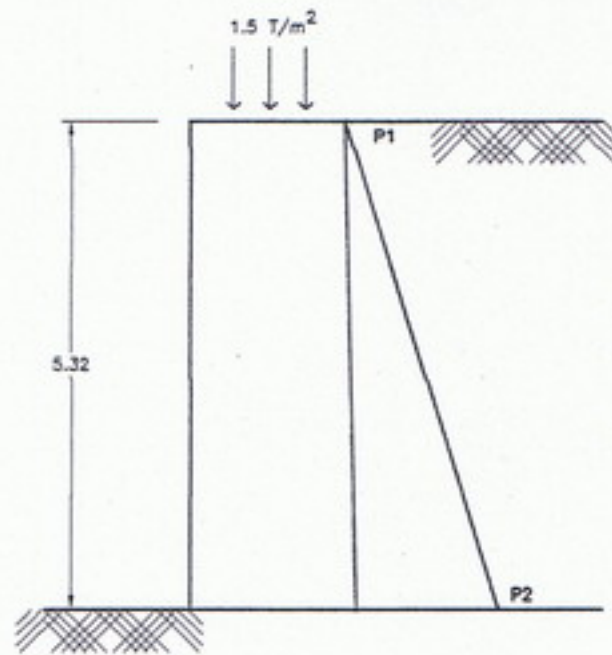


รายการคำนวณ

เชื่อกันดิน



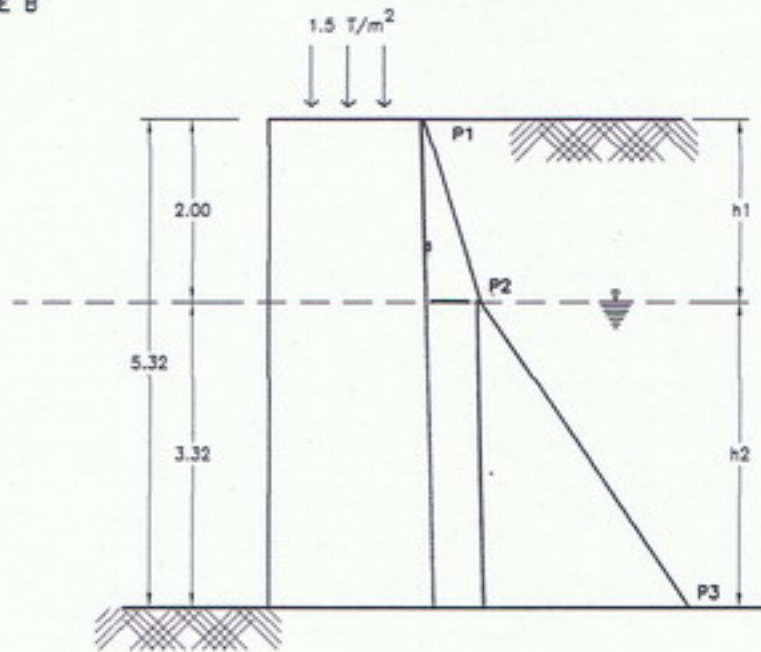
CASE A



$$\begin{aligned} \phi &= 33^\circ, C=0 \\ r &= 1,500 \text{ kg/m}^3 \\ r_{\text{sat}} &= 1,775 \text{ kg/m}^3 \\ r' &= 755 \\ k_a &= 0.295 \end{aligned}$$

$$\begin{aligned} P_1 &= K_a P \\ &= 0.295 \times 1,500 = 442.50 \text{ kg/m}^2 \\ P_2 &= P_1 + K_a r h \\ &= 442.50 + 0.295 (1,500 \times 4.92) \\ &= 2,620 \text{ kg/m}^2 \\ V_{\text{max}} &= \frac{1}{2} (442.50 + 2,620) 5.32 \\ &= 8,147 \text{ kg} \\ M_{\text{max}} &= 442.50 \times \frac{5.32^2}{2} + \frac{1}{2} (2,620 - 442.50) \frac{5.32^2}{3} \\ &= 16,534 \text{ kg-m} \end{aligned}$$

CASE B



$\phi = 33^\circ$, $C=0$
 $r = 1,500 \text{ kg/m}^3$
 $r \text{ sat} = 1,775 \text{ kg/m}^3$
 $r' = 775$
 $k_a = 0.295$

$$P_1 = K_a P$$

$$= 0.295 \times 1,500 = 442.50 \text{ kg/m}^2$$

$$P_2 = P_1 + K_a r h_1$$

$$= 442.50 + 0.295 (1,500 \times 2)$$

$$= 1,327.50 \text{ kg/m}^2$$

$$P_3 = P_2 + K_a r' h_2$$

$$= 1,327.50 + 0.295 (775 \times 3.32)$$

$$= 2,087 \text{ kg/m}^2$$

$$V_{\max} = \frac{1}{2} (442.50 + 1,327.50) \times 2 + \frac{1}{2} (1,327.50 + 2,087) \times 3.32$$

