>**

$e_x = M_x / P$  - cm

$e_y = M_y / P$  - cm

$e_{bx} = [0.67 p_g m + 0.17](t - d')$  3.96 cm

$e_{by} = [0.67 p_g m + 0.17](b - d')$  3.96 cm

$e_{ax} = M_{sx} / (P_a - 1/P_o)$  0.07 cm

$e_{ay} = M_{sy} / (P_a - 1/P_o)$  0.07 cm

$P_a = 0.85 A_g (0.25 f_c' + f_s p_g)$  6,187 kg

$P_o = F_a A_g$  21,489 kg

$I_x = 1/12 b t^3 + (2n - 1) A_{st} (g t)^2 / 4$  4,691  $cm^4$

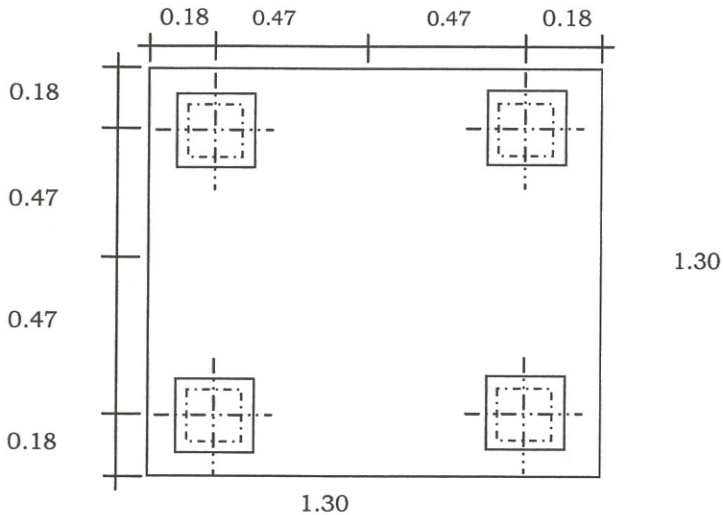
$I_y = 1/12 t b^3 + (2n - 1) A_{st} (g t)^2 / 4$  4,691  $cm^4$

$S_x = I_x / c_x$  626  $cm^3$

$S_y = I_y / c_y$  626  $cm^3$

$M_{sx} = F_b S_x$  591 kg-m

**Structure :** CVT Support Foundation  
**Project :** PEA Substations  
**Location :** Han Ka Substation  
**Date :**



**Dimension :**

<b>Abutment :</b>	bx	0.15	m
	by	0.15	m
	Depth	1.50	m
<b>Piles :</b>	SQ 0.15 x 0.15 x 3.0 m		
	Width / Diameter of Piles	0.15	m

**Materials Properties :**

Concrete :	fc' (28-day concrete cylinder)	210	ksc
Reinforcing Steels :	SD 30 and SR 24		

**Load :**

Column Load	1.25	Ton	
Bending Moment	0.50	Ton.m	
Horizontal Force	0.00	Ton	
Weight of Footing	0.27	Ton	
Total	2.05	Ton	
Number of Piles	4	Piles	
Each Pile Carry Load	0.51	Ton	
Compression 1	0.58	Ton	: PASS
Compression 2	0.05	Ton	

**Depth of Footing:**

Mmax	1088	kg.m
Required Depth of Footing	10	cm
Use Depth	13	cm
Thickness of Footing	20	cm

**Check Overturning:**

Overturning Moment	0.50	Ton.m
Resisting Moment		
Soil Weight Above Footing	2.14	Ton.m
Footing Weight	0.38	Ton.m
Pile Friction	5.64	Ton.m
Compression Load	0.59	Ton.m
Total Resisting Moment	8.75	Ton.m

**Check Shear:****Beam Type Shear**

x	2.0	cm	
P'	0.3	Ton	
V	0.7	Ton	
v	0.39	ksc	< v <sub>c</sub> : PASS
v <sub>C</sub>	4.20	ksc	

**Punching Shear**

Width of footing at distance d/2 from face of column	28.00	m	
x <sub>1</sub>	8.5	cm	
P <sub>1</sub> '	0.5	Ton	
V	1.8	Ton	
v	1.24	ksc	< v <sub>p</sub> : PASS
v <sub>P</sub>	7.68	ksc	