$$= 7,439 \text{ kg}$$

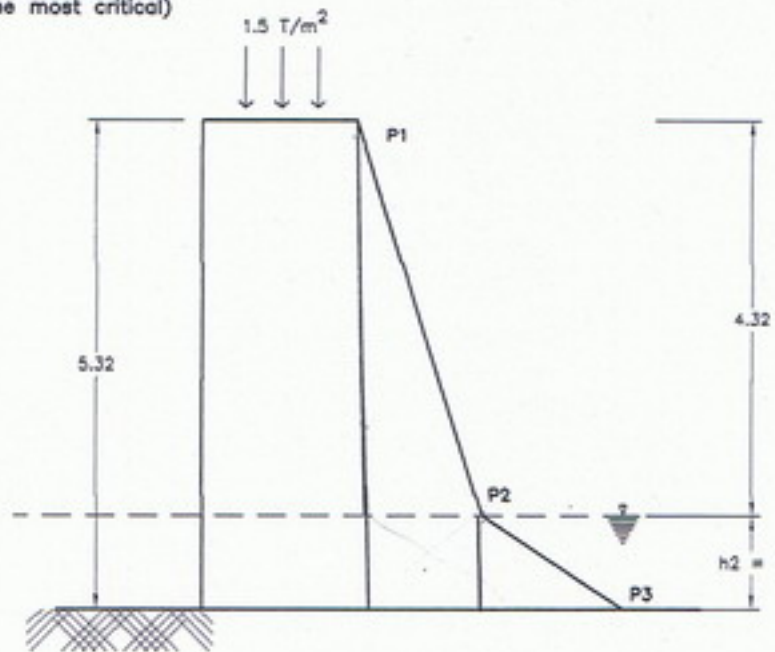
$$M_{\max} = \left(442.50 \times \frac{5.32^2}{2} \right) + \left(\frac{1}{2} (1,327.50 - 442.50) \times 2 \times \left(\frac{2}{3} + 3.32 \right) \right)$$

$$+ \left((1,327.50 - 442.50) \times \frac{3.32^2}{2} \right) + \left(\frac{1}{2} (2,087 - 1,327.50) \times 3.32 \times \left(\frac{3.32}{3} \right) \right)$$

$$= 6,261.91 + 3,528.20 + 4,877.42 + 1,395.25$$

$$= 16,063 \text{ kg} \cdot \text{m}$$

CASE C(The most critical)



$\phi = 33^\circ; C=0$
 $r = 1,500 \text{ kg/m}^3$
 $r_{\text{sat}} = 1,775 \text{ kg/m}^3$
 $r' = 775$
 $k_a = 0.295$

$$\begin{aligned}
 P_1 &= K_a P \\
 &= 0.295 \times 1,500 = 442.50 \text{ kg/m}^2
 \end{aligned}$$

$$\begin{aligned}
 P_2 &= P_1 + K_a r h \\
 &= 442.50 + 0.295 (1,500 \times 4.32) \\
 &= 2,354 \text{ kg/m}^2
 \end{aligned}$$

$$\begin{aligned}
 P_3 &= P_2 + K_a r' h_2 + r_w \\
 &= 2,354 + 0.295 (775 \times 1) + 1,000(1) \\
 &= 3,583 \text{ kg/m}^2
 \end{aligned}$$

$$\begin{aligned}
 V_{\text{max}} &= \frac{1}{2} (442.50 + 2,354) 4.32 + \frac{1}{2} (2,354 + 3,583) 1 \\
 &= 9,009 \text{ kg}
 \end{aligned}$$

$$\begin{aligned}
 M_{\text{max}} &= \left(442.50 \times \frac{5.32^2}{2} + \left(\frac{1}{2} (2,354 - 442.50) 4.32 \times \left(\frac{4.32}{3} + 1 \right) \right) \right. \\
 &\quad \left. + \left((2,354 - 442.50) \times 1 \times 0.50 \right) + \left(\frac{1}{2} (3,583 - 2,354) \times 1 \times \frac{1}{3} \right) \right) \\
 &= 6,261.91 + 10,074.37 + 995.75 + 204.83 \\
 &= 17,500 \text{ kg-m}
 \end{aligned}$$

Case	M_{\max} (kg-m)	V_{\max} (kg)
A	16,534	8,147
B	16,063	7,439
C	17,500	9,009
USE	17,500	9,009

Design Wall

USE $f_c' = 200$ ksc, $f_y = 3,000$ ksc, $R = 14.76$

$$d = \frac{\sqrt{M}}{\sqrt{Rb}} = \frac{\sqrt{17,500 \times 100}}{\sqrt{14.76 \times 100}} = 34.43 \text{ cm}$$

USE $t = 80$ cm ; $d = 68$ cm

Check Shear

$$V_c = 0.29 \sqrt{f_c'} b d$$

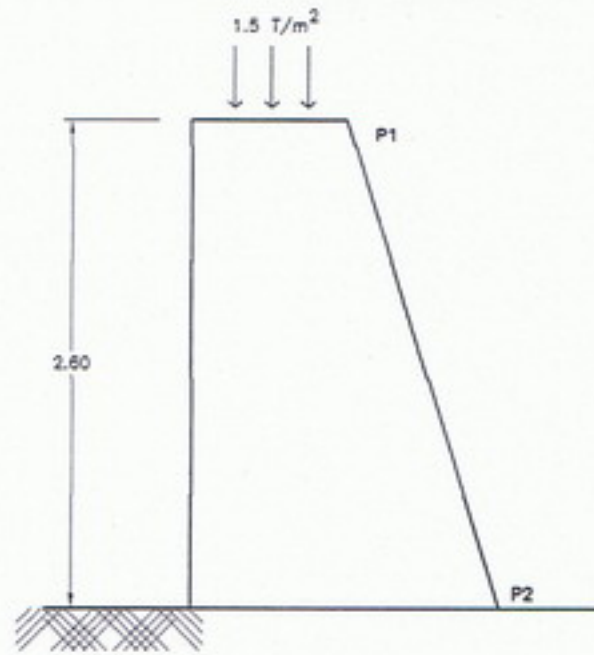
$$= 0.29 \sqrt{200} (100)(68)$$

$$= 27,888 \text{ kg} > V_{\max} = 9,009$$

$$A_{s_{\text{req}}} = \frac{M}{f_s j d} = \frac{17,500 \times 100}{1,500 \times 0.878 \times 68} = 19.54 \text{ cm}^2$$

$$A_{s_{\text{min}}} = \frac{14}{f_y} b d = \frac{14}{3,000} (100 \times 68) = 31.73 \text{ cm}^2$$

USE $\emptyset 25$ mm. @ 0.15 m. ($A_s = 32.75 \text{ cm}^2/\text{m}$)



○ At (-2.60 m)

$$P_1 = K_a P = 0.295 \times 1,500 = 442.50 \text{ kg/m}^2$$

$$P_{(-2.60)} = P_1 + K_a rh = 442.50 + 0.295 (1,500 \times 2.60) = 1,593 \text{ kg/m}^2$$

$$V_{\max} = \frac{1}{2} (442.50 + 1,593) \times 2.60 = 2,647 \text{ kg}$$

$$M_{\max} = 442.50 \times \frac{2.60^2}{2} + \frac{1}{2} (2,647 - 1,593) \times \frac{2.6^2}{3} = 1,495.65 + 1,187.51$$

$$= 2,683 \text{ kg-m}$$

$$d = \sqrt{\frac{2,683 \times 100}{14.76 \times 100}} = 13.48 \text{ cm}$$

$$\text{USE } t = 40 \text{ cm ; } d = 28 \text{ cm}$$

$$A_{s_{\text{req}}} = \frac{2,683 \times 100}{1,500 \times 0.875 \times 28} = 7.30 \text{ cm}^2$$

$$A_{s_{\text{min}}} = \frac{14}{f_y} bd = \frac{14}{3,000} (100 \times 28) = 13.07 \text{ cm}^2$$

$$\text{USE } \varnothing 25 \text{ mm. @ } 0.30 \text{ m. (} A_s = 16.37 \text{ cm}^2/\text{m.)}$$

เหล็กเสริมแนวนอน

$$\begin{aligned} A_s &= 0.002 b d_{sv} \\ &= 0.002 \times 100 \times 50 \\ &= 10 \text{ cm}^2/\text{m} \end{aligned}$$

$$\text{- ด้านสัมผัสดิน} = \frac{1}{3}(10) = 3.34 \text{ cm}^2$$

USE \varnothing 9 mm. @ 0.20 m.

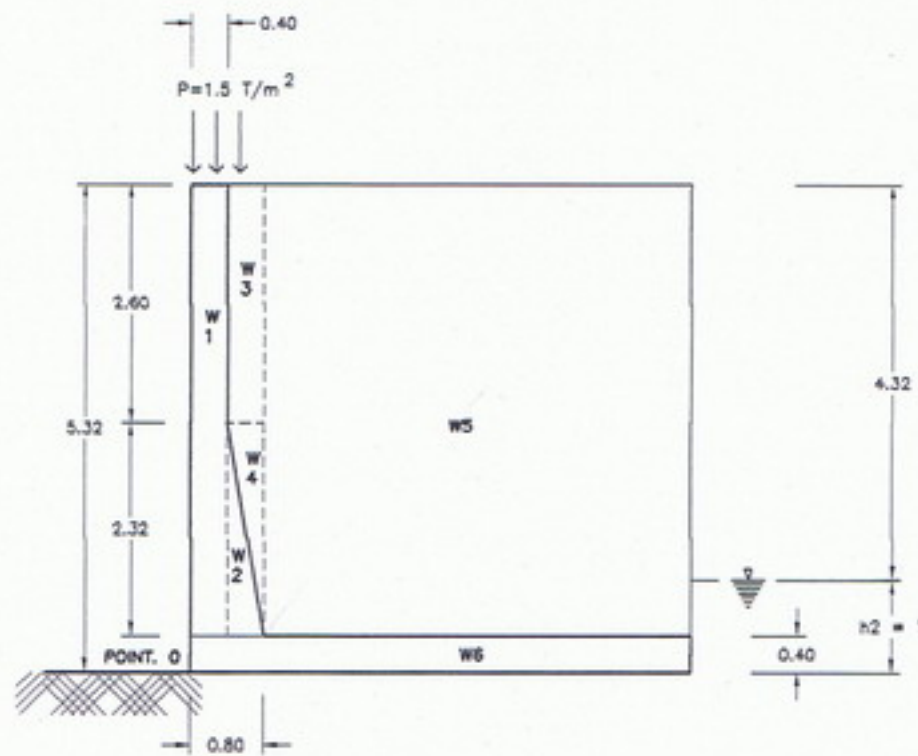
$$\text{- ด้านไม่สัมผัสดิน} = \frac{2}{3}(10) = 6.67 \text{ cm}^2$$

USE \varnothing 12 mm. @ 0.15 m.