**Reinforcement:****Long Bar**

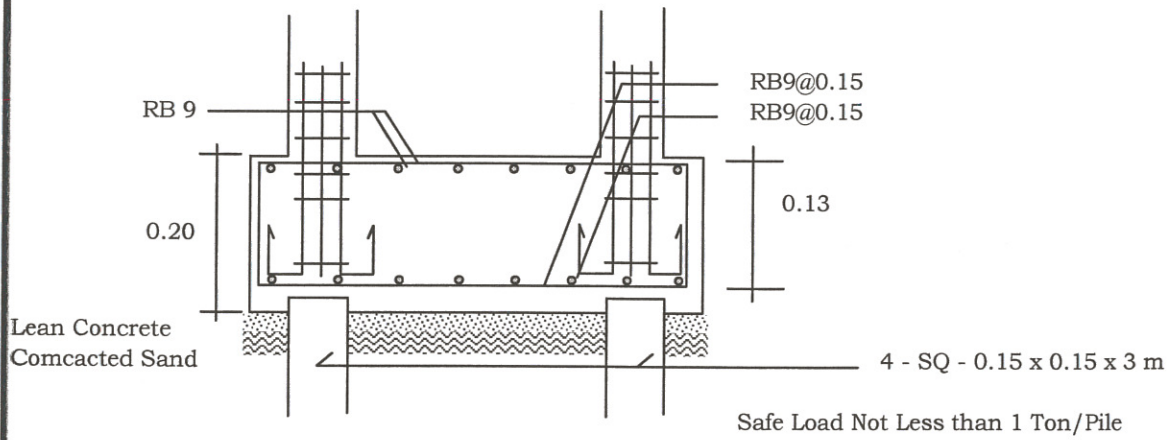
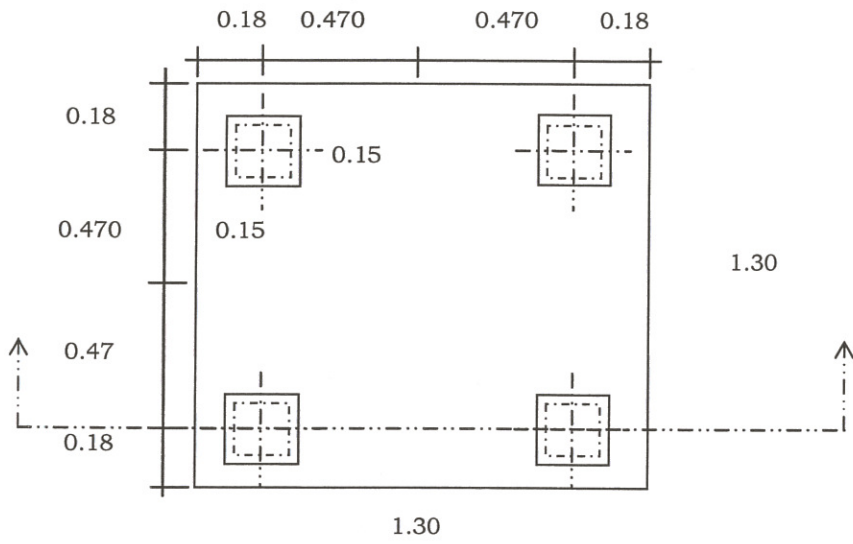
Min. As	5.20	cm <sup>2</sup>	
Req. As	6.33	cm <sup>2</sup>	
Allowable Bond Stress	35.20	ksc	
Required Perimeter	2.87	cm	
Use	RB 9 @ 0.15		
As	3.82	cm <sup>2</sup>	
Total Actual Perimeter	16.96	cm	
Spacing	15.00	cm	
Development Length	4.8	cm	
Actual Anchorage Length	50.5	cm	> 1.25L <sub>d</sub> : PASS

**Short Bar**

Min As	5.20	cm <sup>2</sup>	
Req. As	6.33	cm <sup>2</sup>	
Allowable Bond Stress	35.20	ksc	
Required Perimeter	2.87	cm	
Use	RB 9 @ 0.15		
As	3.82	cm <sup>2</sup>	
Total Actual Perimeter	16.96	cm	
Spacing	15.00	cm	
Development Length	4.8	cm	
Actual Anchorage Length	50.5	cm	> 1.25L <sub>d</sub> : PASS

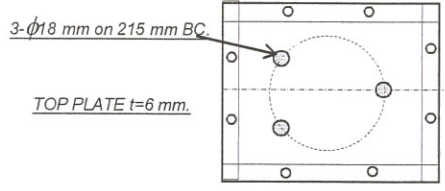


**Footing Plan and Section:**



DESIGNED :		JOB NO.	SUBJECT : LIGHTNING ARESSTER	PAGE
CHECKED :			SUPPORTING STRUCTURE	

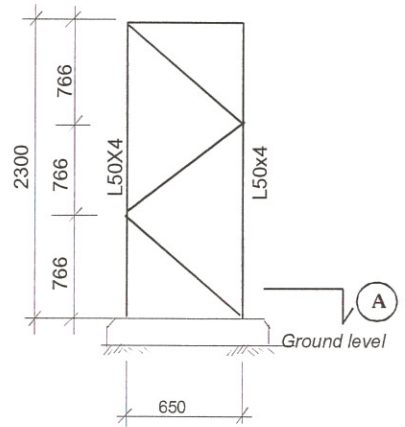
**1. STRUCTURAL DESIGN DRAWING**



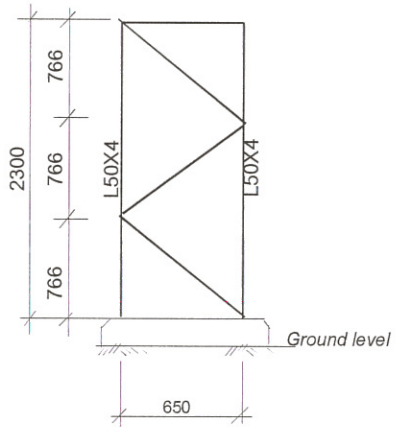
**TOP VIEW**

**NOTES**

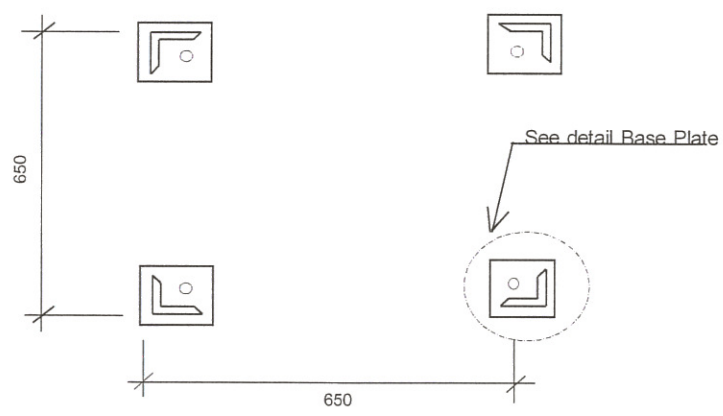
1. BLANK MEMBERS ARE L40x40x3
2. BLANK BOLTS ARE M16-1
3. NO INDICATED BOLT SIZE ARE M16
4. ALL DIMENSION ARE IN MILLIMETERS
5. ALL STRUCTURAL STEEL ARE JIS G3101 SS400
6. ALL BOLTS & NUTS ARE ASTM A394 TYPE 0