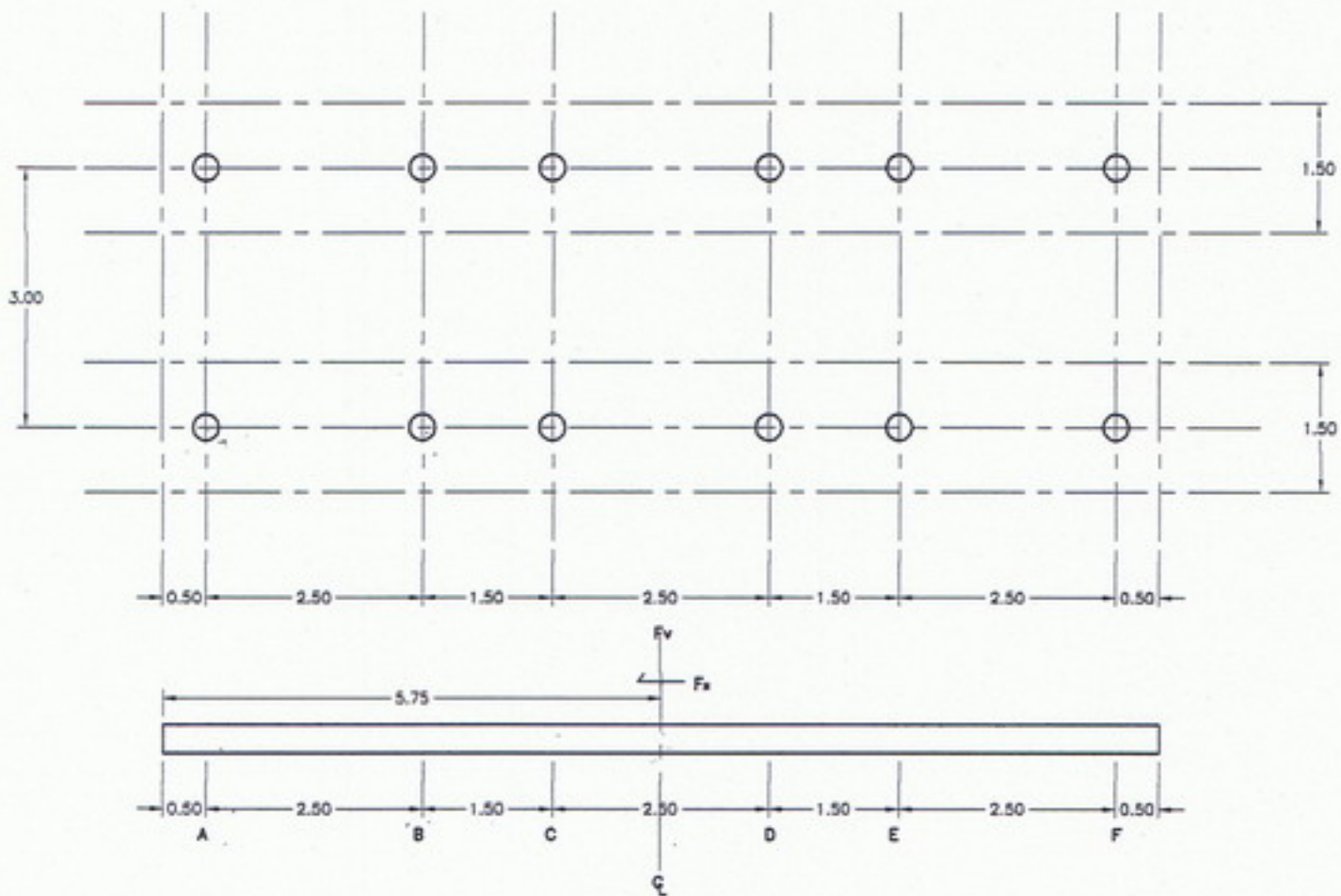
เหล็กเสริมแนวตั้ง

$$A_s = \frac{2}{3}(0.0015)(100)(50) = 5 \text{ cm}^2$$

USE \varnothing 12 mm. @ 0.225 m.



$$\begin{aligned}
 W_1 &= (0.40 \times 4.92 \times 1 \times 2,400) = 4,723.20 \text{ kg/m} \\
 X_1 &= 0.20 \text{ m.} \\
 W_2 &= \left(\frac{1}{2} \times 0.40 \times 2.32 \times 1 \times 2,400\right) = 1,113.60 \text{ kg/m} \\
 X_2 &= \left(0.40 + \frac{0.40}{3}\right) = 0.53 \text{ m.} \\
 W_3 &= (0.40 \times 2.60 \times 1 \times 1,500) = 1,560 \text{ kg/m} \\
 X_3 &= 0.60 \text{ m.} \\
 W_4 &= \left(\frac{1}{2} \times 0.40 \times 2.32 \times 1 \times 2,400\right) = 696 \text{ kg/m} \\
 X_4 &= \left(\frac{2}{3} \times 0.40\right) + 0.40 = 0.67 \text{ m.} \\
 W_5 &= (10.70 \times 4.32 \times 1 \times 1,500 + 0.60 \times 10.70 \times 1 \times 1,775) = 80,731.50 \text{ kg/m} \\
 X_5 &= 6.15 \text{ m.} \\
 W_6 &= (0.40 \times 11.50 \times 1 \times 2,400) = 11,040 \text{ kg/m} \\
 X_6 &= 5.75 \text{ m.} \\
 W_7 &= 1,500 \text{ kg/m} \\
 X_7 &= 5.75 \text{ m.}
 \end{aligned}$$