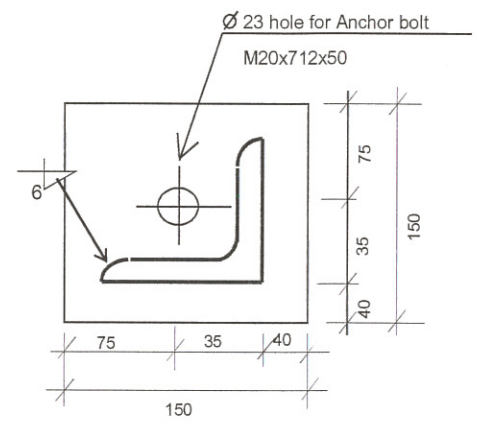
**FRONT VIEW**



**SIDE VIEW**



**SECTION A-A**




**BASE PLATE = 9 MM.**

Total weight of steel structure = 150 kg.. (Approx. and included weight of bolts, plates nut, zinc)  
 Wind load on steel structure = 1.0x100x1.75  
 = 175 kg. (Shape factor = 1.75)

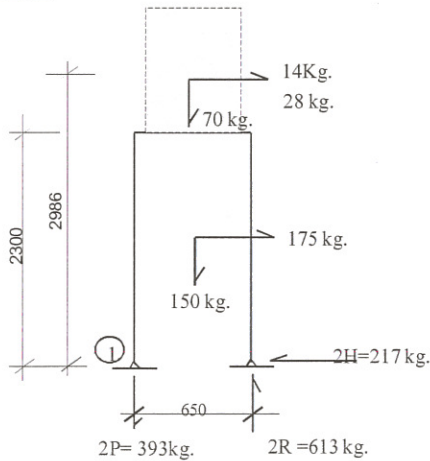
**2. Detail of equipment**

Item no.	Total height (mm.)	Height of equipment (mm.)	Height of steel structure (mm.)	Weight of equipment (kg.)
A3.2	3,672	1,372	2,300	70 (APPROX.)

  
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Weight of equipment = 70 kg.  
 Wind load on equipment = 1.372x0.3x67 (Approx. diameter equipment = 300 mm.)  
 = 28 kg.  
 Short circuit or dynamic load = 0.2xG  
 = 0.2x70 = 14 kg.  
 Center of gravity = 686 mm.

**3. Analysis and design**



**LOAD DIAGRAM**

$$\begin{aligned} \sum M \text{ AROUND } \textcircled{1} &= 0 \\ 2R \times 0.65 &= (150+70) \times 0.65/2 + (14+28) \times 2.986 \\ &\quad + 175 \times 2.3/2 \\ 2R &= 613 \text{ kg.} \\ \sum F_y &= 0 \\ 2P &= 613 - 150 - 70 \\ &= 393 \text{ kg.} \\ \sum F_x &= 0 \\ 2H &= 14 + 28 + 175 \\ &= 217 \text{ kg.} \end{aligned}$$

Maximum compression in bracing =  $H/(650/1,005)$   
 =  $217/2/(650/1,005)$   
 = 168 kg./bracing  
 Maximum compression in post = R  
 =  $613/2$   
 = 307 kg./leg

**3.1 Design post**

Assume post size L50x4 unit weight = 3.06 kg/m, sectional area = 3.892 cm<sup>2</sup>,  
 radius of gyration Rx = 1.53 cm. Rv = 0.983 cm.

Maximum unsupported length Lv = 153 cm.

Maximum compression in post = 307 kg.

$$\begin{aligned} KLx/Rx &= (1)(153)/(1.53) = 100 \\ KLv/Rv &= (1)(153)/0.983 = 155.64 \\ Cc &= \sqrt{2\pi^2 E/FY} = 126.91 > KL/R \end{aligned}$$

Allowable compressive stress

Fa = 907 ksc. (AISC 1.5-1)

Allowable compressive strength

= FaxArea = 907x3.892 = 3,530 kg  
 > 307 kg. OK.

So we can use post size L50x50x4

  
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DESIGNED :		JOB NO.	SUBJECT : LIGHTNING ARESSTER	PAGE
CHECKED :			SUPPORTING STRUCTURE	

### 3.2 Design bracing

Assume bracing size L40x40x3, unit weight =1.83 kg/m., sectional area =2.336 cm<sup>2</sup>.

,radius of gyration , Rv = 0.790cm.