$$F_H = 11.359 \text{ T/m}$$

$$F_V = 101.37 \text{ T/m}$$

$$e = 5.75 - 5.638 = 0.112 \text{ m.}$$

$$Q = \frac{v}{n} + \frac{(v)(e)(x)}{\sum(x)^2}$$

$$\text{At A, } Q_A = \left[\frac{101.37}{6} + \frac{(101.37 \times 0.112 \times 5.25)}{(5.25^2 \times 2 + 2.75^2 \times 2 + 1.25^2 \times 2)} \right] \times 3$$

$$= 53.12 \text{ tons.}$$

$$\text{At F, } Q_F = \left[\frac{101.37}{6} + \frac{(101.37 \times 0.112 \times (-5.25))}{(5.25^2 \times 2 + 2.75^2 \times 2 + 1.25^2 \times 2)} \right] \times 3$$

$$= 48.25 \text{ tons.}$$

Check Horizontal Force

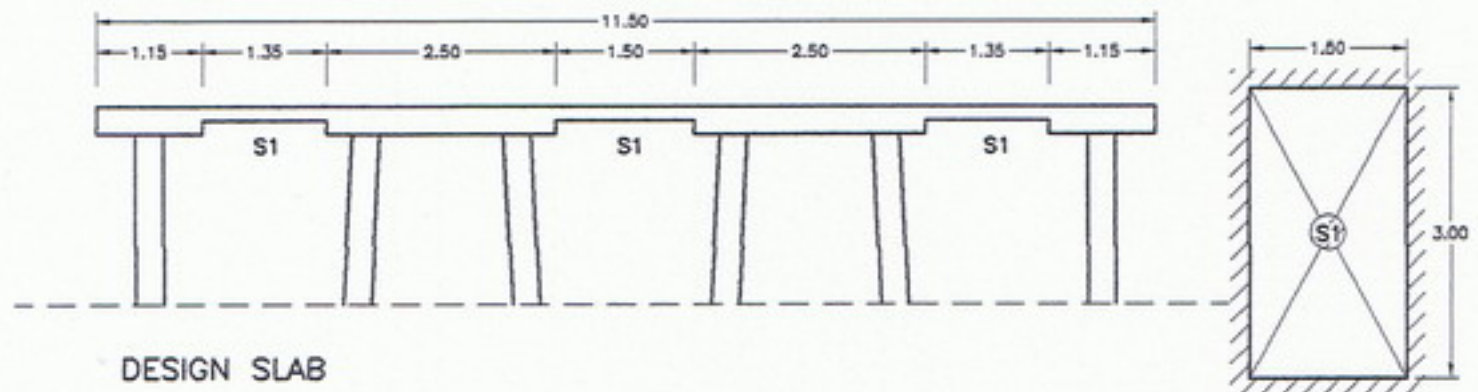
$$F_H = 11.359 \times 3 = 34.10 \text{ tons.}$$

เสาเข็มตำแหน่ง B, C, D, E รับแรงแนวนอน

ตอกเสาเข็มเอียง 1:4 ($Q_F + Q_B = 60 \text{ T/P}$ USE F.S. = 2)

$$R_H = 60 \left(\frac{1}{4.123} \right) \times 4 = 58.21 \text{ tons} > F_H$$

Design Slab



$$LL = [(4.92 \times 1,500) + (1,500)] \times 1 = 8,800 \text{ kg-m.}$$

$$DL = 0.40 \times 2,400 \times 1 = 960 \text{ kg-m.}$$

$$W = 960 + 8,880 = 9,840 \text{ kg-m.}$$

$$M_{\max} = \frac{1}{8} w l^2 = \frac{1}{8} (9,840)(1.35^2) = 2,242 \text{ kg-m.}$$

$$d = \sqrt{\frac{M}{Rb}} = \sqrt{\frac{(2,242)(100)}{14.76 \times 100}} = 12.32 \text{ cm.}$$

USE $d = 30 \text{ cm}$; $t = 40 \text{ cm}$.

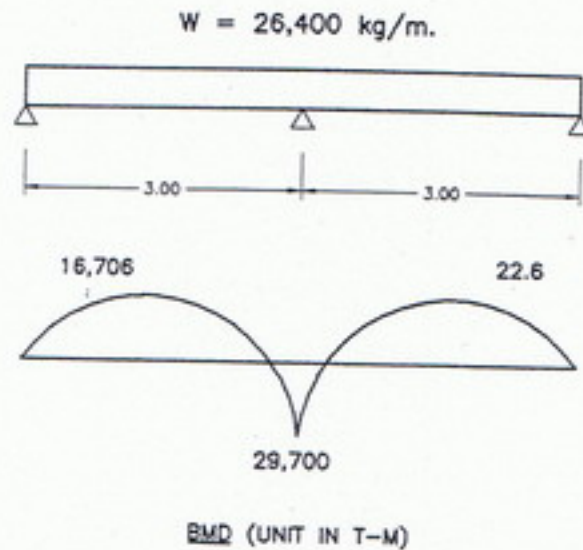
$$A_s = \frac{M}{f_j d} = \frac{(2,242)(100)}{1,500 \times 0.875 \times 30} = 5.69 \text{ cm}^2$$

USE $\varnothing 9 \text{ mm. @ } 0.125 \text{ m. (2 \text{ ชั้น})}$

$$A_s^t = 0.0025 \times 100 \times 30 = 7.5 \text{ cm}^2$$

USE $\varnothing 9 \text{ mm. @ } 0.10 \text{ m. (2 \text{ ชั้น})}$

DESIGN CAB BEAM 2.5 m.



$$W = (4.92 \times 1,500) + (1,500) + (0.70 \times 2,400) \times 2.50 = 26,400 \text{ kg/m.}$$

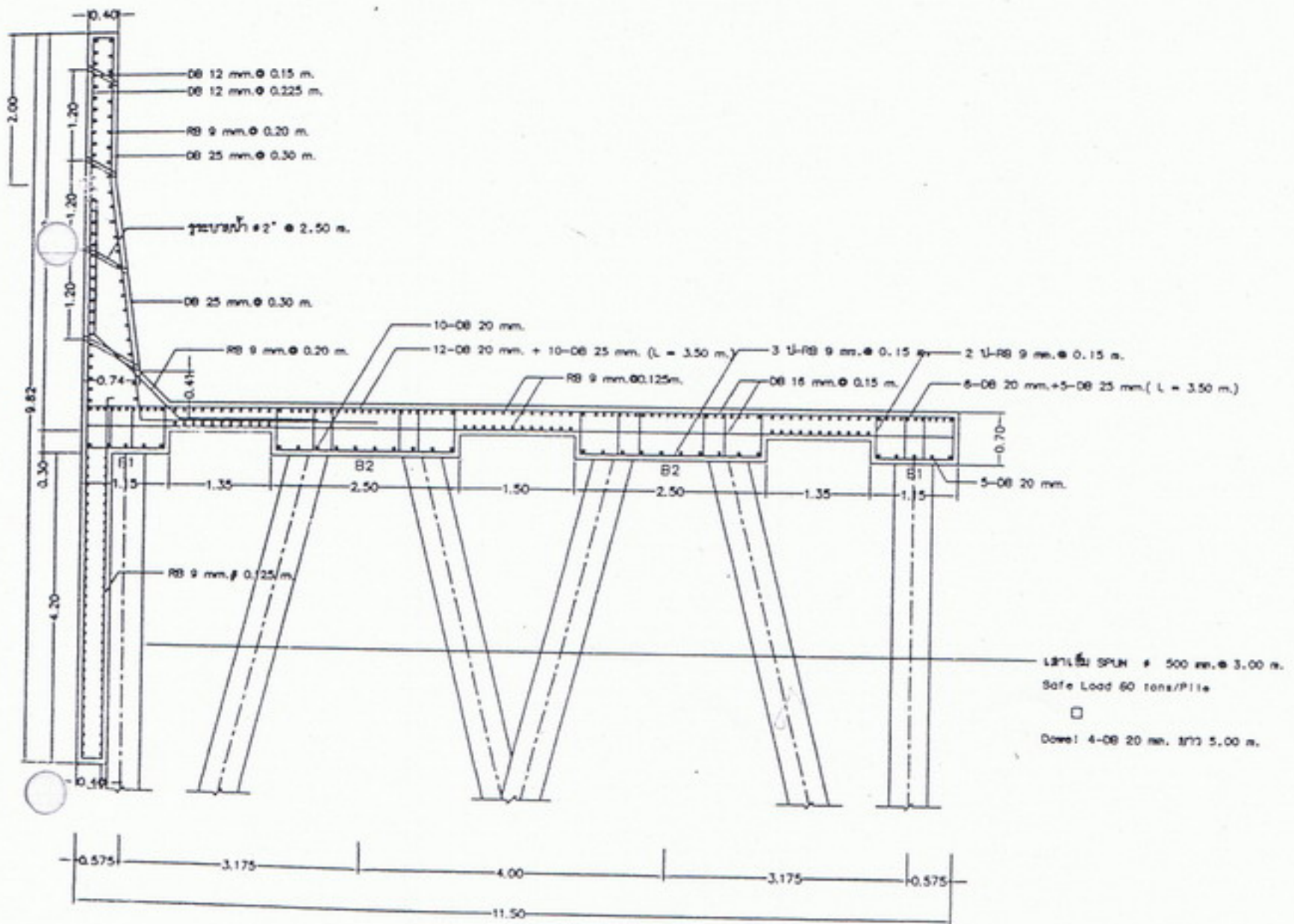
BEAM # CAP BEAM

>SPAN 1 - section 2.5 x .7 , L= 3 m.

w(for MOMENT)= 26400 kg/m : w(for SHEAR)= 26400 kg/m
 ML = 0 kgm / As = 0 sq.cm.
 MR = 29700 kgm / As = 34.8 sq.cm.
 VL = 29700 kg. : VR = 49500 kg. / STIR.#6mm.@ .35
 M+ = 16706 kgm / As = 19.58 sq.cm.
 at 1.13 m. from left support
 R 1 = 29700 kg.