Maximum unsupported length . Lv = 100.5 cm.

$$\text{Maximum compression in bracing} = 168 \text{ kg.}$$

$$KLv/Rv = (1)(100.5)/0.790 = 127.22$$

$$Cc = \sqrt{2\pi^2 E/Fy} = 126.91 < KL/R$$

Allowable compressive stress

$$Fa = 649 \text{ ksc.} \quad \text{.....} \quad \text{(AISC 1.5-2)}$$

$$\begin{aligned} \text{Allowable compressive strength} &= FaxArea = 649 \times 2.336 = 1516 \text{ kg.} \\ &> 168 \text{ kg.} \quad \text{OK.} \end{aligned}$$

So we can use bracing size L40x40x3

### Check bolts connection

Assume use bolt connection size M16-1

$$\begin{aligned} \text{Allowable bearing strength (on the contact area)} &= 0.9 \times 2,500 \times 1.6 \times 0.3 \\ &= 1,080 \text{ kg.} > 168 \text{ OK.} \end{aligned}$$

$$\begin{aligned} \text{Allowable shear on bolt} &= 0.22 \times 5,203 \times \pi \times (1.6)^2 / 4 \\ &= 2,300 \text{ kg.} > 168 \text{ OK.} \end{aligned}$$

$$\begin{aligned} \text{Allowable bearing on bolt} &= 0.6 \times 5,203 \times 1.6 \times 0.3 \\ &= 1,498 \text{ kg.} > 168 \text{ OK.} \end{aligned}$$

So we can use bolt connection size M16-1

### 3.3 Design base plate and anchor bolt

$$\text{Maximum compression} = C = 307 \text{ kg./post}$$

$$\text{Maximum tension} = T = 197 \text{ kg./post}$$

$$\text{Allowable bearing stress on concrete } fc = 43.75 \text{ ksc.}$$

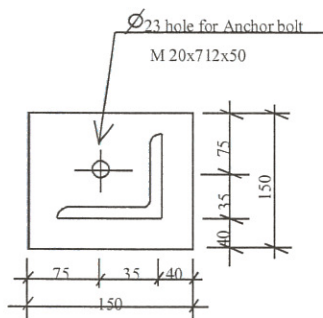
$$\begin{aligned} \text{Bearing stress on base plate} &= 307 / (15 \times 15) = 1.36 \text{ ksc.} \\ &< 43.75 \text{ OK.} \end{aligned}$$

$$\begin{aligned} \text{Uniform load on base plate (from tension)} &= 197 / (11^2) \text{ ksc.} \\ &= 1.6 \text{ ksc.} \end{aligned}$$

$$\begin{aligned} \text{Max. bending moment} &= 0.29 \times 1.6 \times 11^2 \\ &= 56 \text{ kg-cm/cm.} \end{aligned}$$

$$\begin{aligned} \text{Min. plate thickness} &= \sqrt{6 \times 56 / (0.75 \times 2500)} \\ &= 0.42 \text{ cm.} \end{aligned}$$

So we can use base plate 9 mm. Thickness



Assume use anchor bolt size M20x712x50, embeded length =60 cm.,JIS G3101 SS400 Fu = 4,100 ksc.

$$\text{Allowable bonding stress} = 10 \text{ ksc.}$$

$$\text{Allowable bonding strength} = \pi \times 2.0 \times 60 \times 10 = 3,768 \text{ kg.} > 197 \text{ kg. Ok.}$$

$$\begin{aligned} \text{Allowable tensile strength} &= 0.33 \times Fu \times Area = 0.33 \times 4,100 \times \pi \times 2.0^2 / 4 \\ &= 4,248 \text{ kg.} > 197 \text{ kg. Ok.} \end{aligned}$$

So we can use anchor bolt size M20x712x50 per leg.

DESIGNED :		JOB NO.	SUBJECT : LIGHTNING ARESSTER	PAGE
CHECKED :			SUPPORTING STRUCTURE	

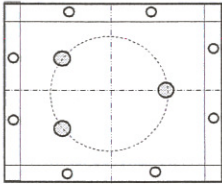
**Check welding**

Assume use welding 6 mm fillet

Max. horizontal force	=	217/2	=	109	kg.
Max. tension	=	393/2	=	197	kg.
Welding length			=	20	cm.
Shearing stress Fv1			=	109/(20x0.6x0.707)	
			=	12.8	ksc.
Tensile stress Fv2			=	196/(20x0.6x0.707)	
			=	23.2	ksc.
Combine shearing stress			=	$\sqrt{12.8^2+23.2^2}$	
			=	26.5	ksc.
Allowable shearing stress Fv			=	1260	ksc. > 26.5 ksc. <b>Ok.</b>

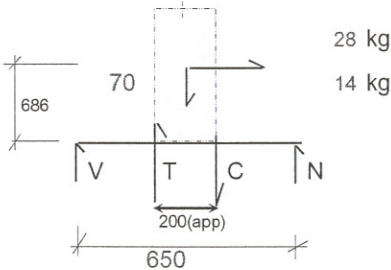
So we can use 6 mm. Fillet weld

**3.4 Design top beam**



From load diagram

C	=	(28+14)x0.686/0.20+70/2	
	=	179	kg.
T	=	(28+14)x0.686/0.20-70/2	
	=	109	kg.



Uniform load on top plate	=	179/(65x65/2)	
	=	0.08	ksc.
Bending moment M	=	0.08x65 <sup>2</sup> /8	kg-cm/cm.
	=	25	kg-cm/cm.
t	=	$(6x25/(0.75x2,500))^{0.5}$	cm.
	=	0.28	cm.

So we can use top plate 6 mm thickness

Assume beam size L40x40x3 unit weight 1.83 kg/m., sectional area =2.336 cm<sup>2</sup>, modulus of section

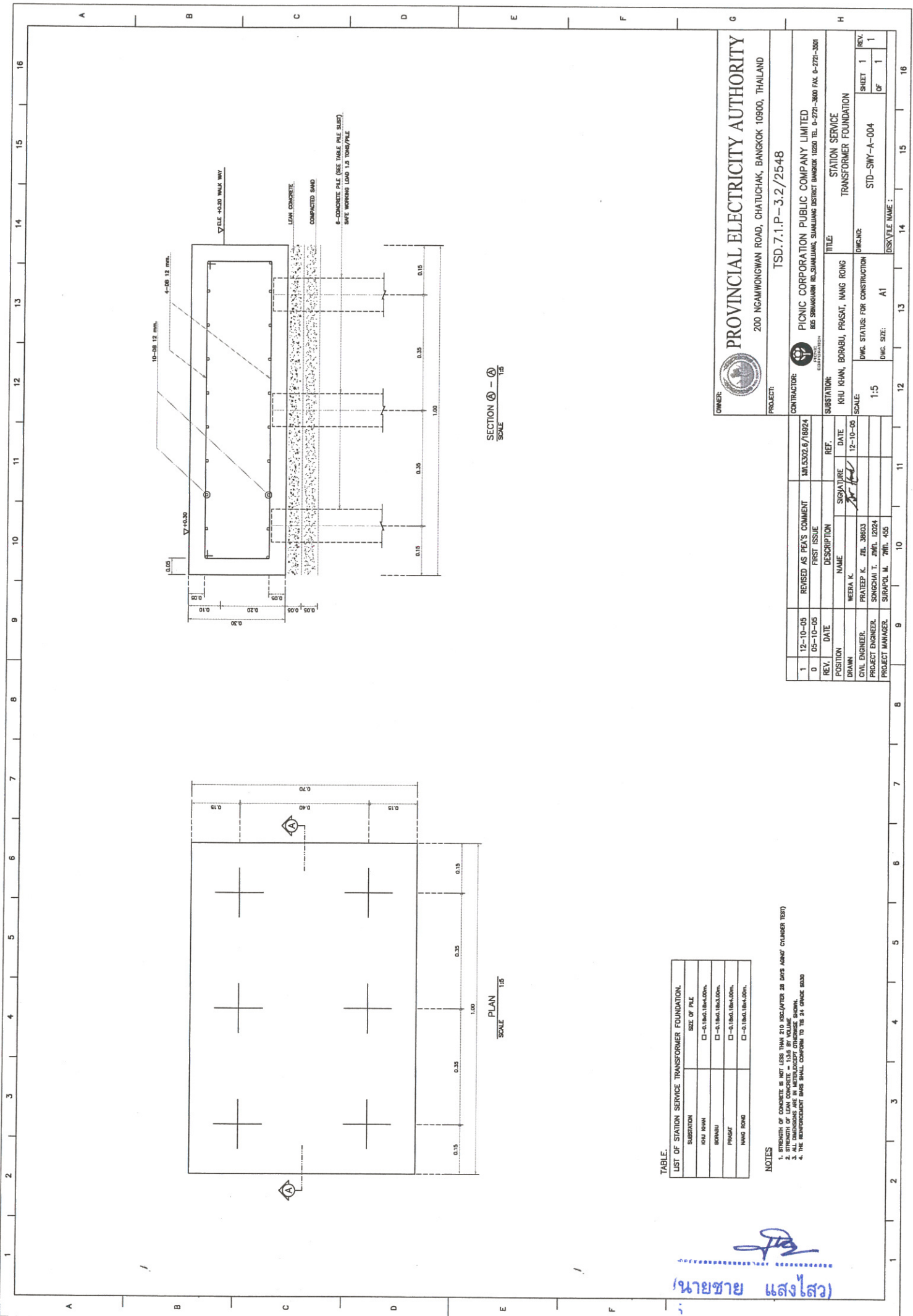
$\bar{Z}_x = \bar{Z}_y = 1.21 \text{ cm}^3$ , moment of inertia  $I_x = I_y = 3.53 \text{ cm}^4$ .

Uniform load on beam	=	((28+14)x0.686/0.65+70/2)/0.65	kg/m
	=	122	kg/m
Max. moment	=	$wL^2/8$	kg-m
	=	$(122+1.83)x0.65^2/8$	kg-m
	=	6.54	kg-m



Bending stress fb	=	M/Z	=	11x100/1.21	=	540	ksc.
Allowable bending stress Fb			=	0.66Fy	=	1,650	> 540 ksc. <b>OK.</b>
Allowable deflection	=	L/360	=	65/360	=	0.181	cm.
Actual deflection	=	$5WL^4/384EI$	=	$5x(122+1.83)/100x65^4/384EI$			
			=	0.040	<	0.181	<b>OK.</b>

So we can use beam size L40x40x3



SECTION A - A  
SCALE 1:5

PLAN  
SCALE 1:5

TABLE  
LIST OF STATION SERVICE TRANSFORMER FOUNDATION.

SUBSTATION	SIZE OF PILE
KHU KHAN	□-0.18x0.18x4.0m.
BORABU	□-0.18x0.18x3.0m.
PRANG	□-0.18x0.18x4.0m.
MANG RONG	□-0.18x0.18x4.0m.

- NOTES
1. STRENGTH OF CONCRETE IS NOT LESS THAN 24. (EXCEPT 28 DAYS AVERAGE CUMBER TEST)
  2. STRENGTH OF LEAN CONCRETE IS 12.5 BY VOLUME.
  3. ALL DIMENSIONS ARE IN METERS EXCEPT OTHERWISE SHOWN.
  4. THE REINFORCEMENT BARS SHALL CONFORM TO TB 24 GRADE 8000

OWNER: **PROVINCIAL ELECTRICITY AUTHORITY**  
200 NGAMWONGWAN ROAD, CHATUGHAK, BANGKOK 10900, THAILAND

PROJECT: TSD.7.1.P-3.2/2548

CONTRACTOR: **PICNIC CORPORATION PUBLIC COMPANY LIMITED**  
805 SINGHAKHAI RD. SANGKHAWI, SAMKANG DISTRICT BANGKOK 10250 TEL. 0-2771-3600 FAX. 0-2771-3501