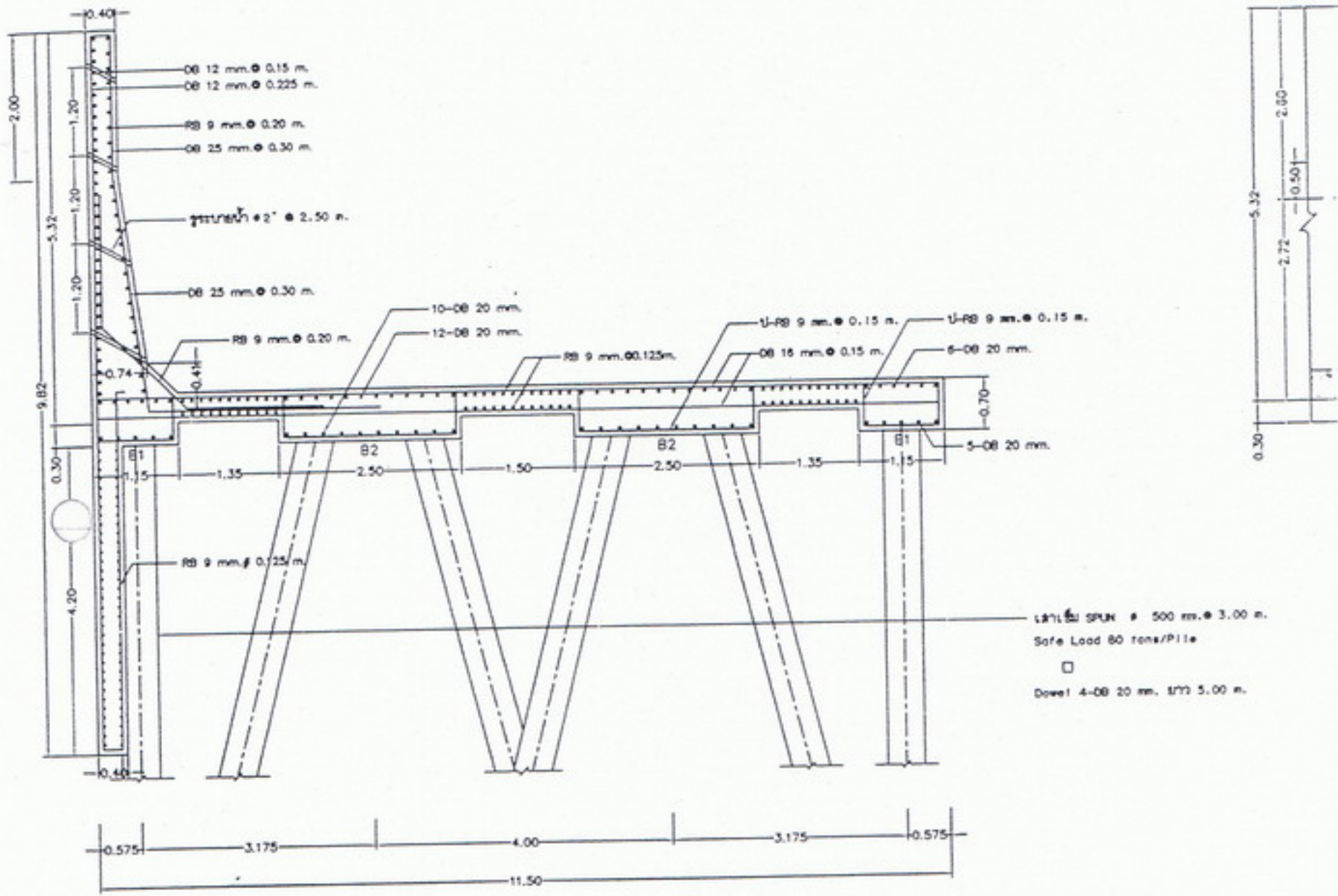
>SPAN 2 - section 2.5 x .7 , L= 3 m.

w(for MOMENT)= 26400 kg/m : w(for SHEAR)= 26400 kg/m
 ML = -29700 kgm / As = 34.8 sq.cm.
 MR = 0 kgm / As = 0 sq.cm.
 VL = 49500 kg. : VR = 29700 kg. / STIR.#6mm.@ .35
 M+ = 16706 kgm / As = 19.58 sq.cm.
 at 1.88 m. from left support
 R 2 = 99000 kg.
 R 3 = 29700 kg.