SUBSTATION: KHU KHAN, BORABU, PRANG, MANG RONG  
TITLE: STATION SERVICE TRANSFORMER FOUNDATION

DESIGNER: WEEDA K. PRATEEP K. JEL. 38603  
PROJECT ENGINEER: SONGCHAI T. JML. 10224  
PROJECT MANAGER: SURAPOL M. JML. 455

DWG. STATUS FOR CONSTRUCTION  
DWG. NO.: STD-SWY-A-004  
DWG. SIZE: A1  
SCALE: 1:5

DESIGNER: WEEDA K. PRATEEP K. JEL. 38603  
PROJECT ENGINEER: SONGCHAI T. JML. 10224  
PROJECT MANAGER: SURAPOL M. JML. 455

REVISIONS:

REV.	DATE	DESCRIPTION	BY	DATE
1	12-10-05	REVISED AS PER A COMMENT	MR. S. S. S.	12-10-05
0	05-10-05	FIRST ISSUE	MR. S. S. S.	12-10-05

SHEET 1 OF 1

*(Signature)*  
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**Structure :** Station Service Transformer Foundation

**Project :**

**Location :** Han Ka Substation

**Date :**

**Material Properties:**

Concrete $f_c'$ (Cylinder)	210	ksc
Reinforcing Steel		
SD 30 SR 24		
Pile <input type="checkbox"/> 0.15 x 0.15 m x 3.00 m		

**Loading :**

Equipment Load	600	Kg
Maximum Bending Moment	7	kg.m
Maximum Shear Force	110	kg

**Dimension :**

No. of Pile	6	Piles
Distance between pile	0.55	m
Width	40	cm
Required Depth of Footing	1	cm
Use	23	cm
Thickness of Footing	30	cm

**Punching Shear :**

Perimeter	152	m
$v'$	0.031	ksc Pass

**Reinforcement :**

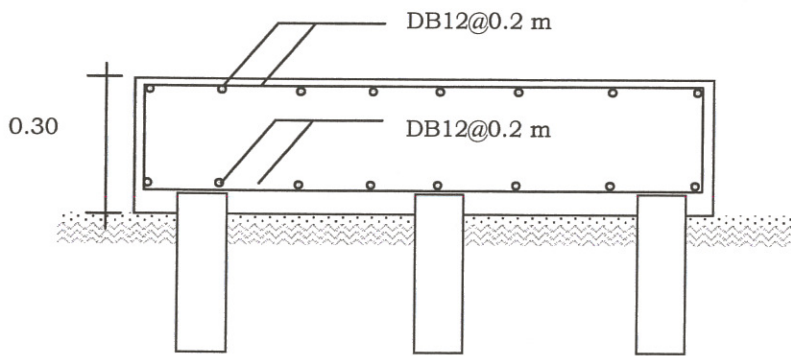
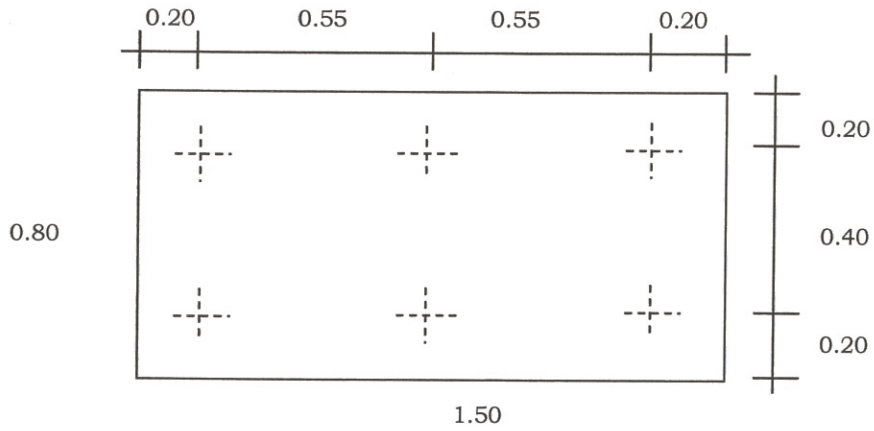
$M_R$	3155	kg.m
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Single Reinforcement

**Main Reinforcement :**

$A_{SR}$	0.02	cm <sup>2</sup>
Required $A_{ST}$	0.02	cm <sup>2</sup>
Use DB 12 @ 0.20		m
	5.65	cm <sup>2</sup>
Reinforcement Ratio	0.006	

**Footing Plan and Section :**

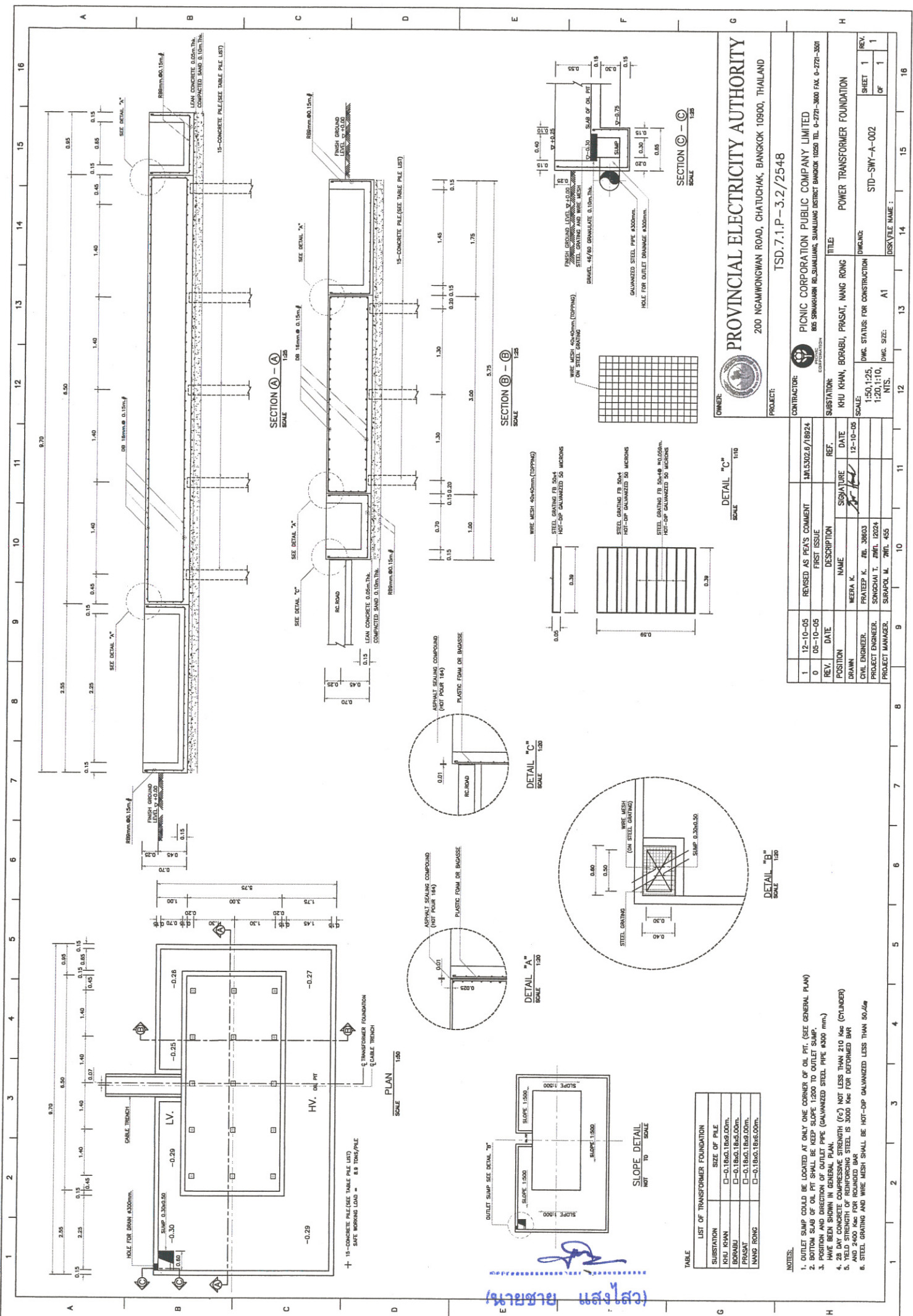


6 - SQ 0.15 x 0.15 x 3 m





POWER TRANSFORMER FOUNDATION WITH OIL GUTTER



OWNER: **PROVINCIAL ELECTRICITY AUTHORITY**  
 200 NGAIWONGWAN ROAD, CHATUCHAK, BANGKOK 10900, THAILAND

PROJECT: TSD.7.1.P-3.2/2548

CONTRACTOR:	<b>PICNIC CORPORATION PUBLIC COMPANY LIMITED</b> 888 SRINAKHON RU-SUWANNAK, SUWANNAKH DISTRICT BANGKOK 10250 TEL. 0-2771-3600 FAX. 0-2771-3501
SUBSTATION:	<b>KHU KHAN, BORABU, PRASAT, NANG RONG</b>
TITLE:	<b>POWER TRANSFORMER FOUNDATION</b>
SCALE:	1:50, 1:25, 1:20, 1:10, NTS.
DWG. STATUS:	FOR CONSTRUCTION
DWG. NO.:	STD-SWY-A-002
DWG. SIZE:	A1
DISK/FILE NAME:	

NO.	REV.	DATE	DESCRIPTION	SIGNATURE	DATE	REF.
1	12-10-05		REVISED AS PER COMMENT		12-10-05	
0	05-10-05		FIRST ISSUE			

POSITION	NAME	SIGNATURE	DATE
DRAWN	MEENA K.		12-10-05
CIVIL ENGINEER	PRATEEP K. JIL. 38603		
PROJECT ENGINEER	SANGCHAI T. JPHL. 12024		
PROJECT MANAGER	SURAPOL M. JPHL. 455		

TABLE  
LIST OF TRANSFORMER FOUNDATION

SUBSTATION	SIZE OF PILE
KHU KHAN	□-0.18x0.18x0.00m.
BORABU	□-0.18x0.18x0.00m.
PRASAT	□-0.18x0.18x0.00m.
NANG RONG	□-0.18x0.18x0.00m.

- NOTES:
- OUTLET SUMP SHALL BE LOCATED AT ONLY ONE CORNER OF OIL PIT. (SEE GENERAL PLAN)
  - BOTTOM SLAB OF OIL PIT SHALL BE KEPT SLOPE 1:200 TO OUTLET SUMP.
  - POSITION AND DIRECTION OF OUTLET PIPE (GALVANIZED STEEL PIPE #300 mm.) SHALL BE SHOWN IN GENERAL PLAN.
  - 20% OF REINFORCING BARS SHALL BE BENT UPWARDS (60°) NOT LESS THAN 210 mm (CYLINDER) AND 2400 mm FOR ROUNDED BAR.
  - YIELD STRENGTH OF REINFORCING STEEL IS 3000 N/mm<sup>2</sup> FOR UPBENTED BAR.
  - STEEL GRATING AND WIRE MESH SHALL BE HOT-DIP GALVANIZED LESS THAN 50.4um