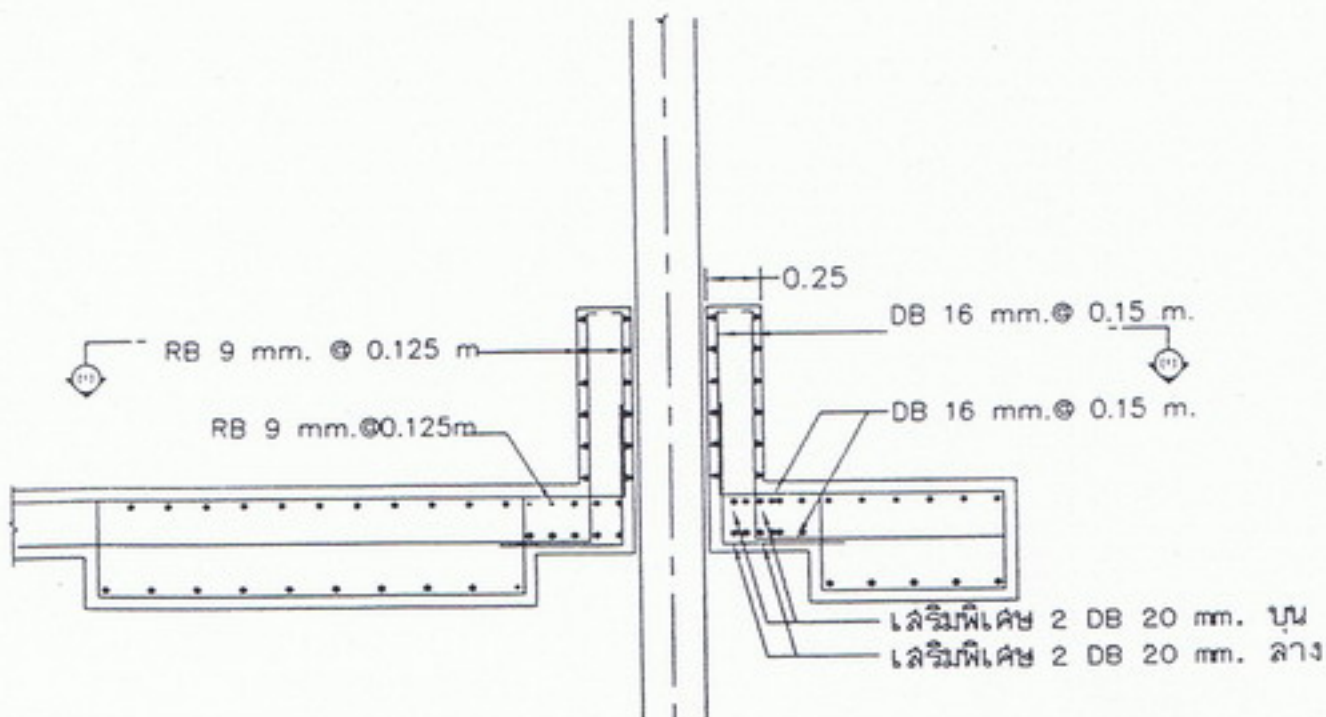
Section A - A

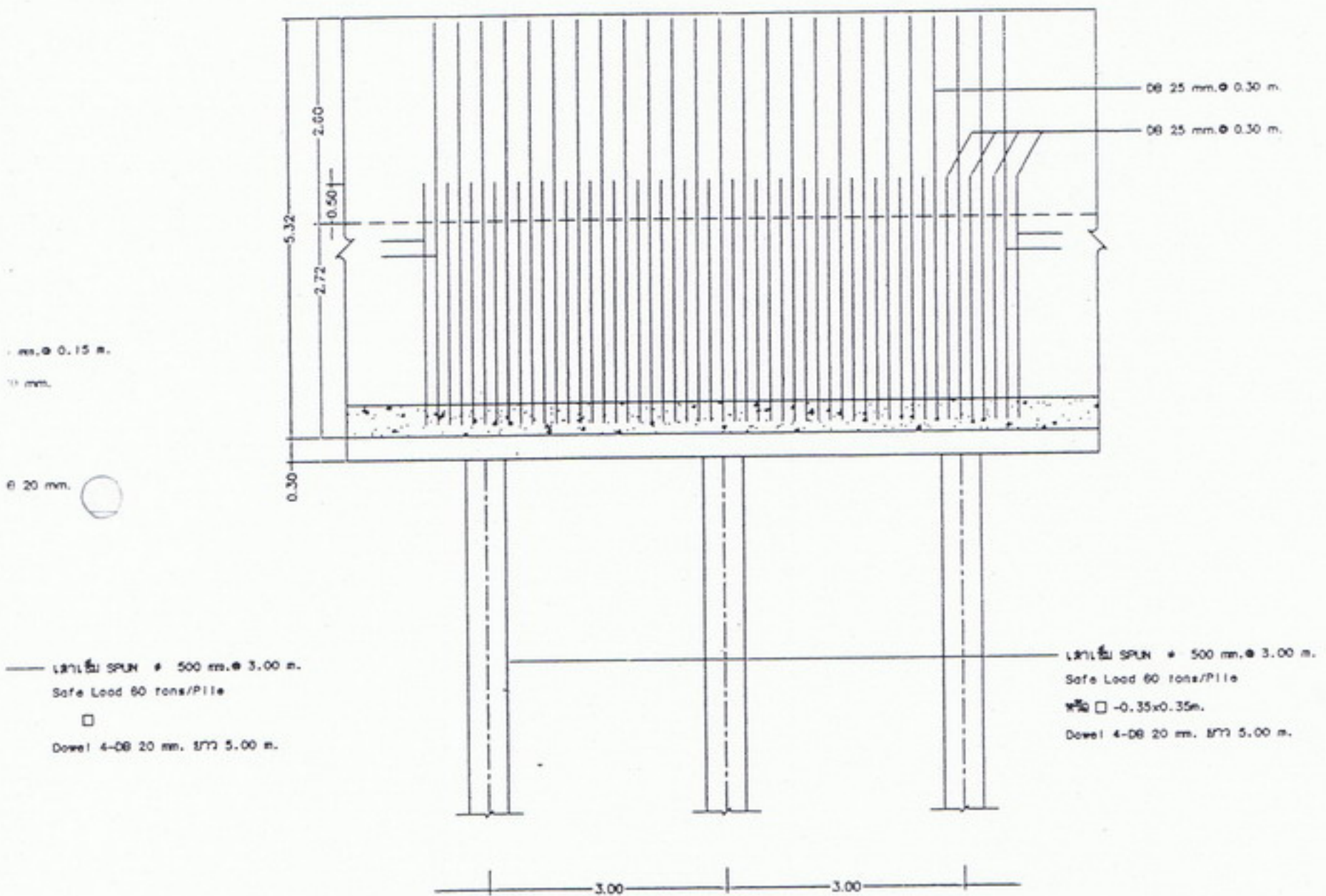
Scale 1 : 100



Typical Section

Scale 1 : 100





แบบขยายรูปตัดตาวายาว เชื้อนกันดิน

Scale 1 : 100