(นายชาย แสงใส)

**Structure :** Transformer Foundation 25 MVA

**Project :**

**Location :** Han Ka Substation

**Date :**

**Material Properties:**

Concrete  $f_c'$  (Cylinder) 210 ksc  
Reinforcing Steel  
SD 30 SR 24  
Pile  $\square$  0.15 x 0.15 m x 4.00 m

**Loading :**

Equipment Load 64000 Kg  
Maximum Bending Moment 581 kg.m

**Dimension :**

No. of Pile 15 Piles  
Distance between pile 0.83 m  
Width 95 cm  
Required Depth of Footing 5 cm  
Use 63 cm  
Thickness of Footing 70 cm

**Punching Shear :**

Perimeter 312 m  
 $v'$  0.322 ksc Pass

**Reinforcement :**

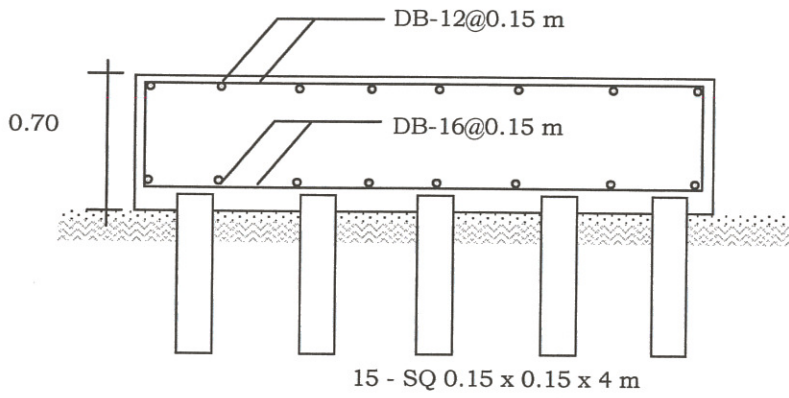
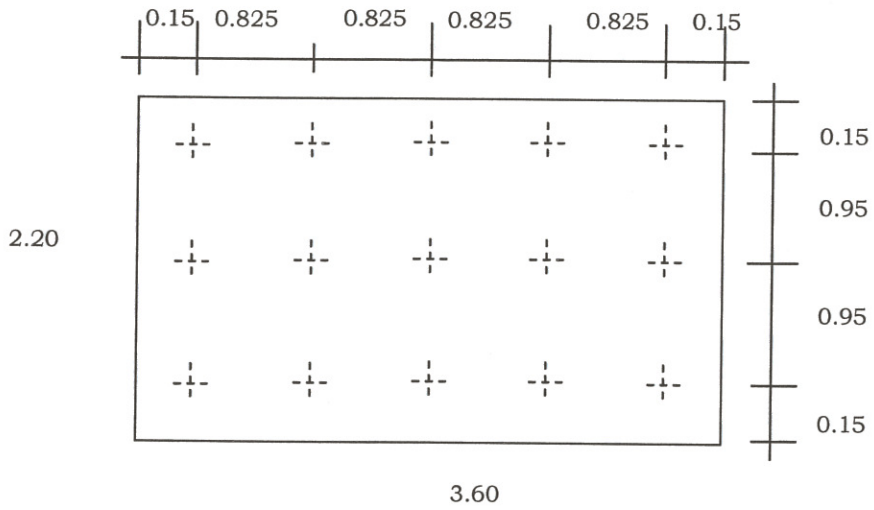
$M_R$  56225 kg.m

Single Reinforcement

**Main Reinforcement :**

$A_{SR}$  0.70  $cm^2$   
 $M'$  0 kg.m  
 $f_s'$  0 ksc  
 $A_{S1}$  0.00  $cm^2$   
Required  $A_{SC}$  0.00  $cm^2$   
Required  $A_{ST}$  0.70  $cm^2$   
Use  $A_{SC}$  : 2 DB 16 : 4.02  $cm^2$   
Reinforcement Ratio 0.0007  
Use DB 16 @ 0.15 m  
14.07  $cm^2$   
Reinforcement Ratio 0.002

**Footing Plan and Section :**



**Structure :** Oil Gutter  
**Project :**  
**Location :** Han Ka Substation  
**Date :**

**Material Properties:**

Concrete $f_c'$ (Cylinder)	210	ksc
Reinforcing Steel		
SD 30	SR 24	

**Gutter Slab**

**Loading :**

Maximum Bending Moment	200	kg.m
Maximum Shear Force	250	kg

**Dimension of Beam :**

Width of Gutter	145	cm
Required Depth of Gutter Slab	2	cm
Use	10	cm

**Reinforcement :**

$M_R$	2162	kg.m
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**Main Reinforcement :**

	$A_{SR}$	1.51	$cm^2$	
	$M'$	0	kg.m	
Required	$A_{ST}$	1.51	$cm^2$	
$A_{ST}$ :	RB - 9	:	1.91	$cm^2$
	Reinforcement Ratio	0.001		
USE	RB - 9	@	0.15	m

**Gutter Wall**

**Loading :**

Maximum Bending Moment	200	kg.m
Maximum Shear Force	250	kg

**Dimension of Beam :**

Required Depth of Gutter Wall	3	cm
Use	10	cm

**Reinforcement :**

$M_R$	1491	kg.m
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**Main Reinforcement :**

	$A_{SR}$	1.51	$cm^2$	
	$M'$	0	kg.m	
Required	$A_{ST}$	1.51	$cm^2$	
$A_{ST}$ :	RB - 9	:	1.91	$cm^2$
	Reinforcement Ratio	0.002		
	RB - 9	@	0.15	m

**Section :**

